



COURSE OUTLINE

- I. INTRODUCTION & BASIC CONCEPTS
- II. MODELING DYNAMIC SYSTEMS
- III. CONTROL SYSTEM COMPONENTS
- IV. STABILITY
- V. TRANSIENT RESPONSE
- VI. STEADY STATE RESPONSE
- VII. DISTURBANCE REJECTION
- VIII. BASIC CONTROL ACTIONS & CONTROLLERS
- IX. FREQUENCY RESPONSE ANALYSIS

X. SENSITIVITY ANALYSIS

XI. ROOT LOCUS ANALYSIS

SENSITIVITY - OBJECTIVES

Getting familiar with the concept of sensitivity.

Applying sensitivity analysis to basic components of control systems.

Investigation of sensitivity of control systems to parameter variations.

SENSITIVITY - Definition

Nise Section 7.7, Dorf&Bishop Section 4.2

- There are many uncertainties encountered in the design and analysis of control systems.
- In modeling and parameter selection imperfections and inaccuracies always exist.
- Parameters may also vary in time due to age, wear, etc.

SENSITIVITY - Definition

- One of the basic design criteria for control systems is to minimize the sensitivity of the response to modelling inaccuracies and parameter variations.
- In control system terminology, a system that is insensitive to external disturbances and parameter variations is called a robust system.

SENSITIVITY - Definition

The sensitivity function of a system is defined as the ratio of the percentage variation of the system transfer function, M, to the percentage variation of a system parameter, k.

$$S_k^M = \frac{\frac{dM}{M}}{\frac{dk}{k}} = \frac{\text{percentage change in M (due to a change in k)}}{\text{percentage change in k}}$$

SENSITIVITY Open Loop Control System

Consider the open loop control system.

$$C(s)$$

$$C(s)$$

$$C(s)$$

Sensitivity of C(s) w.r.t. G(s)

$$S_G^C = \frac{dC/C}{dG/G}$$

SENSITIVITY Open Loop Control System

$$C(s) = G(s)R(s)$$

$$dC(s) = dG(s)R(s)$$

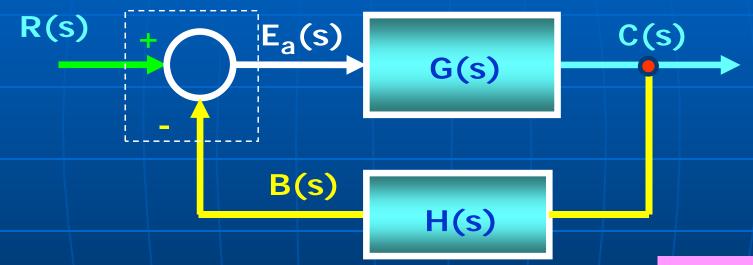
$$S_G^C = \frac{G}{C} \frac{dC}{dG} = \frac{G}{GR} \frac{(dG)R}{dG} = 1$$



Therefore, any change or uncertainity in the transfer function of the open loop system is directly reflected in the output of the system.

SENSITIVITY Closed Loop System

 Consider the general (canonical) form of the closed loop control system.



- Sensitivity of C(s) w.r.t. G(s)
- Sensitivity of C(s) w.r.t. H(s)

$$S_G^C = \frac{dC/C}{dG/G}$$

$$S_{H}^{C} = \frac{dC/C}{dH/H}$$

Feedforward and feedback elements

Express the output in terms of the input.

$$\frac{C(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)}$$

$$C(s) = \frac{G(s)}{1 + G(s)H(s)}R(s)$$

$$dC = \frac{dG(1 + GH) - G(GdH + HdG)}{(1 + GH)^{2}}R = \frac{dG - G^{2}dH}{(1 + GH)^{2}}R$$

$$\frac{dC}{C} = \left[\frac{dG - G^{2}dH}{(1 + GH)^{2}} R \right] \left(\frac{1 + GH}{G} \right) \frac{1}{R} = \frac{dG - G^{2}dH}{G(1 + GH)}$$



$$\frac{dC}{C} = \frac{1}{1 + GH} \frac{dG}{G} - \frac{GH}{1 + GH} \frac{dH}{H}$$

Feedforward and feedback elements

$$\frac{dC}{C} = \frac{1}{1 + GH} \frac{dG}{G} - \frac{GH}{1 + GH} \frac{dH}{H}$$

Let dH=0:

$$S_G^C = \frac{dC/C}{dG/G} = \frac{1}{1 + GH}$$

Let dG=0:

$$S_{H}^{C} = \frac{dC/C}{dH/H} = -\frac{GH}{1 + GH}$$

Feedforward and feedback elements

If large controller gains are chosen so that :

$$|G(s)H(s)| \rightarrow \infty$$

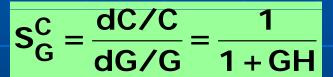
Then

$$\lim_{GH\to\infty} S_G^C = 0$$

which is very good!

$$lim_{GH\to\infty}S_H^C = -1$$

which is not so good!



$$S_H^C = \frac{dC/C}{dH/H} = -\frac{GH}{1 + GH}$$

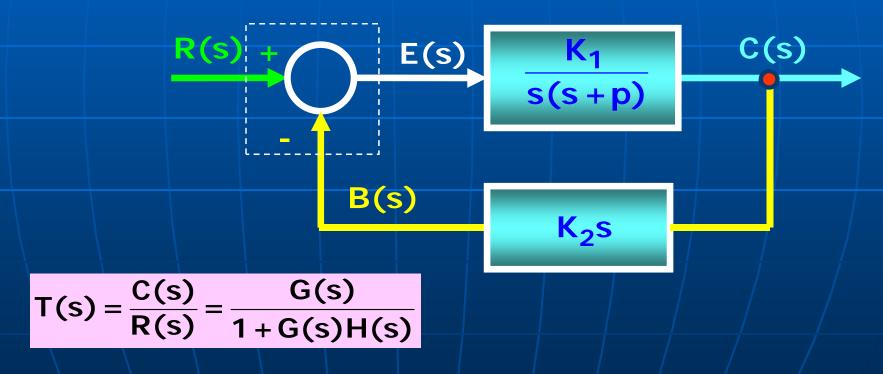
Feedforward and feedback elements

Therefore by choosing

$$|G(s)H(s)| \to \infty$$

- The effects of parameter variations in feedforward elements (i.e. the controller, the actuator, the plant) can be suppressed.
- The effects of the parameter variations in feedback elements (sensors) <u>cannot</u> be suppressed and their variations will be fully reflected in the variation of the output.
- Conclusion: Quality of a feedback control system depends on the quality of measurement.

Let us determine the sensitivity of the transfer function of the system represented by the block diagram shown, to variations in each of the parameters K₁, K₂, and p.



Sensitivity of the transfer function w.r.t. variations in the feedforward gain K₁.

$$T(s) = \frac{\frac{K_1}{s(s+p)}}{1 + \frac{K_1K_2s}{s(s+p)}} = \frac{K_1}{s(s+p+K_1K_2)}$$

$$S_{K_{1}}^{T}(s) = \frac{K_{1}}{T} \frac{dT}{dK_{1}} = \frac{K_{1}}{K_{1}} \frac{1}{s} \frac{(s+p+K_{1}K_{2})-K_{1}(K_{2})}{(s+p+K_{1}K_{2})^{2}} \frac{1}{s} \frac{(s+p+K_{1}K_{2})-K_{1}(K_{2})}{(s+p+K_{1}K_{2})^{2}}$$

$$S_{K_1}^{T}(s) = \frac{s+p}{s+p+K_1K_2}$$

Sensitivity of the transfer function w.r.t. variations in the feedback gain K₂.

$$T(s) = \frac{\frac{K_1}{s(s+p)}}{1 + \frac{K_1K_2s}{s(s+p)}} = \frac{K_1}{s(s+p+K_1K_2)}$$

$$S_{K_{2}}^{T}(s) = \frac{K_{2}}{T} \frac{dT}{dK_{2}} = \frac{K_{2}}{\frac{K_{1}}{s(s+p+K_{1}K_{2})}} \frac{1 - K_{1}(K_{1})}{s(s+p+K_{1}K_{2})^{2}}$$

$$S_{K_2}^{T}(s) = \frac{-K_1K_2}{s + p + K_1K_2}$$

Sensitivity of the transfer function w.r.t. variations in the open loop pole p.

$$T(s) = \frac{\frac{K_1}{s(s+p)}}{1 + \frac{K_1K_2s}{s(s+p)}} = \frac{K_1}{s(s+p+K_1K_2)}$$

$$S_{p}^{T}(s) = \frac{p}{T} \frac{dT}{dp} = \frac{p}{\frac{K_{1}}{s(s+p+K_{1}K_{2})}} \frac{1}{s} \frac{-K_{1}(1)}{(s+p+K_{1}K_{2})^{2}}$$

$$S_{p}^{T}(s) = \frac{-p}{s + p + K_{1}K_{2}}$$

 It is noted that the sensitivity expressions are in general functions of s.

$$S_{K_1}^{T}(s) = \frac{s+p}{s+p+K_1K_2}$$

$$S_{K_2}^{T}(s) = \frac{-K_1K_2}{s + p + K_1K_2}$$

$$S_p^{\mathsf{T}}(s) = \frac{-p}{s + p + K_1 K_2}$$

 The steady state sensitivities can be obtained by letting s=0 in those expressions.

$$S_{K_1}^{T}|_{ss} = S_{K_1}^{T}(0) = \frac{p}{p + K_1 K_2}$$

$$S_{K_2}^{T}|_{SS} = S_{K_2}^{T}(0) = \frac{-K_1K_2}{p + K_1K_2}$$

$$|S_p^T|_{ss} = S_p^T(0) = \frac{-p}{p + K_1 K_2}$$

The dynamic sensitivity is obtained by letting

$$s=j\omega$$

in the sensitivity expressions, and then by plotting the sensitivity versus frequency.

It is also possible to determine the sensitivity of the roots of the characteristic equation for small variations of a parameter in a similar manner.

SENSITIVITY - Reading

Study Examples 7.10-7.12, and solve Exercise 7.21 and problems 7.44-7.45 in Nise.

Dorf & Bishop 4.8 Design Example: Mars Rover Vehicle, pp. 212-214.