

<u>CH V</u>

COURSE OUTLINE

- I. INTRODUCTION & BASIC CONCEPTS
- **II. MODELING DYNAMIC SYSTEMS**
- **III. CONTROL SYSTEM COMPONENTS**
- **IV. STABILITY**

V. TRANSIENT RESPONSE

- VI. STEADY STATE RESPONSE
- **VII. DISTURBANCE REJECTION**
- **VIII. BASIC CONTROL ACTIONS & CONTROLLERS**
- **IX. FREQUENCY RESPONSE ANALYSIS**
- X. SENSITIVITY ANALYSIS
- XI. ROOT LOCUS ANALYSIS

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TRANSIENT RESPONSE OBJECTIVES

Completed !

In this chapter :

Time response of general first and second order systems to standard test inputs will be obtained.

We are here !

 Specification of transient response as performance characteristics for control systems will be examined.

 The selection of controller parameters to meet transient response specifications will be explored.

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TRANSIENT RESPONSE of SECOND ORDER SYSTEMS Nise Section 4.4, 4.5, 4.6

There exists a large number of second order systems which are represented by the same general second order differential equation and the corresponding transfer function :

$$a_2 \frac{d^2 x}{dt^2} + a_1 \frac{d x}{dt} + a_0 x = b_1 \frac{d y}{dt} + b_0 y$$
$$G(s) = \frac{X(s)}{Y(s)} = \frac{b_1 s + b_0}{a_2 s^2 + a_1 s + a_0}$$

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$$G(s) = \frac{b_1 s + b_0}{a_2 s^2 + a_1 s + a_0}$$

There exists two more general representations of the transfer functions of second order systems. The first is :

$$\mathbf{G(s)} = \frac{\mathbf{C(s)}}{\mathbf{R(s)}} = \frac{\mathbf{K}\left(\eta\omega_{n}s + \omega_{n}^{2}\right)}{s^{2} + 2\xi\omega_{n}s + \omega_{n}^{2}} \qquad \mathbf{K} = \mathbf{G(0)} = \frac{\mathbf{b}_{0}}{\mathbf{a}_{0}}$$
$$\eta = \frac{\mathbf{b}_{1}}{\mathbf{b}_{0}}\sqrt{\frac{\mathbf{a}_{0}}{\mathbf{a}_{2}}}$$

K : steady state or dc gain. η : characteristic time ratio. <u>ξ</u> : damping ratio.

$$\omega_{n} = \sqrt{\frac{a_{0}}{a_{2}}} \quad \xi = \frac{a_{1}}{2a_{2}} \sqrt{\frac{a_{2}}{a_{1}}}$$

 ω_n : undamped natural frequency.

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$$G(s) = \frac{b_1 s + b_0}{a_2 s^2 + a_1 s + a_0}$$

TRANSIENT RESPONSE of SECOND ORDER SYSTEMS

The <u>second</u> general form of the transfer function for the second order systems is in the form :

$$\frac{G(s) = \frac{C(s)}{R(s)} = \frac{K(T_0 s + 1)}{T^2 s^2 + 2\xi T s + 1}$$

K : steady state (or dc) gain.
 T : system characteristic time.
 T₀ : numerator characteristic time.
 ξ : damping ratio.







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$$G(s) = \frac{C(s)}{R(s)} = \frac{K(T_0 s + 1)}{T^2 s^2 + 2\xi T s + 1}$$

 $\begin{aligned} \mathbf{K} &= \frac{\mathbf{I}}{\mathbf{k}} \\ \mathbf{T}_0 &= \mathbf{0} \end{aligned} \qquad \mathbf{T} = \frac{1}{\omega_n} = \sqrt{\frac{\mathbf{m}}{\mathbf{k}}} \qquad \boldsymbol{\xi} = \frac{\mathbf{c}}{2m\omega_n} \end{aligned}$

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$$\mathbf{m}\ddot{\mathbf{y}} + \mathbf{c}\dot{\mathbf{y}} + \mathbf{k}\mathbf{y} = \mathbf{c}\dot{\mathbf{z}} + \mathbf{k}\mathbf{z}$$



$$G(s) = \frac{C(s)}{R(s)} = \frac{K\left(\eta\omega_n s + \omega_n^2\right)}{s^2 + 2\xi\omega_n s + \omega_n^2} \qquad K = 1 \qquad \eta = \frac{c\omega_n}{k} \qquad \omega_n^2 = \frac{k}{m} \qquad \xi = \frac{c}{2m\omega_n}$$

$$G(s) = \frac{C(s)}{R(s)} = \frac{K\left(T_0 s + 1\right)}{T^2 s^2 + 2\xi T s + 1} \qquad K = 1 \qquad T_0 = \frac{c}{k} \qquad T = \sqrt{\frac{m}{k}} \qquad \xi = \frac{c}{2m\omega_n}$$

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Nise Section 4.5, Dorf&Bishop Section 5.3, Ogata pp.226-229

In this course, we will limit the transient response studies of the second order systems to the step response of the systems represented by the general transfer function of the form :

$$G(s) = \frac{C(s)}{R(s)} = \frac{K\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

Thus numerator dynamics will not be considered.

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$$G(s) = \frac{C(s)}{R(s)} = \frac{K\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

Such a system is classified as :

- undamped if	ξ = 0,
- underdamped if	0 < ξ < 1,
- critically damped if	ξ = 1, and
- overdamped if	ξ > 1.

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$$G(s) = \frac{C(s)}{R(s)} = \frac{K\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

 $s^2 + 2\xi\omega_n s + \omega_n^2 = 0$

The characteristic equation for the second order system is obtained by setting the denominator of the transfer function equal to zero.

The roots of the characteristic equation can be written, in general, as :

$$s_{1,2} = -\xi\omega_n \pm \omega_n \sqrt{\xi^2 - 1}$$

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$$G(s) = \frac{C(s)}{R(s)} = \frac{K\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

The roots of the characteristic equation are called the poles of the system.

$$s_{1,2} = -\xi\omega_n \pm \omega_n \sqrt{\xi^2 - 1}$$

 Similarly, the roots of the numerator polynomial of the transfer function are called the zeroes of the system.

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 $\mathbf{s_{1,2}} = -\xi \omega_{\mathbf{n}} \pm \omega_{\mathbf{n}} \sqrt{\xi^2 - 1}$

Thus, for

• undamped ($\xi=0$) systems there are $s_{1,2} = \pm j\omega_n$ two purely imaginary roots (poles), critically damped (ξ=1)systems, there are two identical (repeated) real roots, $s_{1,2} = -\omega_n$ • overdamped ($\xi > 1$) systems, there are $s_1 = -\omega_{n1}$ two distinct negative real roots, and $s_2 = -\omega_{n2}$ • underdamped ($\xi < 1$) systems, there are two complex conjugate roots. $s_{1,2} = -\xi\omega_n \pm j\omega_n \sqrt{1-\xi^2}$

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$$s_{1,2} = -\xi \omega_n \pm j \omega_d$$
$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$



The roots of the characteristic equation on the complex plane.

$$\xi = 0 \implies s_{1,2} = \pm j\omega_n$$

$$=1 \implies s_{1,2} = -\omega_n$$

$$\xi > 1 \implies s_{1,2} = -\xi \omega_n \pm \omega_n \sqrt{\xi^2 - 1}$$

$$\xi < 1 \implies s_{1,2} = -\xi \omega_n \pm j \omega_d$$

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FIRST ORDER SYSTEMS



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G(s) :

The root of the characteristic equation is always negative and real.

Thus the response will contain an exponential term.

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$$\frac{C(s)}{R(s)} = \frac{K\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$
UNDAMPED SECOND ORDER SYSTEMS

• Undamped System ($\xi = 0$) – Step input :



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G(s) =

$$\mathbf{c}(\mathbf{t}) = \mathbf{K}\mathbf{R}\big(1 - \cos\omega_{\mathbf{n}}\mathbf{t}\big)$$

 It is clear that the step response of a general undamped second order system is a harmonic function with frequency ω_n, superimposed on a step function.



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17

Underdamped System (0<ξ<1) – Step input :

$$G(s) = \frac{C(s)}{R(s)} = \frac{K\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

$$R(s) = \frac{R}{s}$$

$$C(s) = \frac{K\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2} \frac{R}{s}$$

$$R(s) = \frac{R}{s}$$

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$$\mathbf{c(s)} = \mathbf{KR} \left[\frac{1}{s} - \frac{s + \xi \omega_n}{\left(s + \xi \omega_n\right)^2 + \omega_d^2} - \frac{\xi \omega_n}{\left(s + \xi \omega_n\right)^2 + \omega_d^2} \right]$$

Taking the inverse Laplace transform :

$$\mathbf{c}(t) = \mathbf{K}\mathbf{R}\left[1 - \frac{e^{-\xi\omega_{n}t}}{\sqrt{1 - \xi^{2}}}\sin\left(\omega_{d}t + \tan^{-1}\frac{\sqrt{1 - \xi^{2}}}{\xi}\right)\right] \quad t \ge 0$$

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UNDERDAMPED SECOND ORDER SYSTEMS



UNDERDAMPED SECOND ORDER SYSTEMS



CRITICALLY DAMPED SECOND ORDER SYSTEMS

Critically Damped System (ξ=1) – Step input :

$$G(s) = \frac{C(s)}{R(s)} = \frac{K\omega_n^2}{s^2 + 2\omega_n s + \omega_n^2}$$

$$R(s) = \frac{R}{s}$$

$$C(s) = \frac{K\omega_n^2}{(s + \omega_n)^2} \frac{R}{s}$$

$$C(t) = KR \left[1 - e^{-\omega_n t} \left(1 + \omega_n t \right) \right]$$

$$t \ge 0$$

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CRITICALLY DAMPED SECOND ORDER SYSTEMS

Critically damped second order system - ξ **=1 Fast response with no oscillations.** Image



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Overdamped System (ξ>1) – Step input :

$$G(s) = \frac{C(s)}{R(s)} = \frac{K\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

$$R(s) = \frac{R}{s}$$

$$G(s) = \frac{K\omega_n^2}{(s + \xi\omega_n + \omega_d)(s + \xi\omega_n - \omega_d)}$$

$$C(t) = KR\left[1 + \frac{\omega_n}{2\sqrt{\xi^2 - 1}} \left(\frac{e^{-s_1 t}}{s_1} - \frac{e^{-s_2 t}}{s_2}\right)\right] \quad t \ge 0$$

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Overdamped System (ξ>1) – Step input :



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Overdamped System (ξ>1) – Step input :



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Step input response :



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TRANSIENT RESPONSE OBJECTIVES

In this chapter :

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Now we are here !

The selection of controller parameters to meet transient response specifications will be explored.

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TRANSIENT RESPONSE SPECIFICATIONS

Nise Sect. 4.5, 4.6, Dorf&Bishop Section 5.3, Ogata pp.229-235

- The performance of a control system is usually specified in terms of its transient response to a unit step input.
- To be able to compare different systems under the same conditions, the system is assumed to be stable and initially at rest with zero output.

TRANSIENT RESPONSE SPECIFICATIONS

 In specifying the transient response of a control system in relation to its speed of response and relative stability, the most commonly used parameters are :

- Delay Time (t_d),
- Rise Time (t_r),
- Peak Time (t_p),
- Settling Time (t_s),
- Maximum Overshoot (M_p). Stability

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Speed of Response

Relative

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<u>SPECIFICATIONS</u>

- The speed of response is judged by how fast the response reaches the final or steady state value.
- Relative Stability is related to how oscillatory the system will be before reaching the steady state.

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TRANSIENT RESPONSE SPECIFICATIONS



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TRANSIENT RESPONSE SPECIFICATIONS



A better approximation : $t_d \cong \frac{1 + 0.125\xi + 0.469\xi^2}{\omega_n}$

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TRANSIENT RESPONSE SPECIFICATIONS

Rise Time (t_r)

For underdamped systems :

 Time required for the <u>unit step</u> response to reach :

from 0 to 100 %

of the final value.



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Rise Time (t_r)

Note that to minimize t_r :

- 1.ξ must be as small as possible for a given ω_n.
- 2. For a given ξ , ω_n must be as high as possible.



Rise Time (t_r)

For overdamped systems :

Time required for the unit step response to reach :

from 10 to 90 % of the final value.



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Peak Time (t_p)

Time required for the unit step response to reach the peak of the first overshoot.





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Peak Time (t_p)

Note that to minimize t_p :

- 1. ξ must be as small as possible for a given ω_n .
- 2. For a given ξ , ω_n must be as high as possible.



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<u>Maximum</u> <u>Overshoot</u> (M_p)

The highest peak value of the response curve as measured from the final (steady state) value.



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Maximum Overshoot (M_p) Since M_p is obtained at t_p :

$$\mathbf{M}_{\mathbf{p}} = \frac{\mathbf{c}(\mathbf{t}_{\mathbf{p}})}{\mathbf{K}} - \mathbf{1}$$

 $\mathbf{M}_{\mathbf{p}} = \mathbf{e}^{-\pi \left(\frac{\xi}{\sqrt{1-\xi^2}}\right)}$

 $\frac{\mathbf{c}(\mathbf{t})}{\mathbf{K}} \qquad \mathbf{M}_{\mathbf{p}}$ $\mathbf{1} \qquad \mathbf{t}_{\mathbf{p}}$

Time

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<u>Settling Time</u> (t_s)

Time required for the response to reach and stay within a range (either 2 or 5 %) about the final value.



Settling Time (t_s) Approximate expressions are given by :

$$t_{s}(2\%) = \frac{4}{\xi\omega_{n}}$$
$$t_{s}(5\%) = \frac{3}{\xi\omega_{n}}$$

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 If a more general transfer function where numerator dynamics exist, the general form of the transfer function takes the following form.

$$G(s) = \frac{C(s)}{R(s)} = \frac{K(\eta\omega_n s + \omega_n^2)}{s^2 + 2\xi\omega_n s + \omega_n^2}$$

In this case, the expressions for the calculation of relevant transient response specifications are somewhat more involved.

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Rise Time (t_r) (0-100%)



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Settling Time (t_s)

$$t_{s} = \frac{1}{\xi \omega_{n}} \ln \frac{a_{0}}{\varepsilon_{s}}$$

where ε_s is either 0.02 or 0.05 and

$$\mathbf{a}_0 = \frac{\sqrt{\eta^2 - 2\xi\eta + 1}}{\sqrt{1 - \xi^2}}$$

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Maximum Overshoot (Mp)



where

$$a_0 = \frac{\sqrt{\eta^2 - 2\xi\eta + 1}}{\sqrt{1 - \xi^2}} \quad \varphi = \tan^{-1} \left(\frac{\xi - \eta}{\sqrt{1 - \xi^2}} \right) \quad \beta = \sin^{-1} \sqrt{1 - \xi^2}$$

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Note that when

η=0

these expressions will reduce to the forms given earlier for the general system with no numerator dynamics.

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TRANSIENT RESPONSE OBJECTIVES

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- It is noted that for fast response which requires small t_d, t_r, and t_p:
 - on must be as large as possible, and
 - ξ must be as small as possible.



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- On the other hand, for better relative stability (indicated by M_p and t_s), a higher value of ξ is desired.
- In view of the conflicting requirements for fast response and better relative stability, a compromise value for ξ is required, i.e. It is not possible to reduce, say, both rise time and maximum overshoot.

- Therefore, a value within the range 0.5 to 0.8 (0.7 most common) is commonly used.
- For certain applications, such as robotic manipulators, where overshoot is unacceptable, critical damping (ξ = 1) is used.

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TRANSIENT RESPONSE SPECIFICATIONS – Example 1a

- Consider a control system represented by the block diagram shown. Determine the values of K₁ and K₂ such that the
 - maximum overshoot is to be 6 %, and the
 - 5 % settling time is to be <u>at most</u> 4 seconds

for a unit step input.



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TRANSIENT RESPONSE SPECIFICATIONS – Example 1b

First obtain the overall transfer function.





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TRANSIENT RESPONSE SPECIFICATIONS – Example 1c

First obtain the overall transfer function.



TRANSIENT RESPONSE SPECIFICATIONS – Example 1d

Maximum overshoot is to be 6 %.

$$M_{p} = e^{-\pi \left(\frac{\xi}{\sqrt{1-\xi^{2}}}\right)} = 0.06$$

$$-\pi \left(\frac{\xi}{\sqrt{1-\xi^{2}}}\right) = -2.813$$

$$\xi = 0.67$$

$$\frac{\xi}{\sqrt{1-\xi^{2}}} = 0.896$$

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TRANSIENT RESPONSE SPECIFICATIONS – Example 1e

5 % settling time is specified to be <u>at most</u> 4 seconds.

$$t_{s}(5\%) \cong \frac{3}{\xi\omega_{n}} \le 4$$

$$\xi = 0.67$$

$$\omega_{n} \ge \frac{3}{4\xi} = \frac{3}{4(0.67)} \cong 1.12 \text{ [rad/s]}$$

$$\omega_{n} \ge 1.12 \text{ [rad/s]}$$

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TRANSIENT RESPONSE SPECIFICATIONS – Example 1f

Find the range for K₁.



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TRANSIENT RESPONSE SPECIFICATIONS – Example 1g

Find the range for K₂.



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Nise Sect. 4.7, Dorf & Bishop 5.4,pp. 258, Ogata pp. 240-242

The transfer function of an nth order system, with no multiple poles, is given by :

$$G(s) = \frac{K \prod_{i=1}^{m} (s + z_i)}{\prod_{j=1}^{q} (s + p_j) \prod_{k=1}^{r} (s^2 + 2\xi_k \omega_k s + \omega_k^2)}$$

where

- m : number of zeros (-z_i),
- q : number of distinct poles (-p_i),
- r : number of complex conjugate pair poles.

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 As an example, remember the overdamped second order system (ξ>1).

$$\frac{G(s) = \frac{K\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2} = \frac{K}{\left(s + \xi\omega_n + \omega_n\sqrt{\xi^2 - 1}\right)} \frac{\omega_n^2}{\left(s + \xi\omega_n - \omega_n\sqrt{\xi^2 - 1}\right)}$$

 Notice that it is composed of two first order systems.

$$\mathbf{G}(\mathbf{s}) = \frac{\mathbf{K}_1}{\left(\mathbf{s} + \mathbf{p}_1\right)} \frac{\mathbf{K}_2}{\left(\mathbf{s} + \mathbf{p}_2\right)}$$

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The unit step time response of the system will be :

$$\mathbf{y}(t) = \mathbf{a} \left(+ \sum_{j=1}^{q} \mathbf{a}_{j} e^{-\mathbf{p}_{j} t} + \sum_{k=1}^{r} \left[\mathbf{A}_{k} e^{-\xi_{k} \omega_{k} t} \cos\left(\omega_{k} \sqrt{1 - \xi_{k}^{2}} t - \phi_{k}\right) \right] \right)$$

Exponential decays Decaying Oscillations

The step response of a higher order system is composed of the step responses of a number of first and second order underdamped systems.

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- Evidently the larger p_j and $\xi_k \omega_k$ are, the faster will be the decay of the response due to these poles.
- Coefficients a_j and A_k depend not only on poles but also on zeros of the transfer function.

$$y(t) = a + \sum_{j=1}^{q} a_j e^{-p_j t} + \sum_{k=1}^{r} \left[A_k e^{-\xi_k \omega_k t} \cos\left(\omega_k \sqrt{1 - \xi_k^2} t - \phi_k\right) \right]$$

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TRANSIENT RESPONSE OF HIGHER ORDER SYSTEMS Dorf&Bishop, pp. 253-258, Ogata pp. 240-242

Two points to note :

- If the ratio of the real parts of two poles exceeds five (5) and there are no nearby zeros to cancel those poles, the pole nearest to the imaginary axis will be dominant.
- If the value of a zero is very close to that of a pole, then the effect of the pole will be cancelled.



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TRANSIENT RESPONSE OF <u>HIGHER</u> ORDER SYSTEMS – Example a

A control system is represented by the following closed loop transfer function.

$$G(s) = \frac{10s + 29}{\left(s^2 + 2s + 2\right)\left(s^2 + 28s + 75\right)}$$

Estimate the time after which the output y(t) remains within 2% of the final value.

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$$G(s) = \frac{10s + 29}{\left(s^2 + 2s + 2\right)\left(s^2 + 28s + 75\right)}$$

TRANSIENT RESPONSE OF HIGHER ORDER SYSTEMS Example b

System is fourth order and the poles and zeros are :

$$s^{2} + 2s + 2 = 0 \implies p_{1} = -1 + j , p_{2} = -1 - j$$
$$s^{2} + 28s + 75 = 0 \implies p_{3} = -25 , p_{4} = -3$$
$$10s + 29 = 0 \implies z = -2.9$$

$$G(s) = \frac{10(s+2.9)}{(s+1-1j)(s+1+1j)(s+25)(s+3)}$$

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TRANSIENT RESPONSE OF <u>HIGHER</u> ORDER SYSTEMS – Example c

$$G(s) = \frac{10(s+2.9)}{(s+1-j)(s+1+j)(s+25)(s+3)}$$

- As the zero (-2.9) is very near the fourth pole (-3.0), one can cancel these two.
- The third pole (-25.0) is more than five times away from the real part of the complex poles, thus it can be neglected.

$$G(s) = \frac{10}{(s+1-j)(s+1+j)} = \frac{10}{s^2+2s+2}$$

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TRANSIENT RESPONSE OF <u>HIGHER</u> ORDER SYSTEMS – Example d

$$\mathbf{G(s)} = \frac{10}{\mathbf{s}^2 + 2\mathbf{s} + 2}$$

 It is left to the student to show that the 2 % settling time of the simplified system is around 4 seconds.

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TRANSIENT RESPONSE OF <u>HIGHER</u> <u>ORDER SYSTEMS</u> – Example e



 The unit step responses of the fourth order and the simplified second order
system are almost indistinguishable.

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MIDTERM

	2005	2006	2007	2008
Average	71.6	63.3	66.0	56.5
St. Dev.	18.4	24.2	22.1	20.5
Max.	99	100	100	99
Min.	10	12	01	12

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