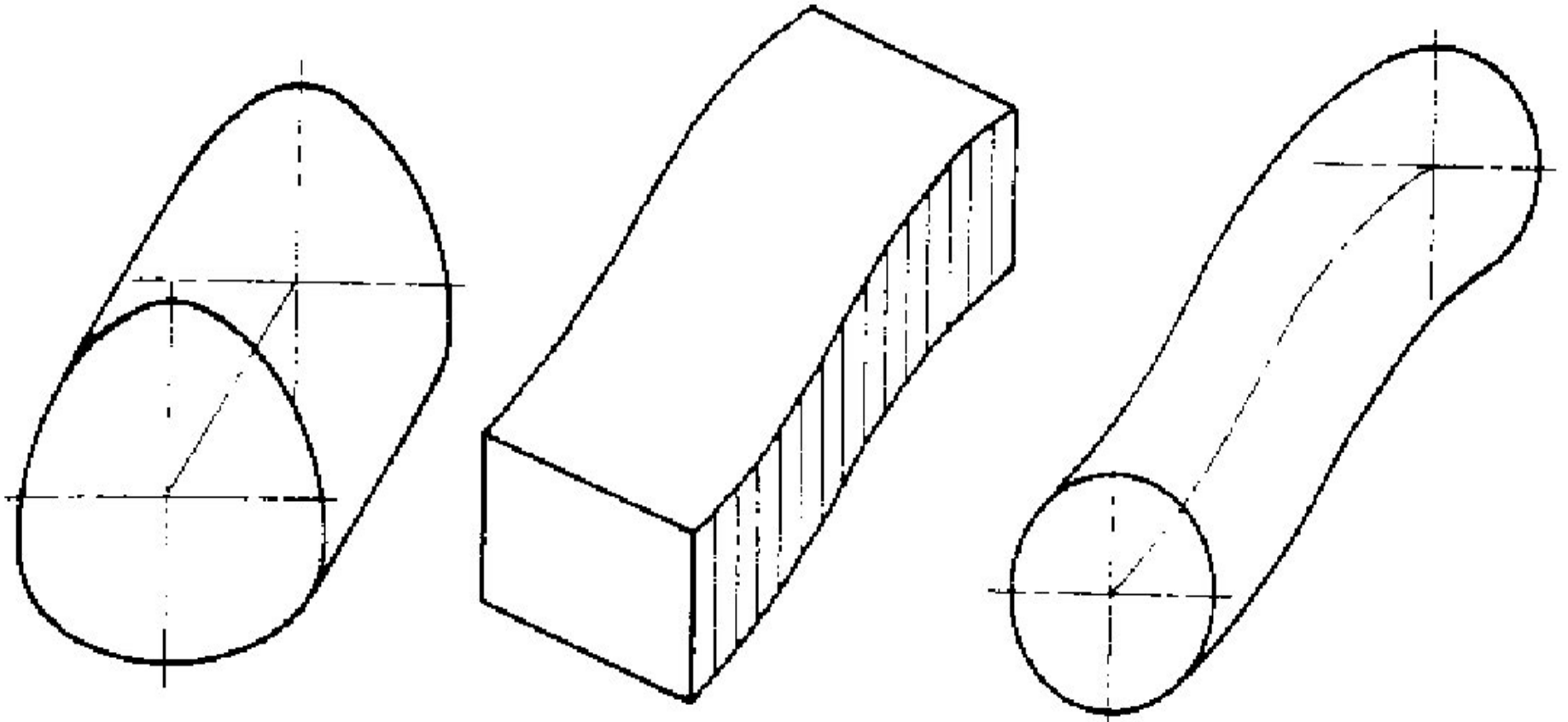
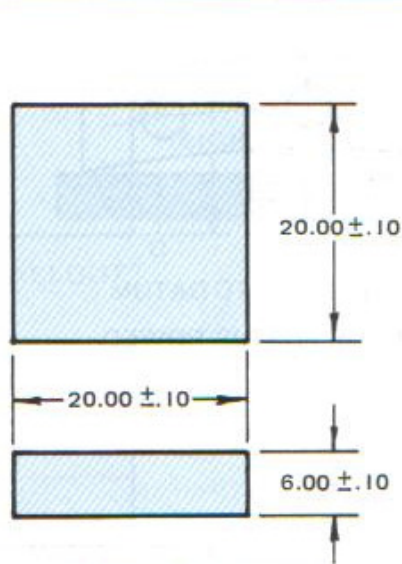
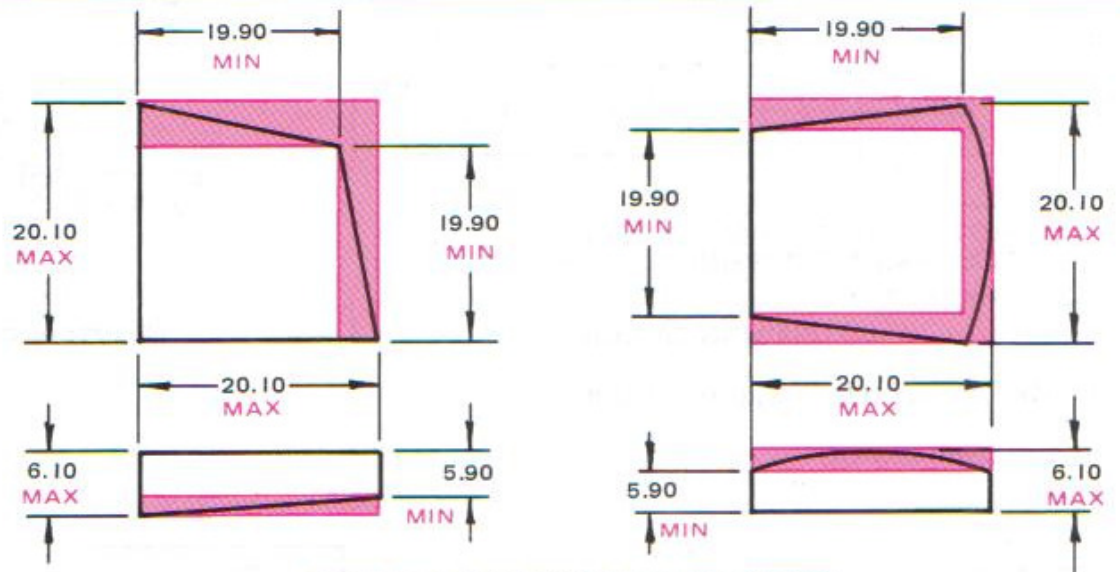


Geometrical Tolerances



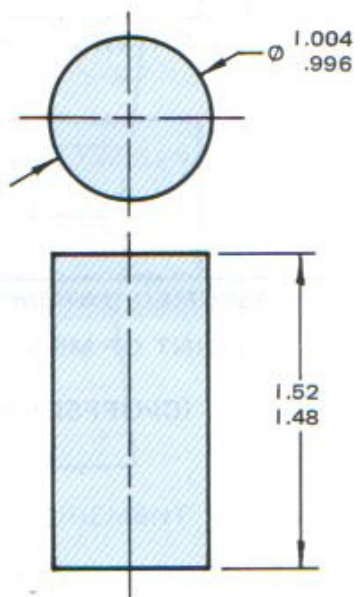


DRAWING CALLOUT

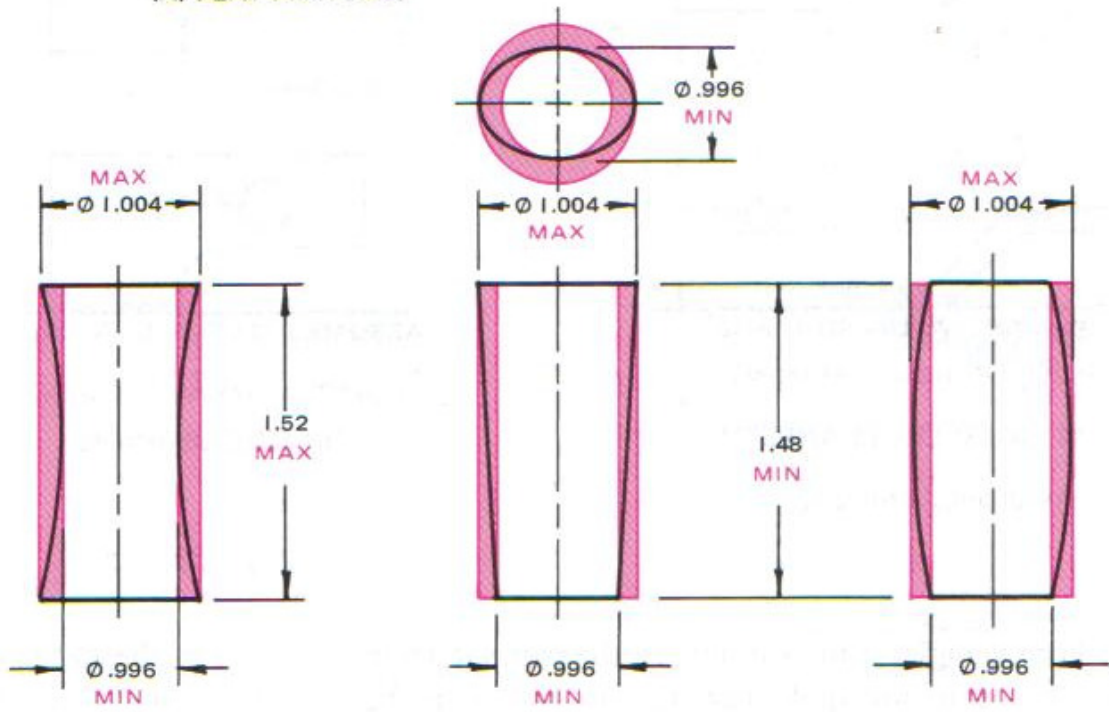


POSSIBLE DEVIATIONS FROM TRUE FORM

(A) FLAT FEATURES



DRAWING CALLOUT



POSSIBLE DEVIATIONS FROM TRUE FORM

(B) CYLINDRICAL FEATURES

What is a Geometrical Tolerance?

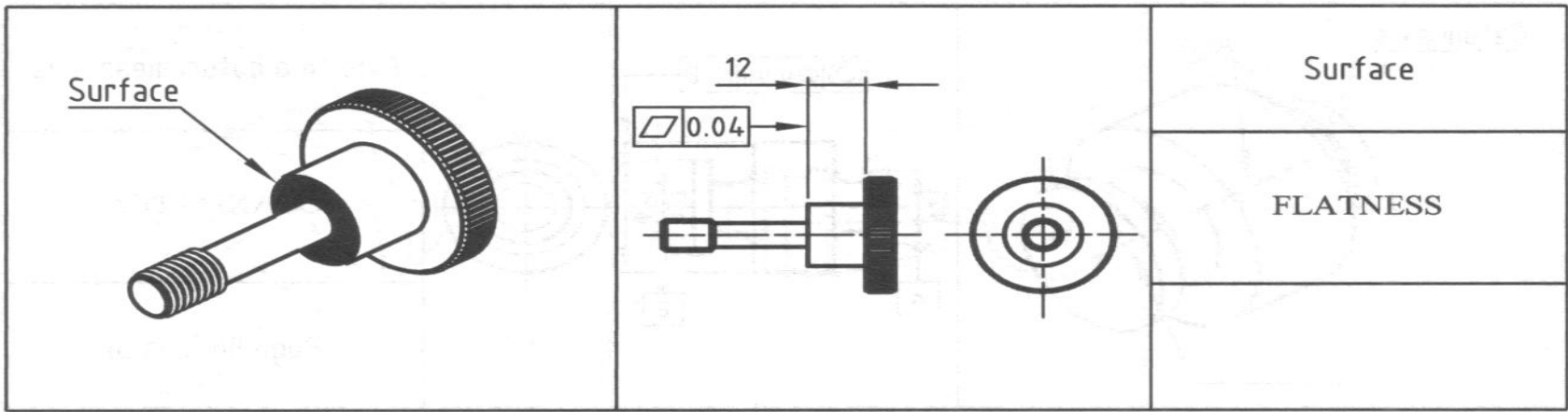
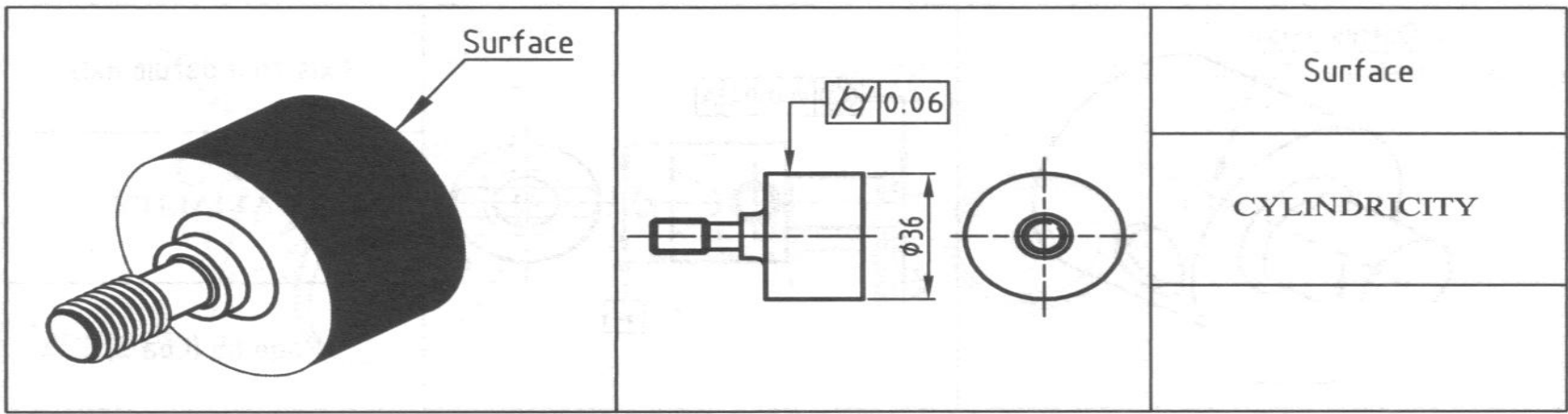
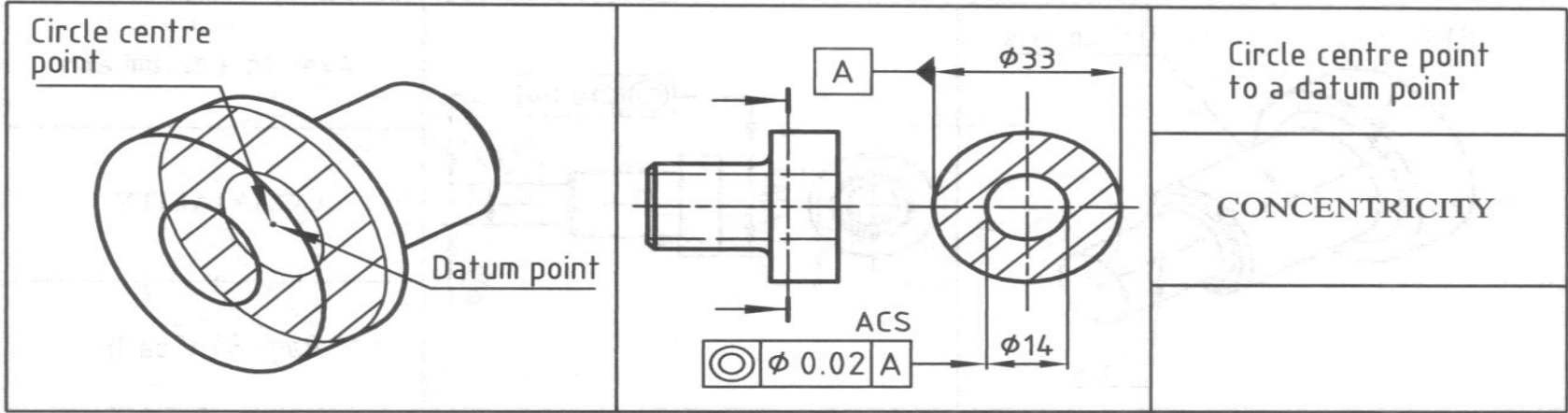
A geometrical tolerance is the maximum allowable variation of form or position of a feature. This is controlled by defining the size and shape of a tolerance zone. The specified part of the feature must be within this tolerance zone.

Geometrical Tolerancing can best be described as a language of symbols placed on technical drawings to adequately define the allowable variation of part geometry.

The current internationally accepted standard in Geometrical Tolerancing is ISO1101: 2004

When to use a Geometrical Tolerance

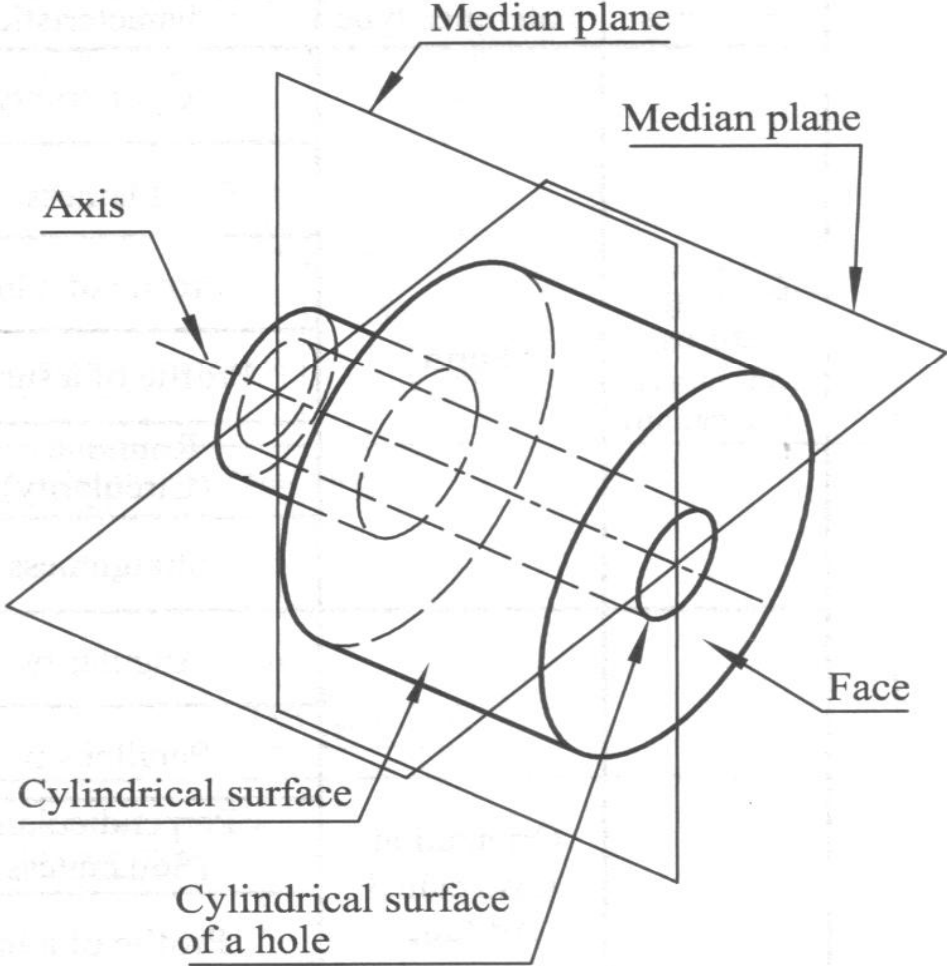
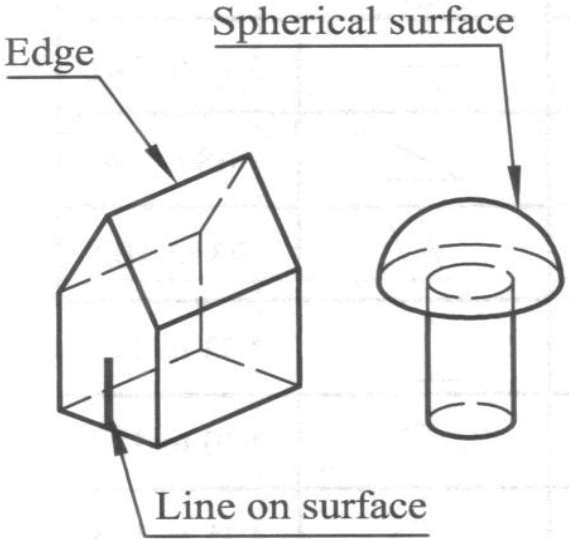
- The size tolerance of a dimension has a certain amount of control over form and attitude but if a better degree of control is required then geometrical tolerances should be used
- Position of a feature is also controlled by geometrical tolerances.
- The use of geometrical tolerances can increase manufacturing costs, so they should only be used when necessary.



SINGLE FEATURES

The following sketches illustrate some of the single features that could be on a component.

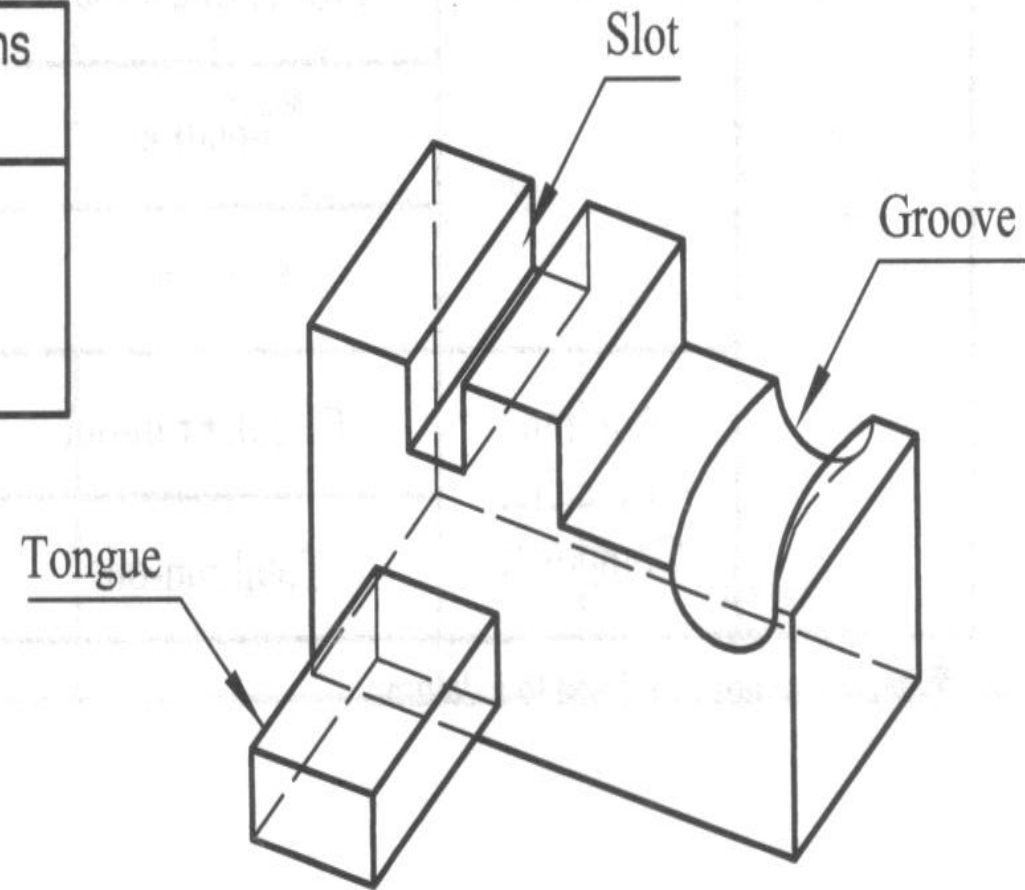
Some examples of single features
An axis
A cylindrical surface
A cylindrical surface of a hole
An edge
A face
A line on a surface
A median plane
A spherical surface



Combinations of Single Features

The following sketch illustrates some combinations of single features that could be on a component.

Some examples of combinations of single features
A groove
A slot
A tongue

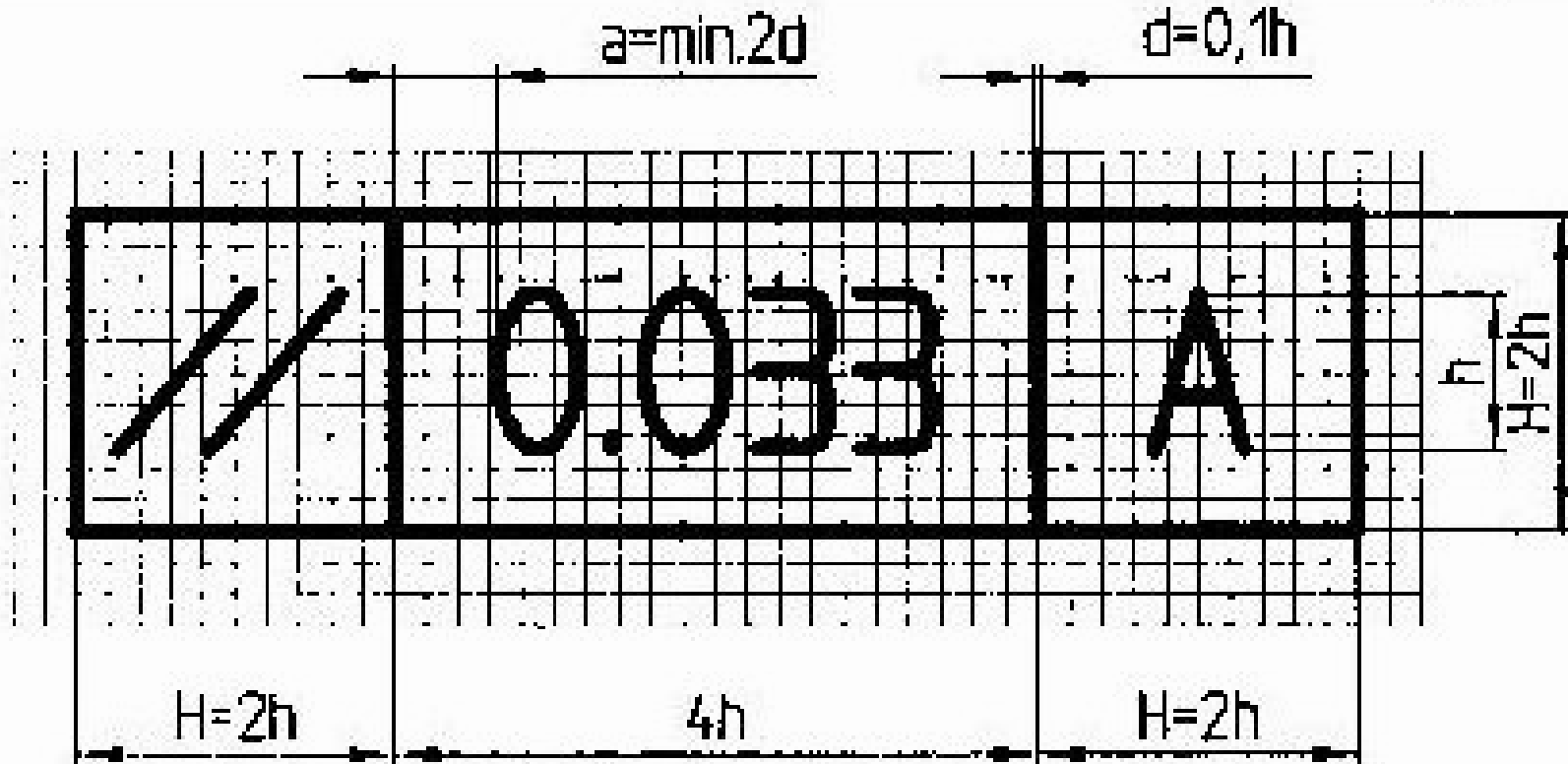


Geometric characteristic symbols

Features	Tolerance type	Characteristic	Symbol
For single features (not related to a datum)	Form	Cylindricity	
		Flatness	
		Profile of a line	
		Profile of a surface	
		Roundness (Circularity)	
		Straightness	
For related features (related to a datum)	Orientation (also called Attitude)	Angularity	
		Parallelism	
		Perpendicularity (Squareness)	
	Location	Concentricity	
		Coaxiality	
		Position	
		Symmetry	
	Run-out (also called Composite)	Circular run-out	
		Total run-out	

SIZE OF FEATURE CONTROL FRAME

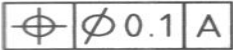
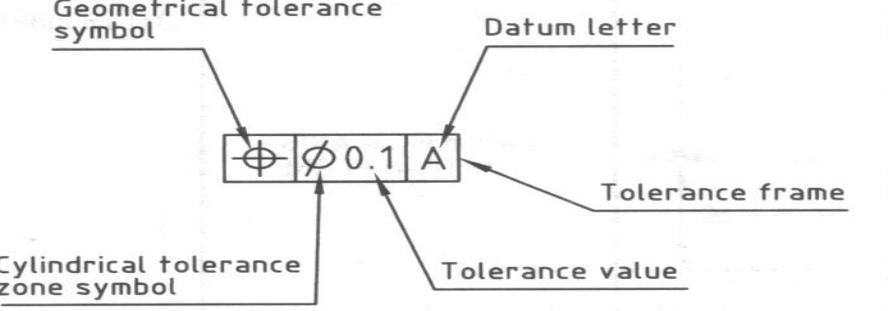
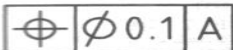
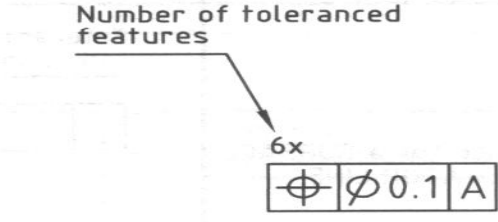
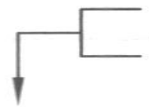
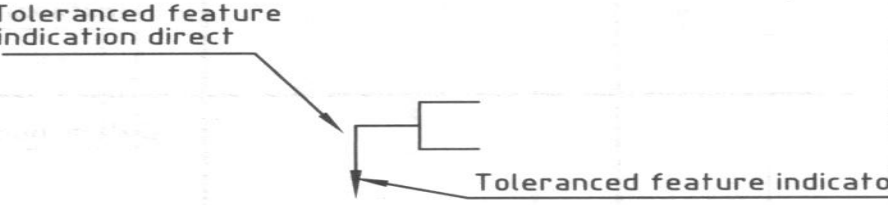
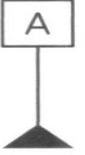
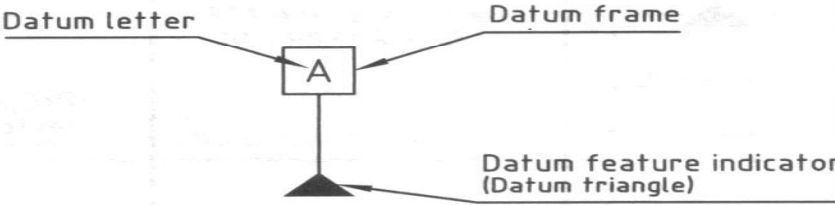
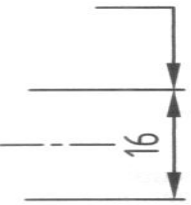
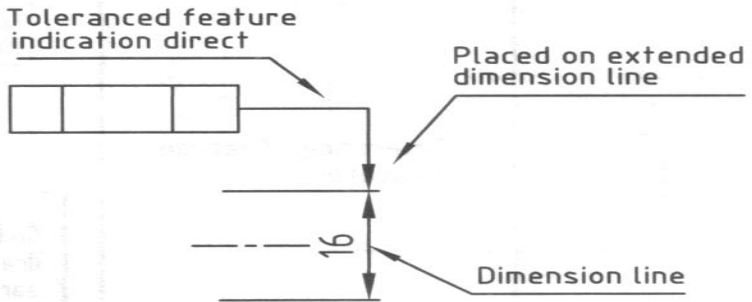
TS 10844



**ŞEKİL VE KONUM ÇEŞİTLERİYLE SEMBOLLERİ
(TS 1304 ISO 1101)**

Eleman Cinsi	Özelliği	Adı	Sembol
TEK ELEMANLAR	ŞEKİL	Doğrusallık	
		Düzlemsellik	
		Dairesellik	
		Silindiriklik	
		Bir çizginin şekli	
		Bir yüzeyin şekli	
BİRBİRLERİYLE İLGİLİ ELEMANLAR	YÖN	Paralellik	
		Diklik	
		Eğiklik (Açısalılık)	
	KONUM	Bir elemanın konumu	
		Ortak merkezlilik, eksenlilik	
		Simetriklik	
	YALPALAMA	Yalpalama	
		Toplam yalpalama	

Symbols for geometrical tolerancing

Symbol on the drawing	Description	Interpretation
	<p>Tolerance frame (also known as a feature control frame)</p>	
<p>6x</p> 	<p>Multiple tolerance frames</p>	<p>Number of tolerated features</p> 
	<p>Toleranced feature indicator</p>	<p>Toleranced feature indication direct</p> 
	<p>Datum indicator</p>	<p>Datum letter</p> <p>Datum frame</p> <p>Datum feature indicator (Datum triangle)</p> 
	<p>Tolerance for an AXIS or a MEDIAN PLANE</p>	<p>Toleranced feature indication direct</p> <p>Placed on extended dimension line</p> <p>Dimension line</p> 

The feature controlled

The feature controlled by the tolerance is indicated by a leader line connecting it to the tolerance frame. At the toleranced feature the leader line terminates in an arrow head which is positioned as follows:

- (1) On the outline of the feature or on an extension of the outline *but not at a dimension line* when the tolerance refers to the line itself or to the surface represented by the line (Fig. 4).
- (2) On the outline or on a projection line of the feature *at a dimension line* when the tolerance refers only to the axis or median plane of the feature so dimensioned (Figs. 5 and 6).
- (3) On the axis or median plane when the tolerance refers to the common axis or median plane of all features lying on that axis or median plane (Figs. 7, 8 and 9).

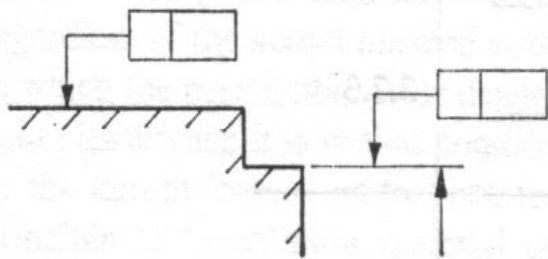


Fig. 4

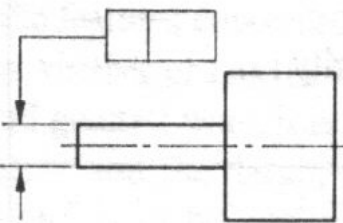


Fig. 5

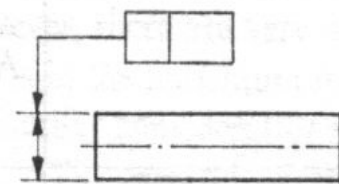


Fig. 6

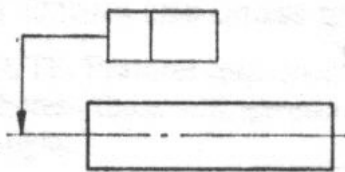


Fig. 7

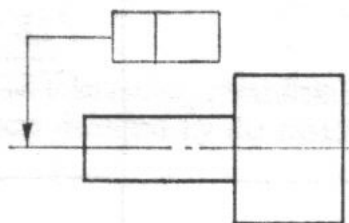


Fig. 8

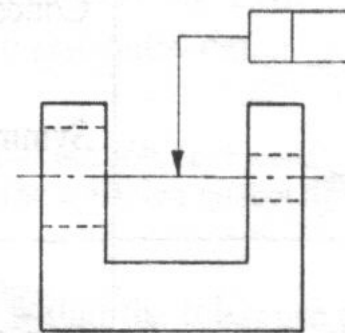


Fig. 9

Tolerances applicable to restricted lengths of features

If a tolerance is applied only to a particular part of a feature, that part is indicated as in Fig. 25.

If the tolerance value over the whole of the considered length or surface is to be qualified by a smaller tolerance on any specified shorter length lying anywhere within it, this is expressed as in Fig. 26 where the tolerance value 0.05 applies to any length 100. This convention used for a feature which is a surface means that the tolerance value is applicable to all lines of the specified length lying in any position and in any direction on the surface.

If the tolerance is only specified in the form of a tolerance value applicable to a specific length as in Fig. 27, an accumulation of tolerance over the whole length or surface is permitted.

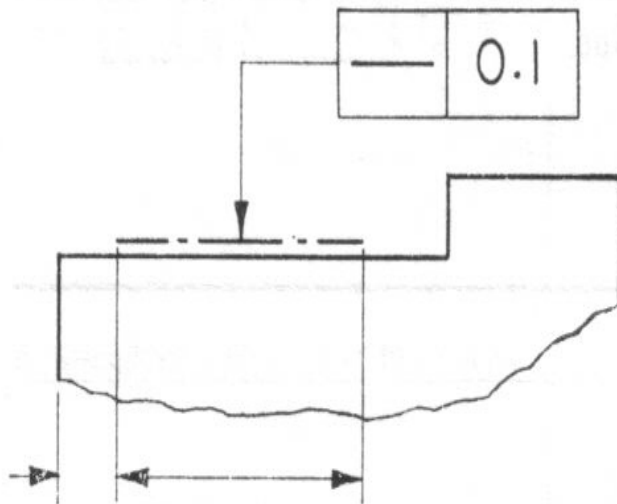


Fig. 25

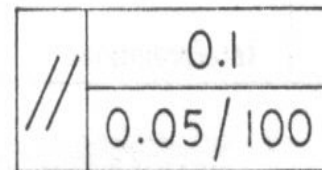


Fig. 26

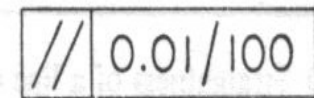
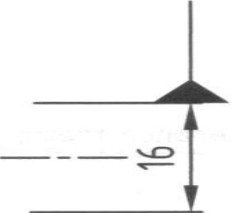
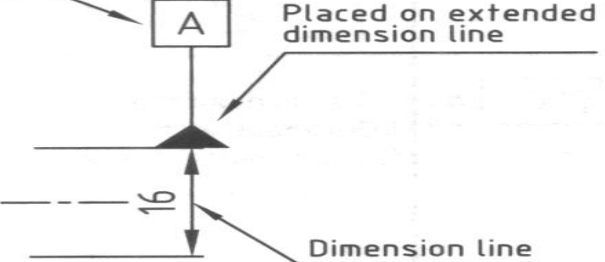
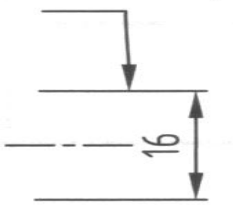
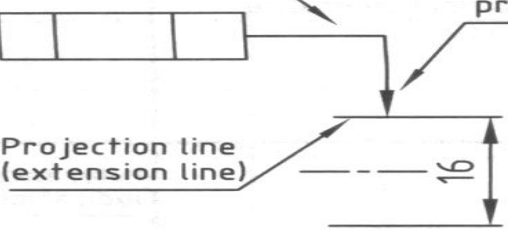
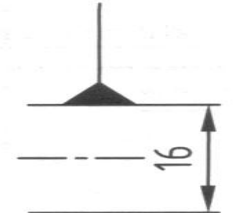
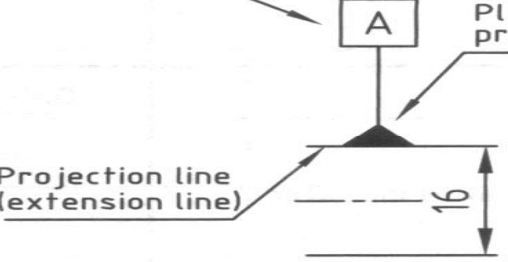




Fig. 27

Symbols for geometrical tolerancing

Symbol on the drawing	Description	Interpretation
	Datum is an AXIS or MEDIAN PLANE	<p>Datum indicator</p>  <p>Placed on extended dimension line</p> <p>Dimension line</p>
	Tolerance for a SURFACE or GENERATOR LINE	<p>Toleranced feature indication direct</p>  <p>Placed on projection line</p> <p>Projection line (extension line)</p>
	Datum is a SURFACE or GENERATOR LINE	<p>Datum indicator</p>  <p>Placed on projection line</p> <p>Projection line (extension line)</p>
	Toleranced feature indicator	<p>Toleranced feature indication by letter</p>  <p>Toleranced feature indicator</p> <p><i>* Obsolete *</i> Shown for reference to drawings prepared to earlier standards.</p>

Datum features

The datum feature(s) is (are) indicated by a leader line from the tolerance frame terminating in a solid triangle the base of which lies as follows:

- (1) On the outline of the feature or an extension of the outline (but not at a dimension line), when the datum feature is the line or surface itself (Fig. 10).
- (2) On the projection line at the dimension line or on the axis when the datum feature is the axis or median plane of the whole component (Figs. 12 and 13) or of the part so dimensioned (Fig. 11).
- (3) On the common axis or median plane of two or more features (Figs. 14 and 15).

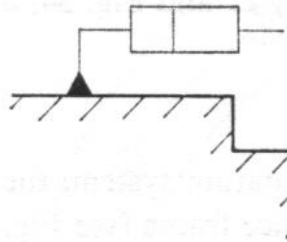


Fig. 10

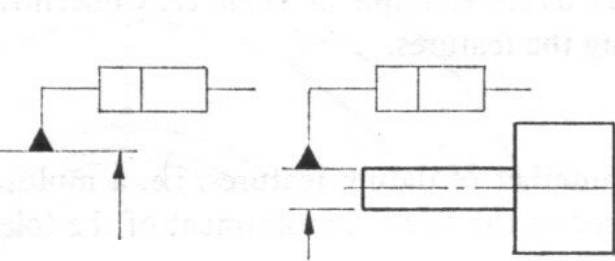


Fig. 11

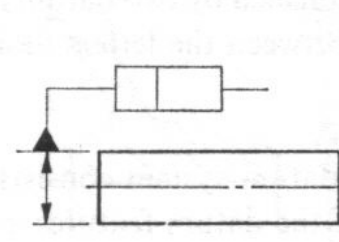


Fig. 12

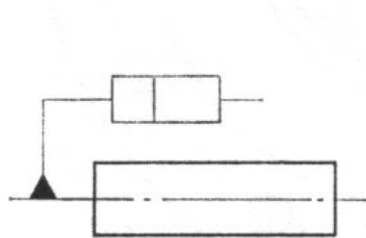


Fig. 13

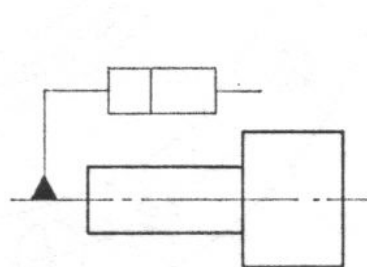


Fig. 14

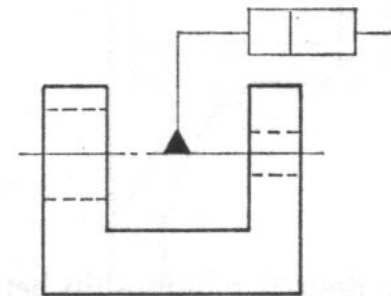
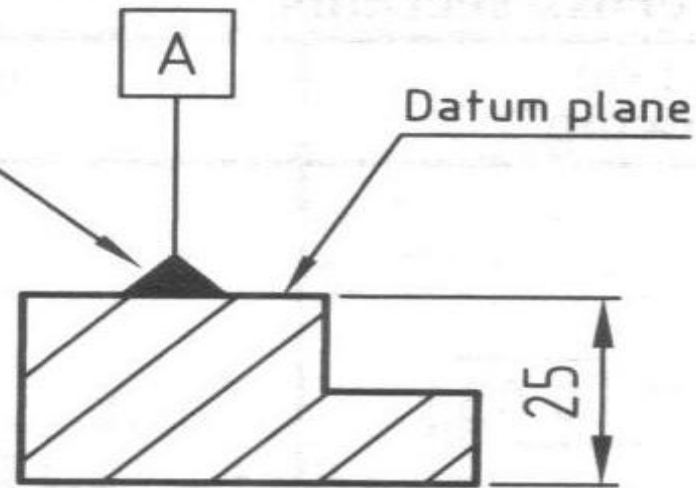


Fig. 15

Interpretation

The datum triangle is placed on the outline of the feature



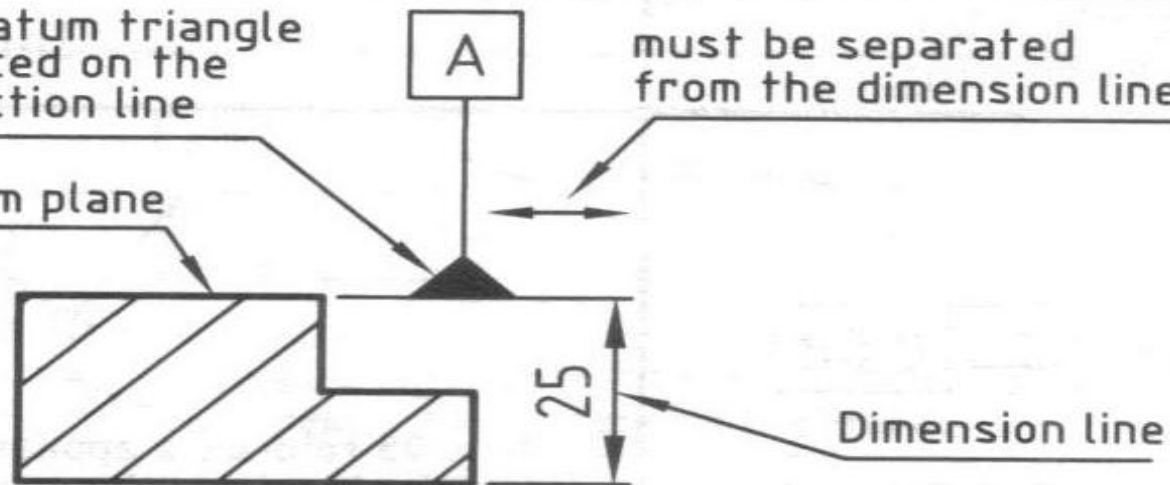
datum is a plane or line

Interpretation

The datum triangle is placed on the projection line

must be separated from the dimension line

Datum plane



If the tolerance frame cannot be connected in a clear and simple manner with the datum feature, a capital letter* in a frame is connected to the datum feature

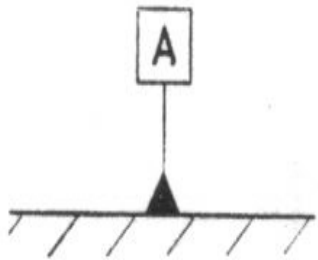


Fig. 16

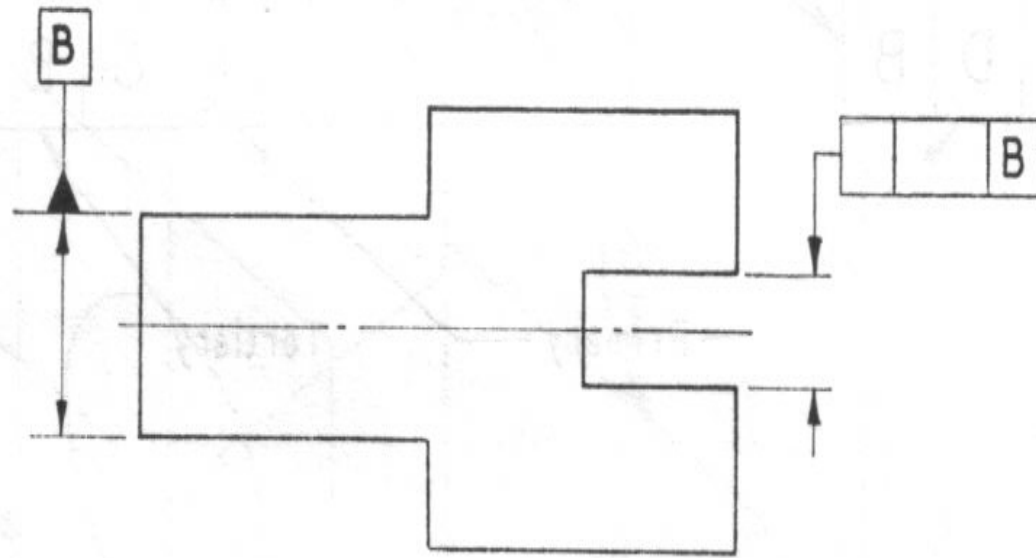
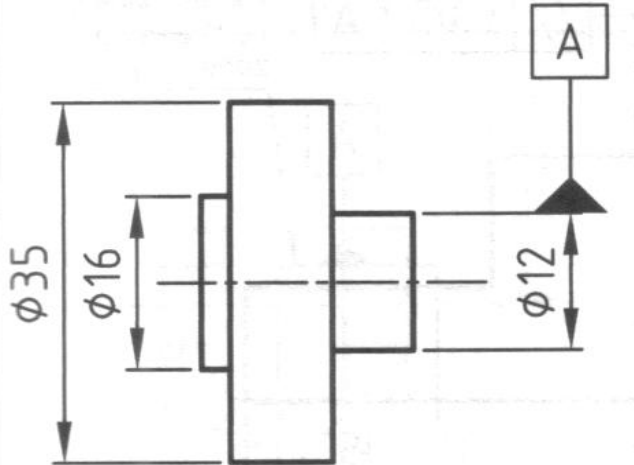
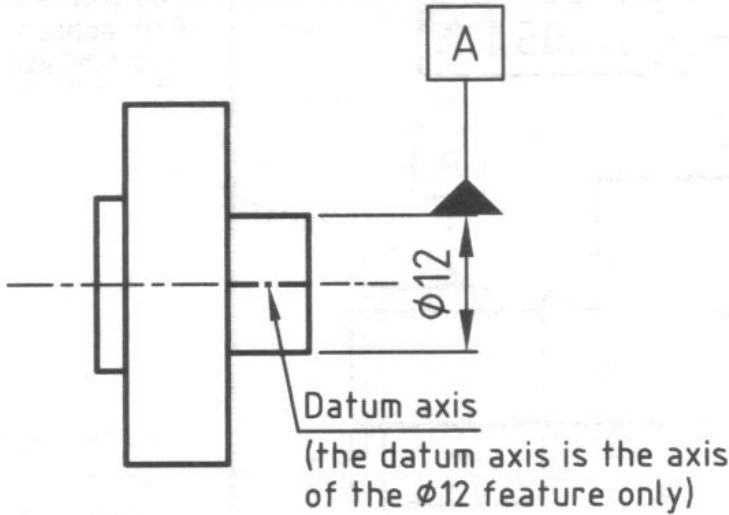
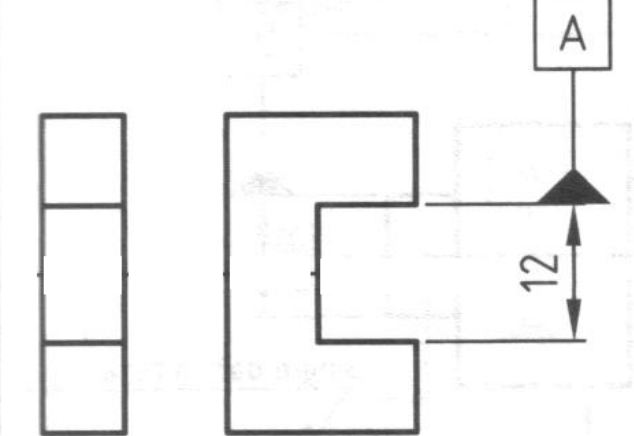
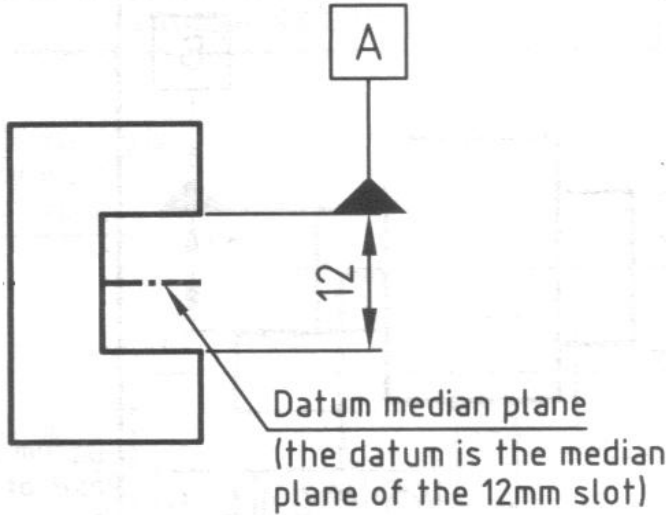


Fig. 17

When the datum is an axis

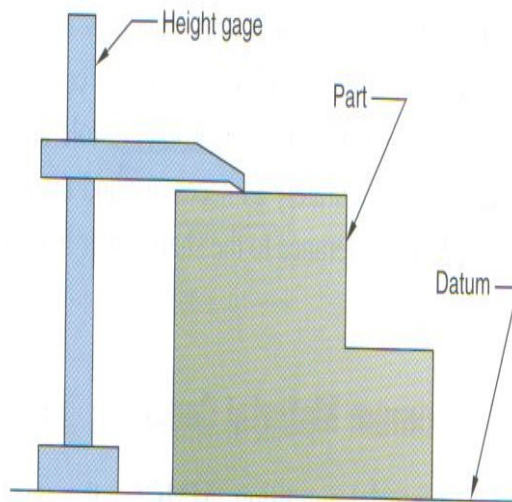
Symbol on the drawing	Interpretation
 <p>A technical drawing of a shaft with three diameters: $\phi 35$, $\phi 16$, and $\phi 12$. A datum symbol 'A' is shown with a feature control frame pointing to the $\phi 12$ diameter. The datum is the axis of this feature.</p>	 <p>The interpretation shows the shaft with a dashed line representing the datum axis, which is the axis of the $\phi 12$ feature. A feature control frame 'A' is shown with a feature control symbol pointing to the $\phi 12$ diameter. A note states: "Datum axis (the datum axis is the axis of the $\phi 12$ feature only)".</p>

When the datum is a median plane

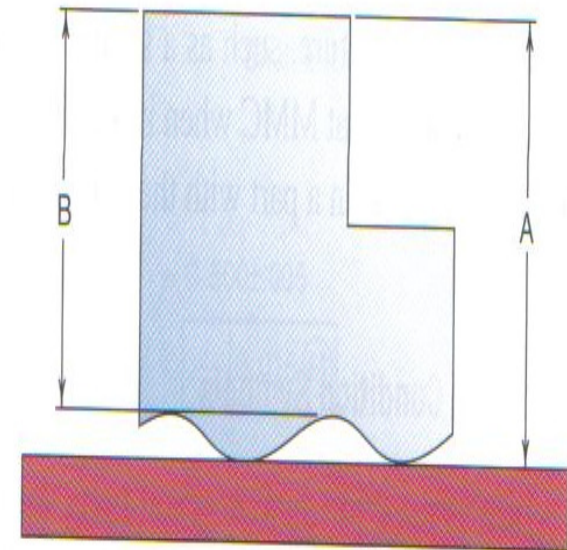
Symbol on the drawing	Interpretation
 <p>A technical drawing of a stepped shaft with a 12mm wide slot. A datum symbol 'A' is shown with a feature control frame pointing to the slot. The datum is the median plane of the slot.</p>	 <p>The interpretation shows the shaft with a dashed line representing the datum median plane, which is the median plane of the 12mm slot. A feature control frame 'A' is shown with a feature control symbol pointing to the slot. A note states: "Datum median plane (the datum is the median plane of the 12mm slot)".</p>

Datums and Datum Features

A **datum** is a starting place for a dimension. A datum may be a perfect plane, a center line, or a point. Datums are perfect, and they are not real. Examples are the center line of a shaft or the point at the center of a sphere. These are theoretical positions that either can be represented with inspection tools or can be derived. For example, a center line is represented by the center of an inspection pin or gage or by the center of an inspection spindle. A center line is derived by measuring to the edge of a gage pin and then adding half the diameter of the pin to locate the center of the gage pin from an edge or another feature. For a hole, the measurement is *not* to the edge of the feature hole but to the largest-gage pin that will fit into the hole.

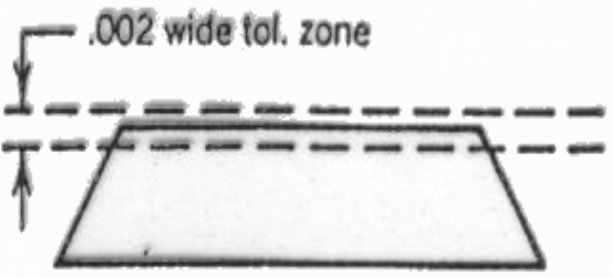
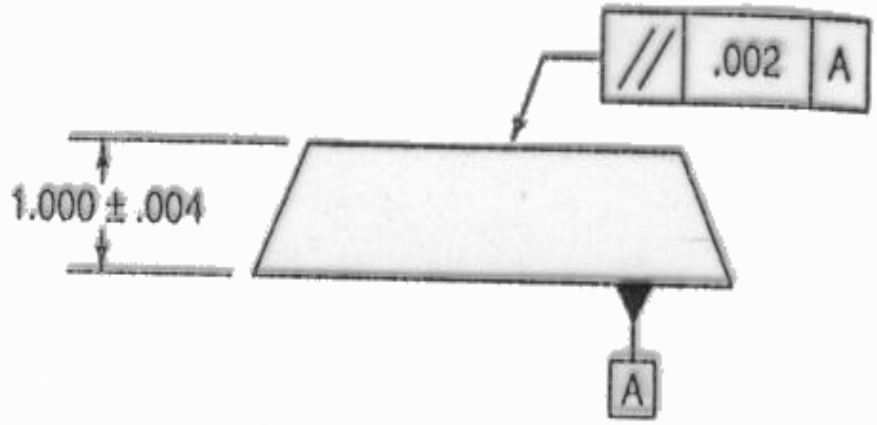


3/16/20 The bottom surface of the part is the datum feature, surface plate is the datum.

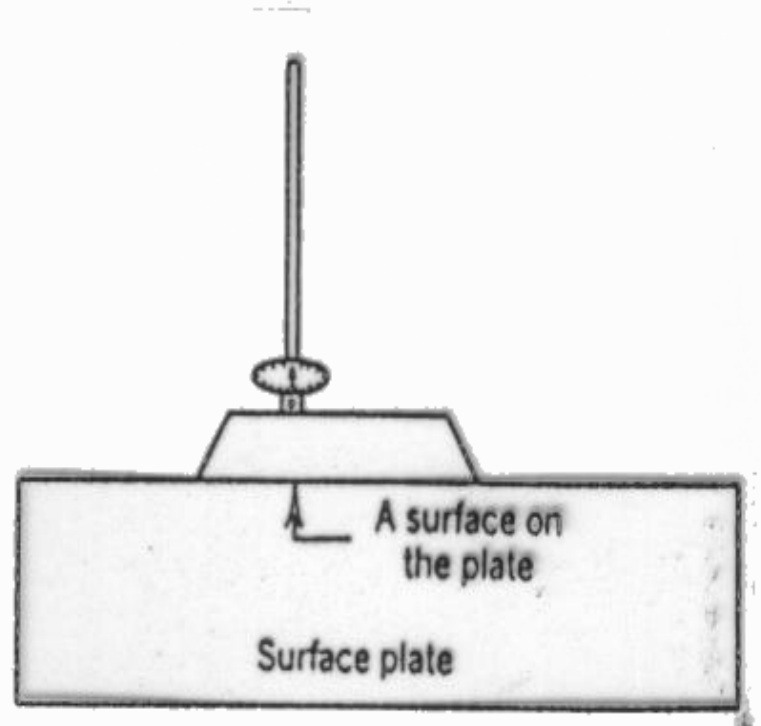


Dr. Murat Sönmez

Parallelism callout.

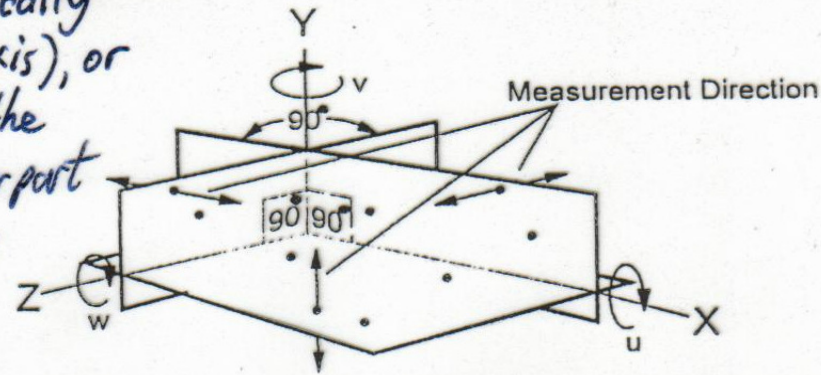


Parallelism tolerance zone.

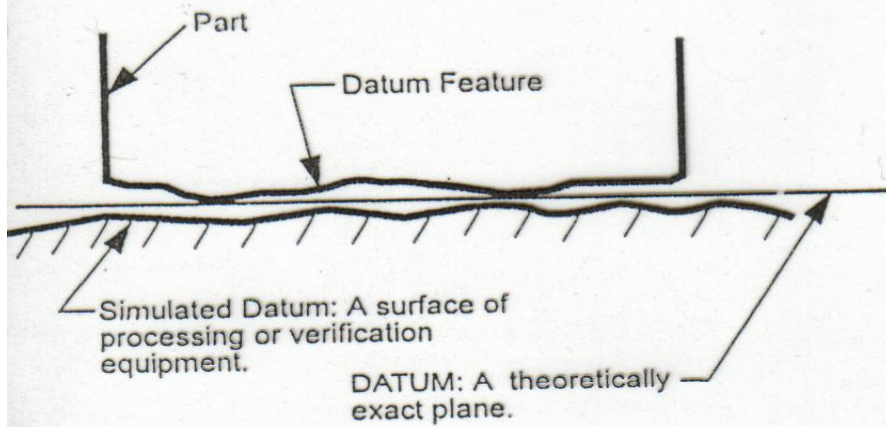


Datum is located.

Datum is a theoretically exact point, line (axis), or plane derived from the true geometric counterpart of a specified datum feature.



Datum Reference Framework. Three Mutually Perpendicular Planes.



Datum

Theoretically perfect points, lines, or planes

Simulated Datum (Datum Simulators)

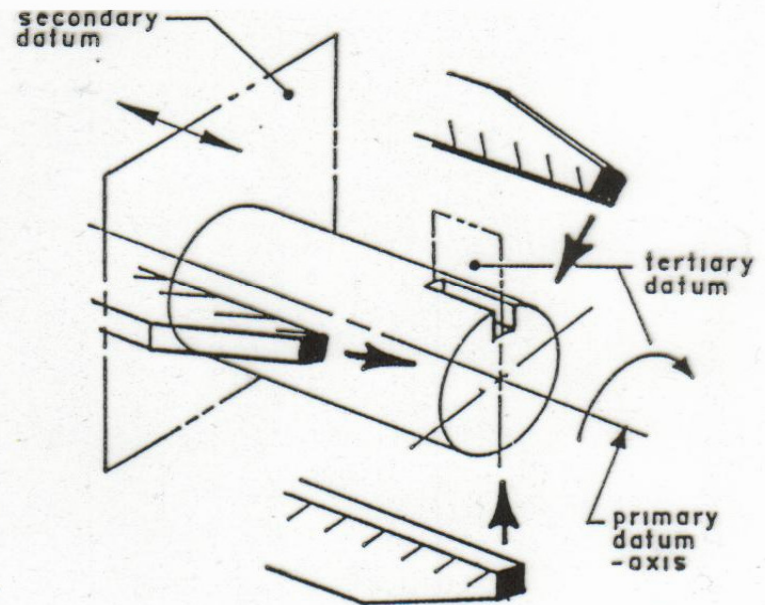
Surfaces and axes of processing or inspection equipment

Datum Feature

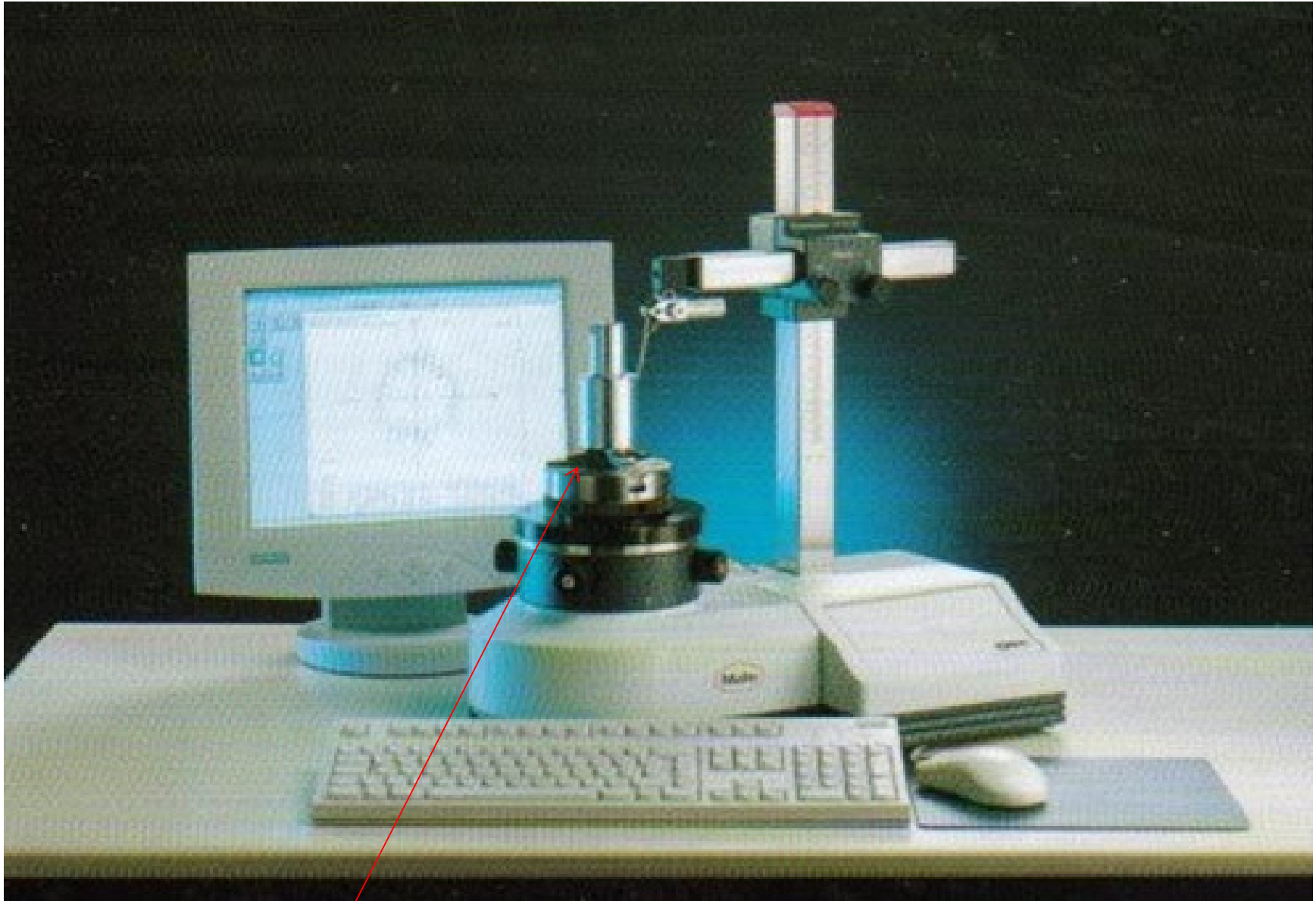
Actual part feature surfaces

Temporary Datum

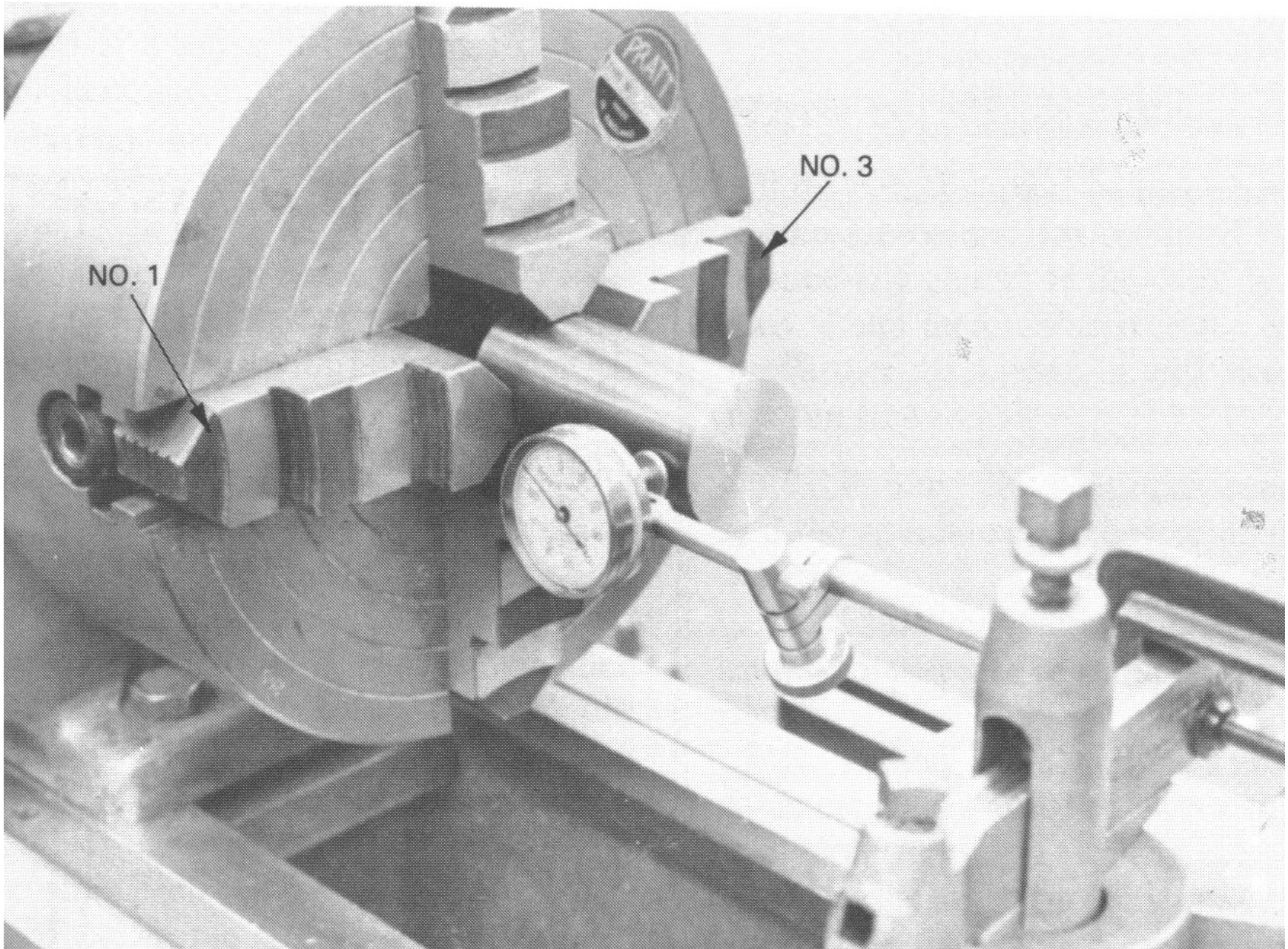
Introduced for processing or inspection purposes (may be removed)



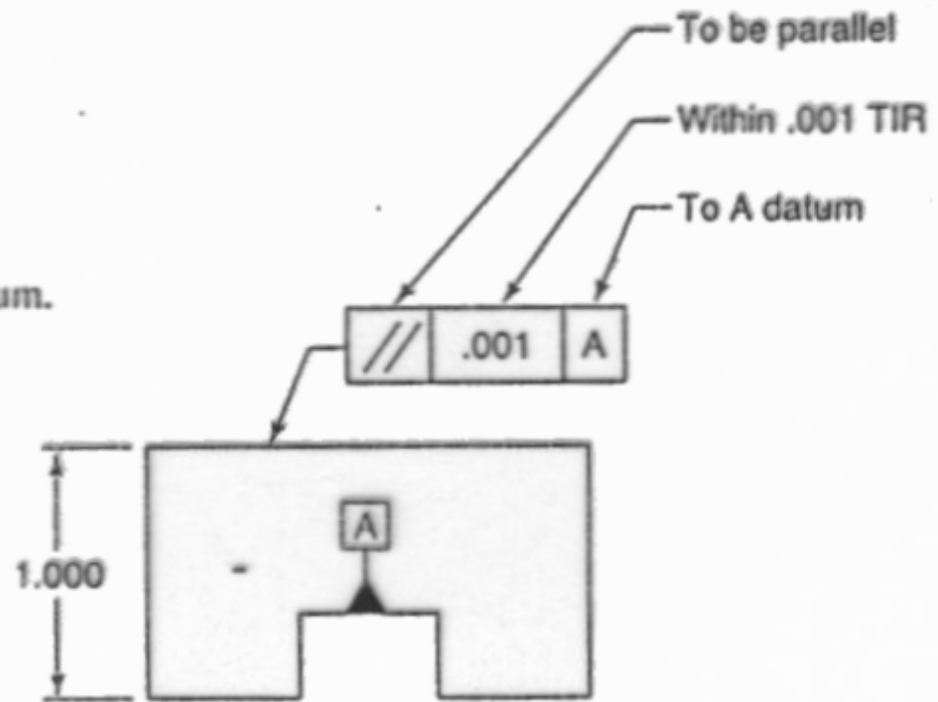




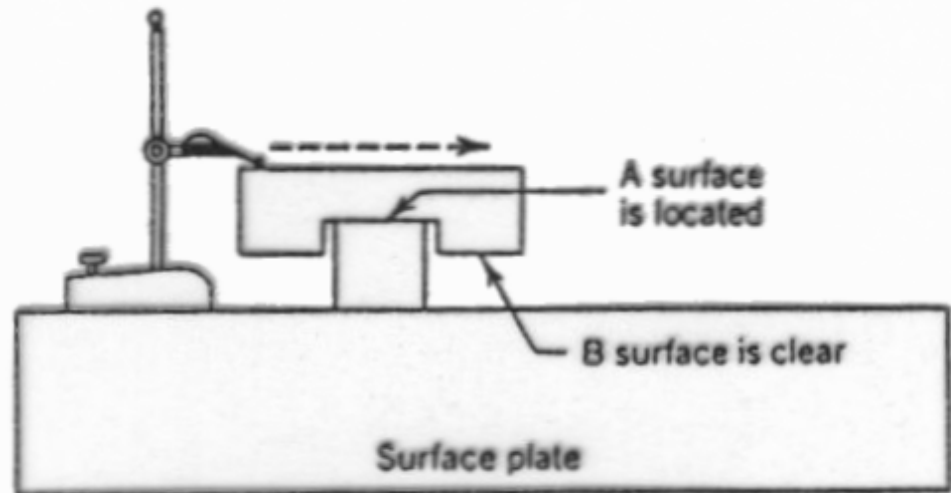
Datum simulator (jaws of the chuck)

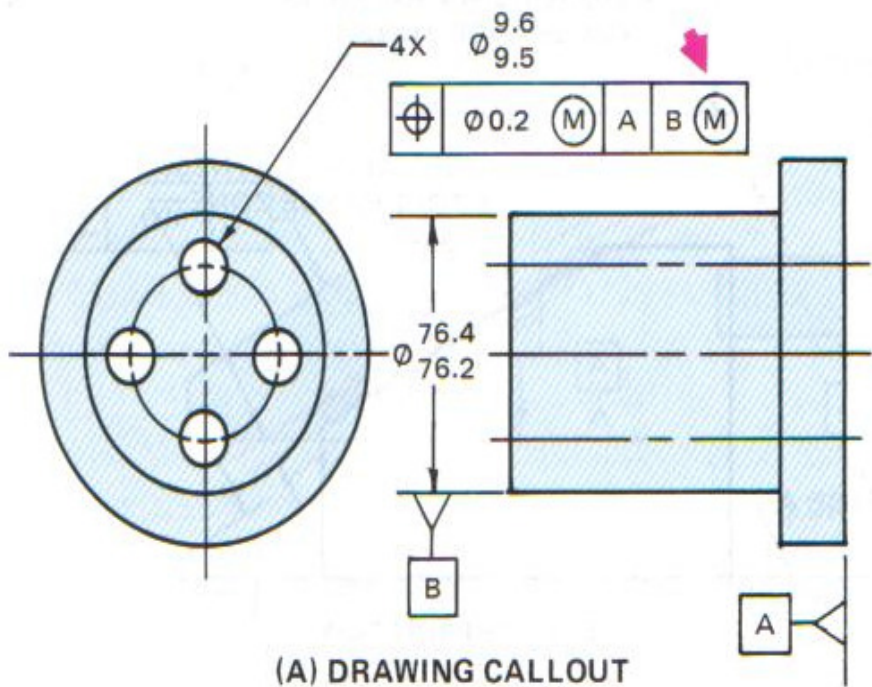


Parallelism to a hidden datum.



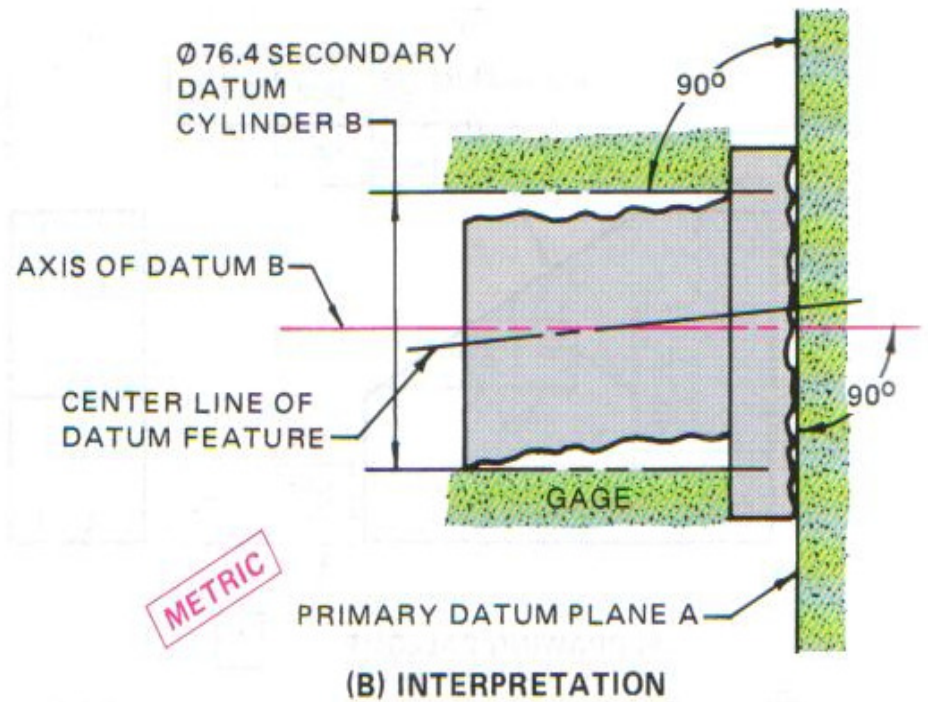
Fixed parallel locates the hidden datum.



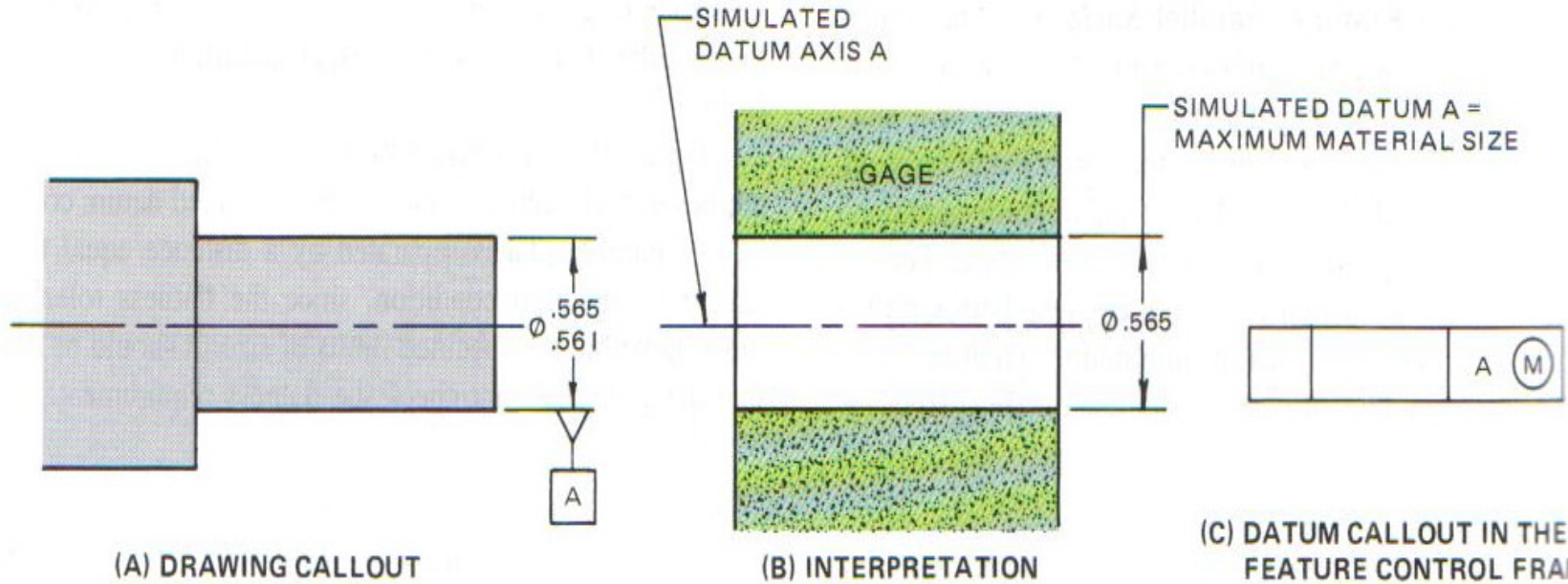


(A) DRAWING CALLOUT

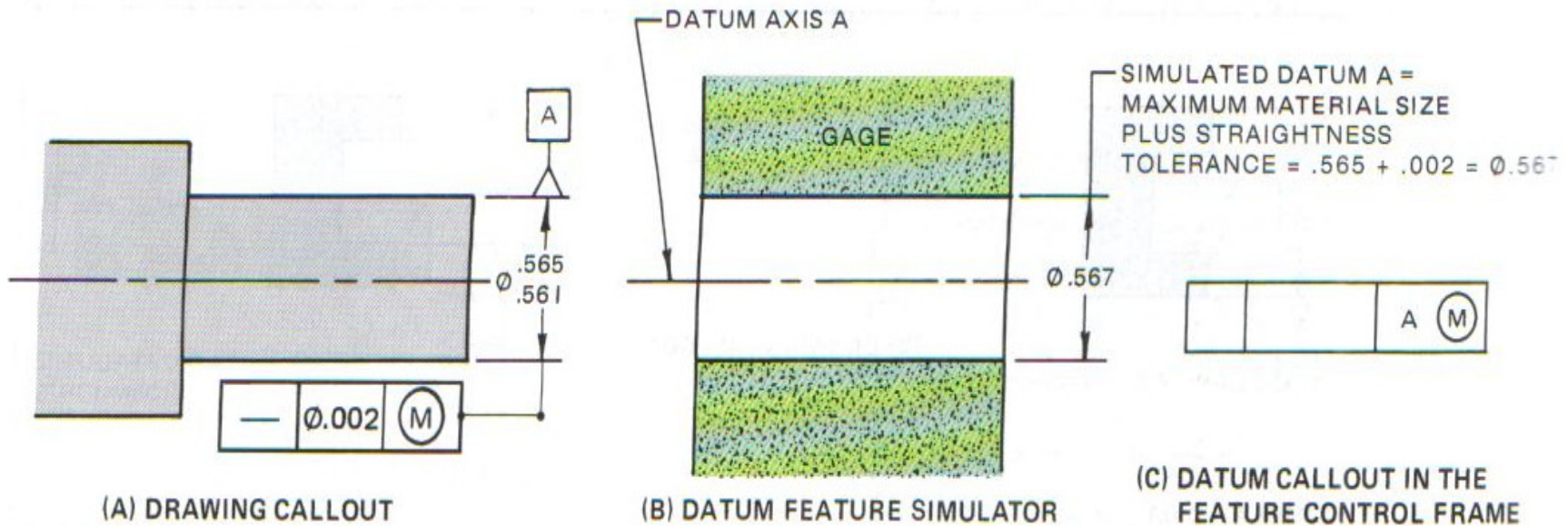
Cylindrical feature as secondary datum.



(B) INTERPRETATION

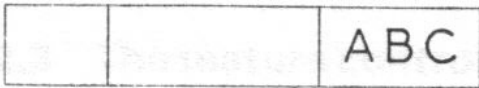


External primary datum without form tolerances—MMC.

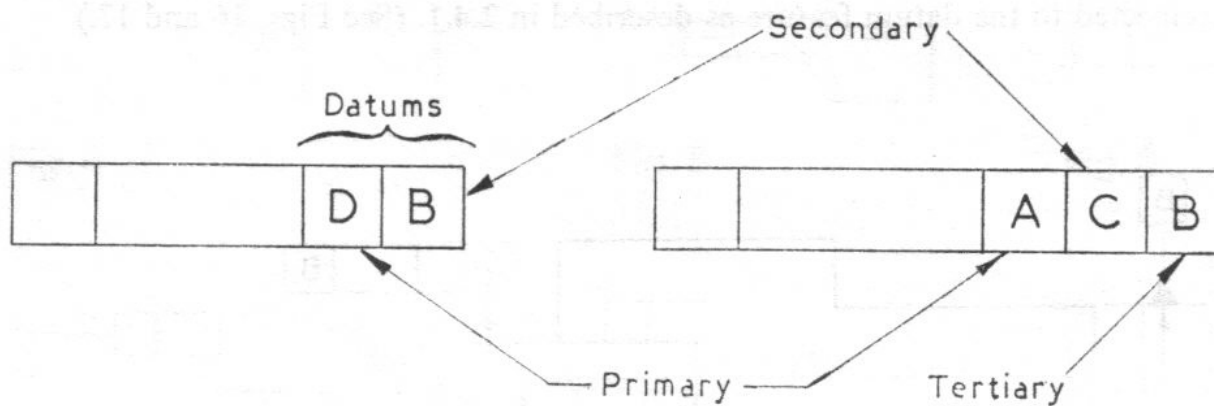


External primary datum with straightness tolerance—MMC.

Where a datum system consists of a number of datum features, i.e. a multiple datum system, the reference letters of the datum features are placed in the third compartment of the tolerance frame



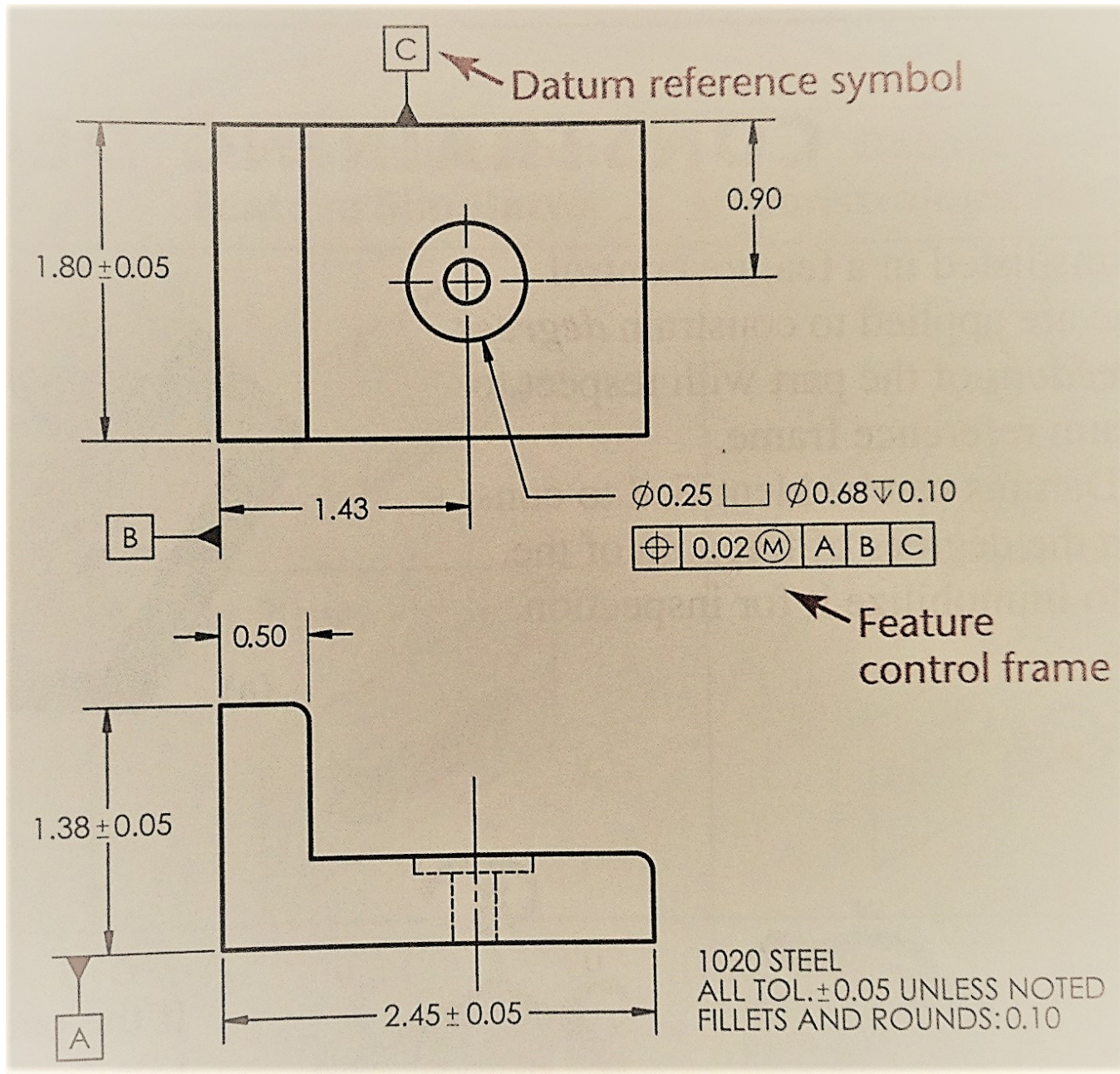
Where the desired relationship between the actual component and the datum system established by the multiple datums has to be obtained by the application of the datum features in a particular order, the designating letters should be quoted, in the needed order from left to right in the third and subsequent compartments of the tolerance frame

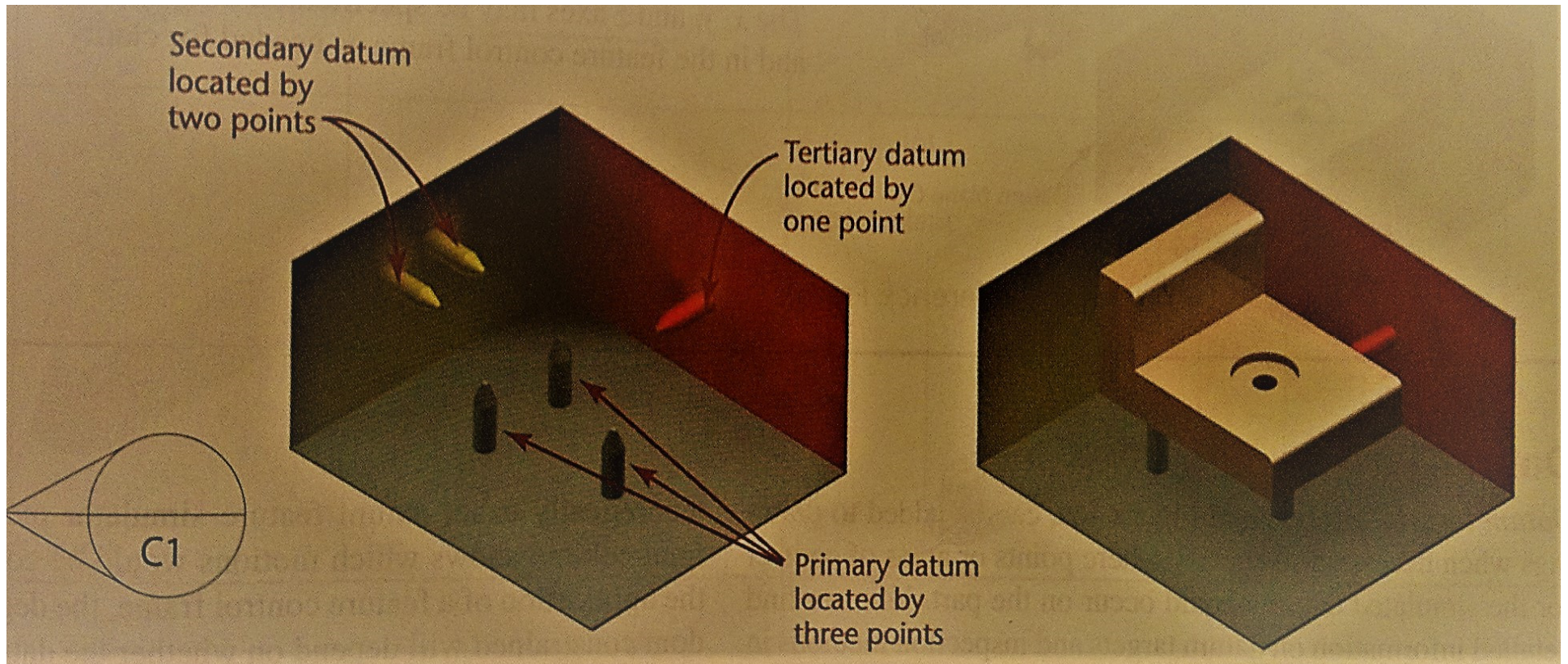


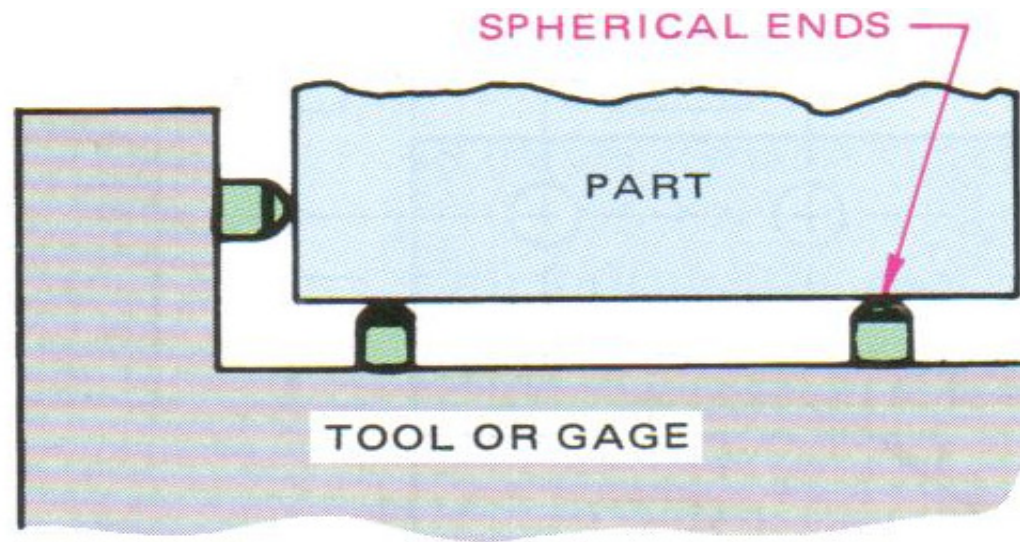
DATUM TARGETS

The full feature surface was used to establish a datum for the features so far designated as datum features. This may not always be practical for these three reasons:

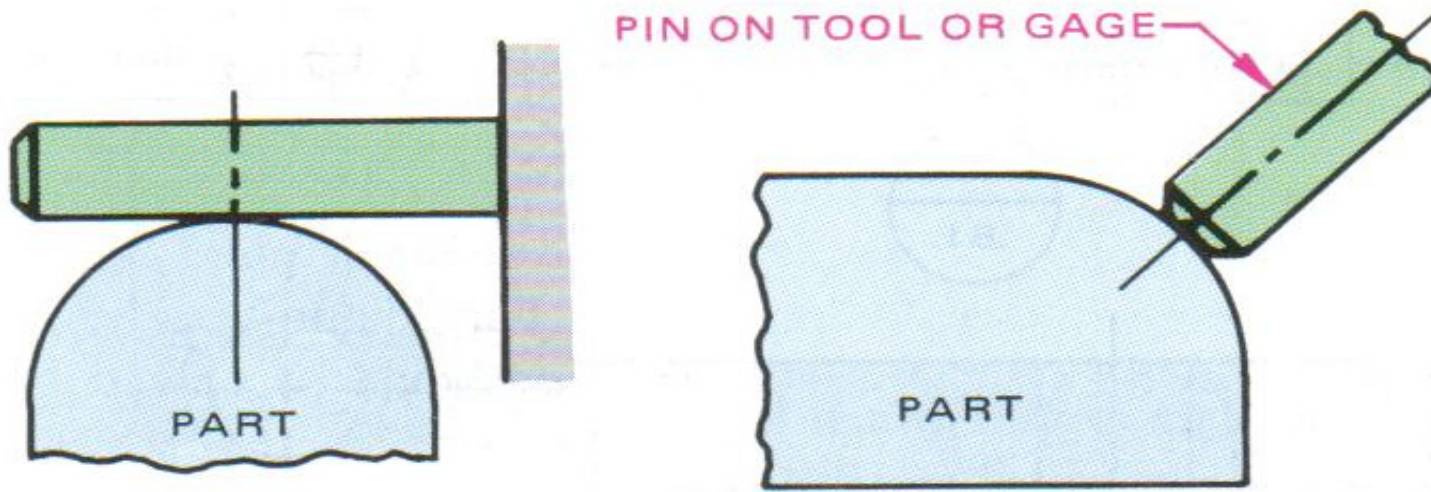
1. The surface of a feature may be so large that a gage designed to make contact with the full surface may be too expensive or too cumbersome to use.
2. Functional requirements of the part may necessitate the use of only a portion of a surface as a datum feature, for example, the portion that contacts a mating part in assembly.
3. A surface selected as a datum feature may not be sufficiently true, and a flat datum feature may rock when placed on a datum plane, so that accurate and repeatable measurements from the surface would not be possible. This is particularly so for surfaces of castings, forgings, weldments, and some sheet-metal and formed parts.







(A)



(B)

(C)

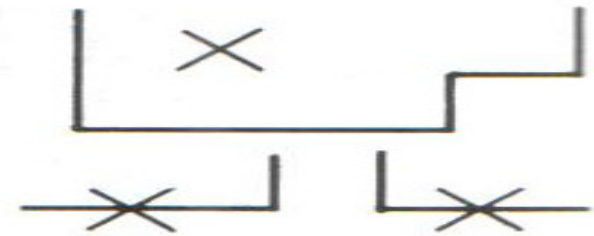
Location of part on datum target points.



Datum target symbol.

TARGET POINT

A CROSS ON THE SURFACE
OR
DATUM POINT LOCATED
ON ADJACENT VIEWS

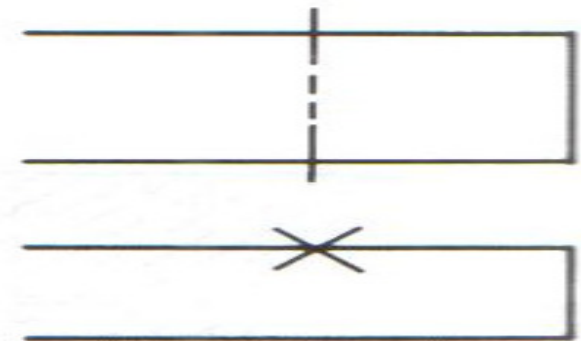


TARGET LINE

A PHANTOM LINE ON THE
SURFACE

AND/OR

A CROSS MAY BE ADDED ON
THE PROFILE (WHERE THE
LINE APPEARS AS A POINT
ON THE SURFACE)

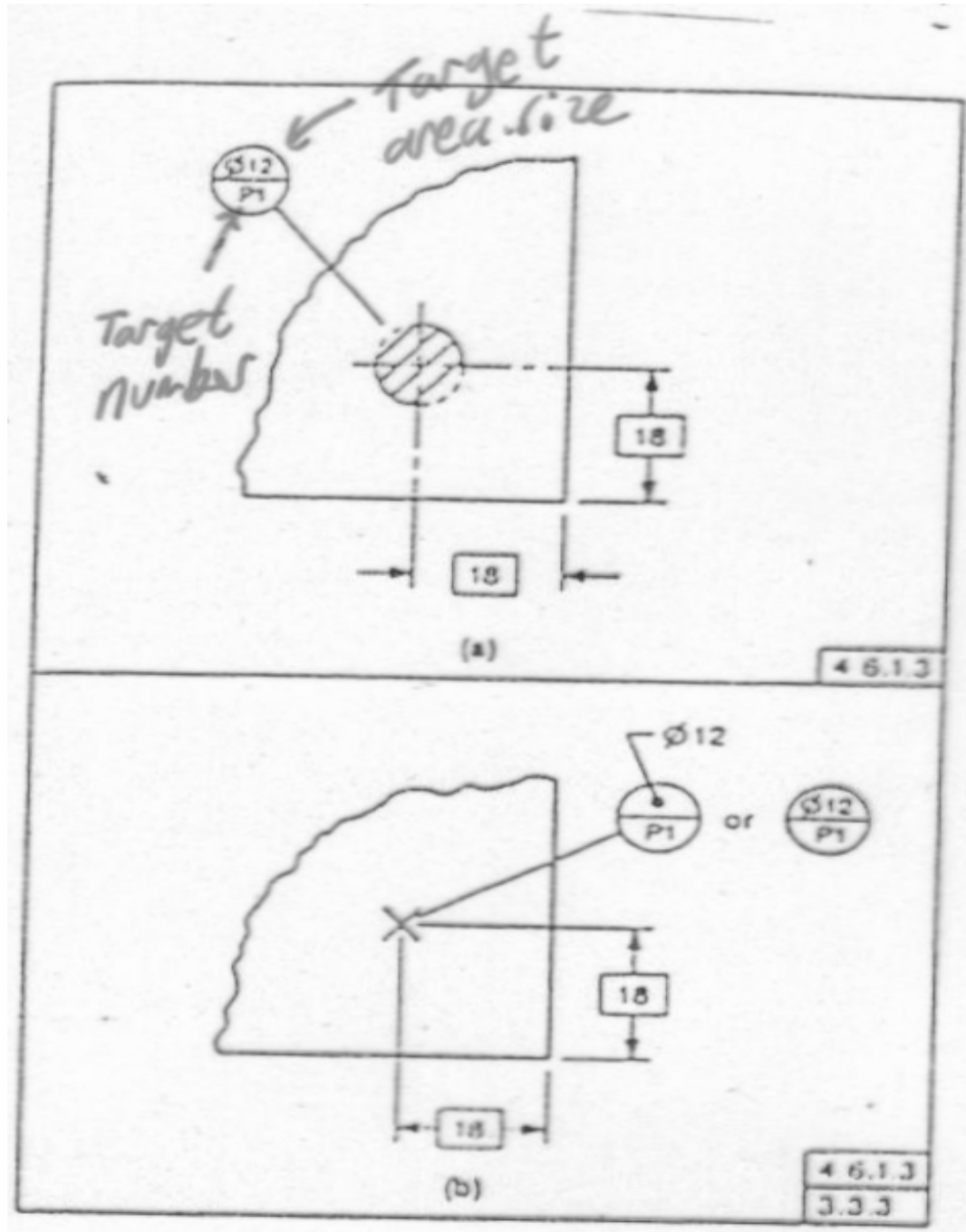


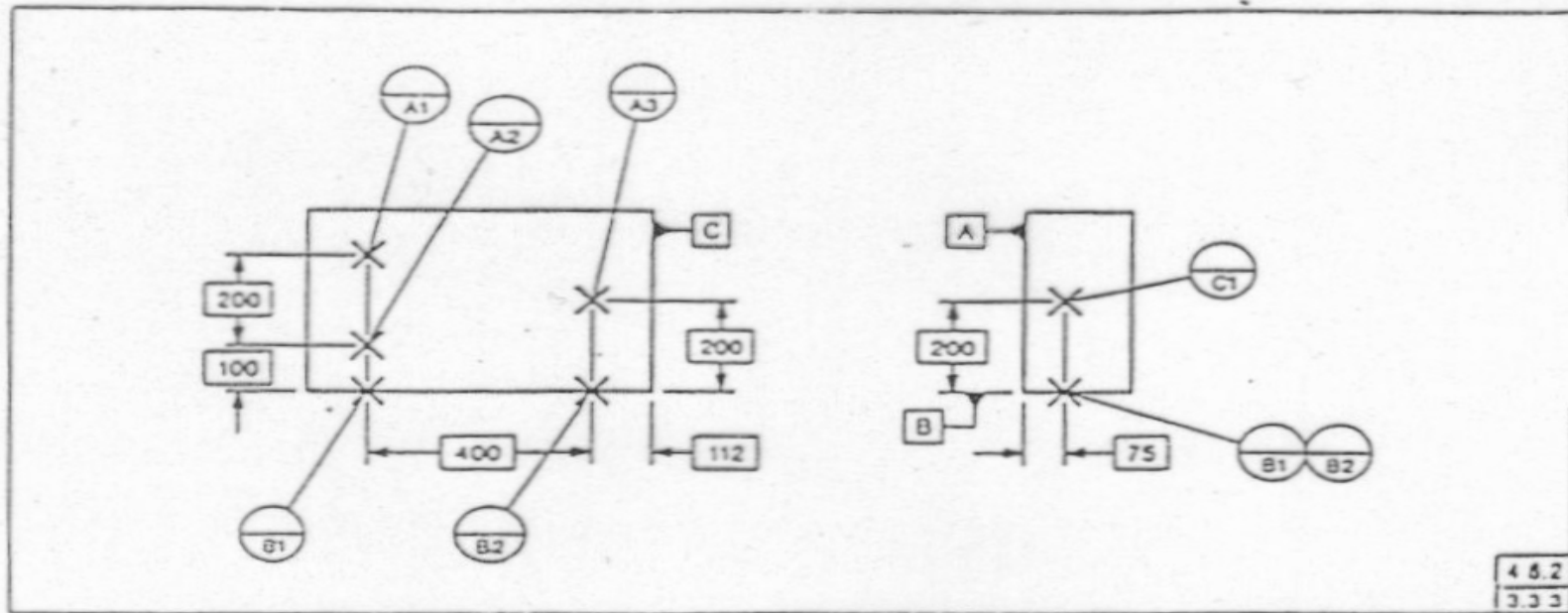
TARGET AREA

A SECTION-LINED AREA ON
THE SURFACE ENCLOSED BY
PHANTOM LINES

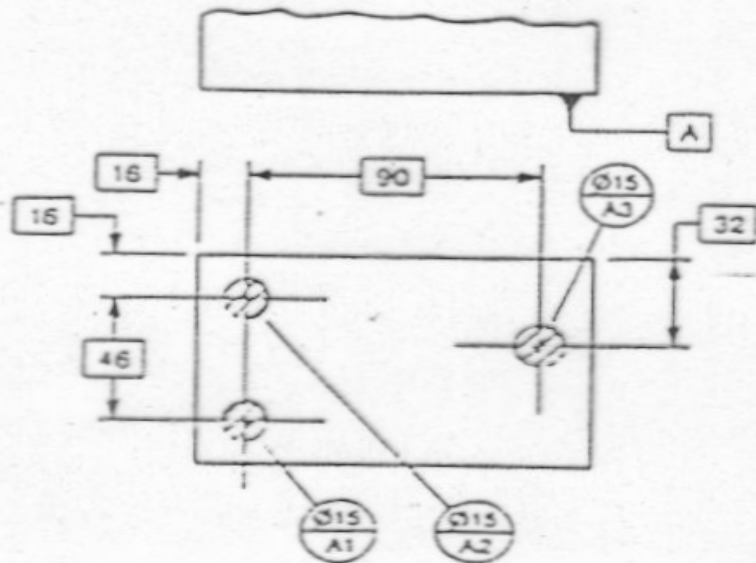


Symbol for a datum target point.

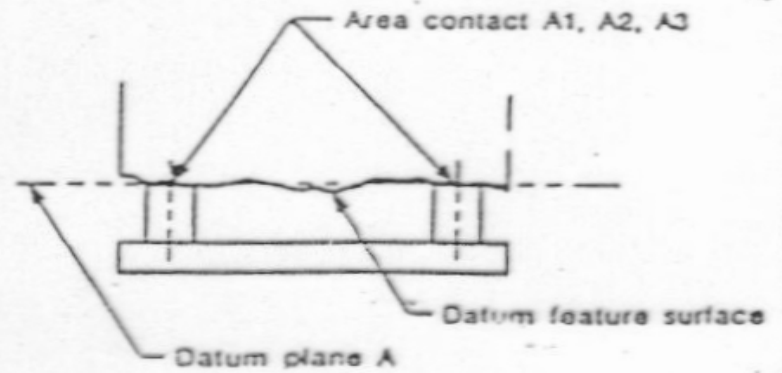




THIS ON THE DRAWING

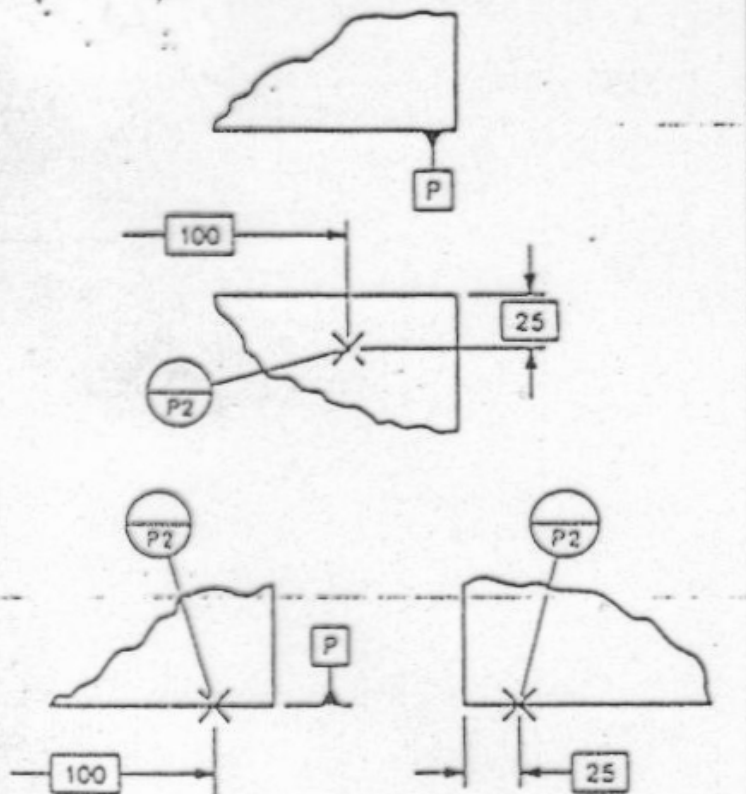


MEANS THIS



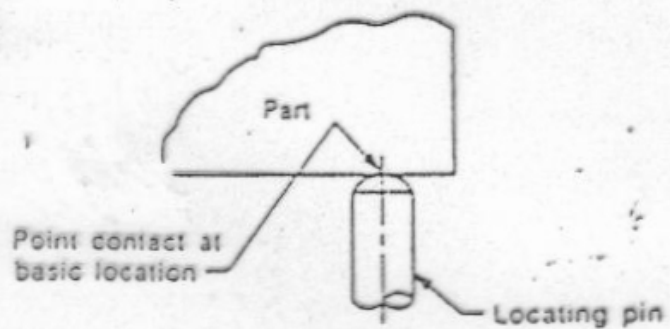
4.6.3

THIS ON THE DRAWING

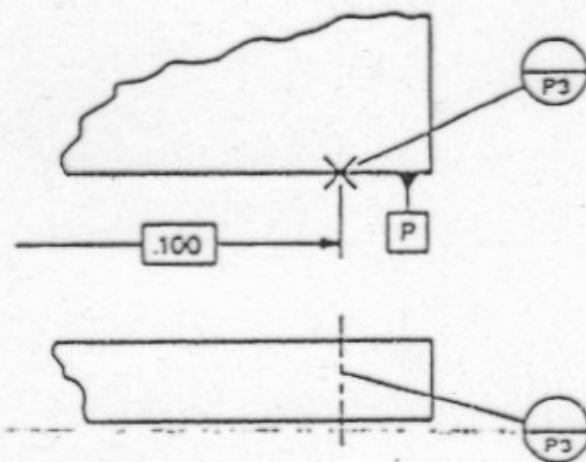


4.6.1.1

MEANS THIS

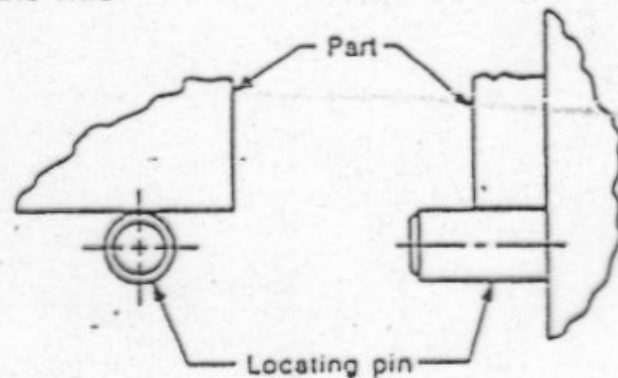


THIS ON THE DRAWING



4.6.1.2

MEANS THIS



Tolerances of straightness. A straightness tolerance may be used to control:

- | | | |
|--|---|---|
| (1) the straightness of a line on a surface,
or (2) the straightness of a line in a single plane, | } | in which cases the tolerance zone is the area between two parallel straight lines in the plane containing the considered line or axis, and the tolerance value is the distance between the lines. |
| or (3) the straightness of a line which is the axis of a feature or features which are solids of revolution. | } | in which case the tolerance zone is a cylinder with a diameter equal to the tolerance value. |

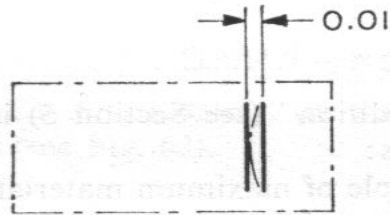
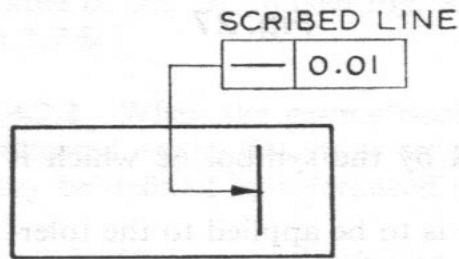
Tolerances of straightness

Examples

Interpretations

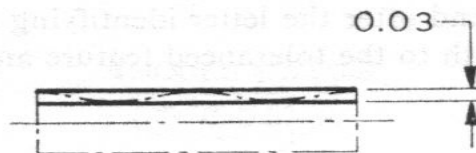
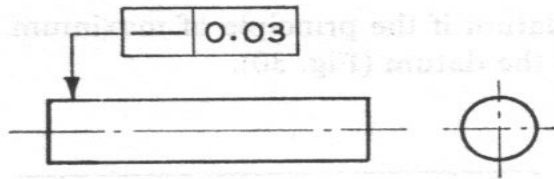
(1) Straightness of a line on a surface

a.



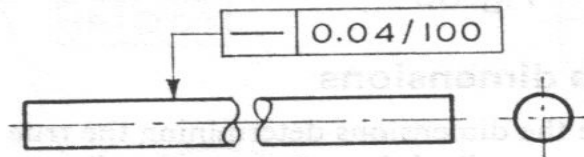
The particular line shown on the surface is required to lie between two parallel straight lines on the surface, 0.01 apart

b.



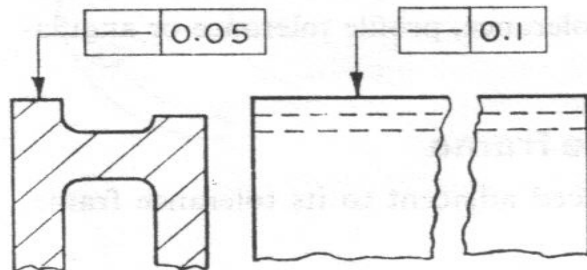
The surface of the feature in any of its positions, is required to lie between two parallel straight lines, 0.03 apart, lying in an axial plane

c.

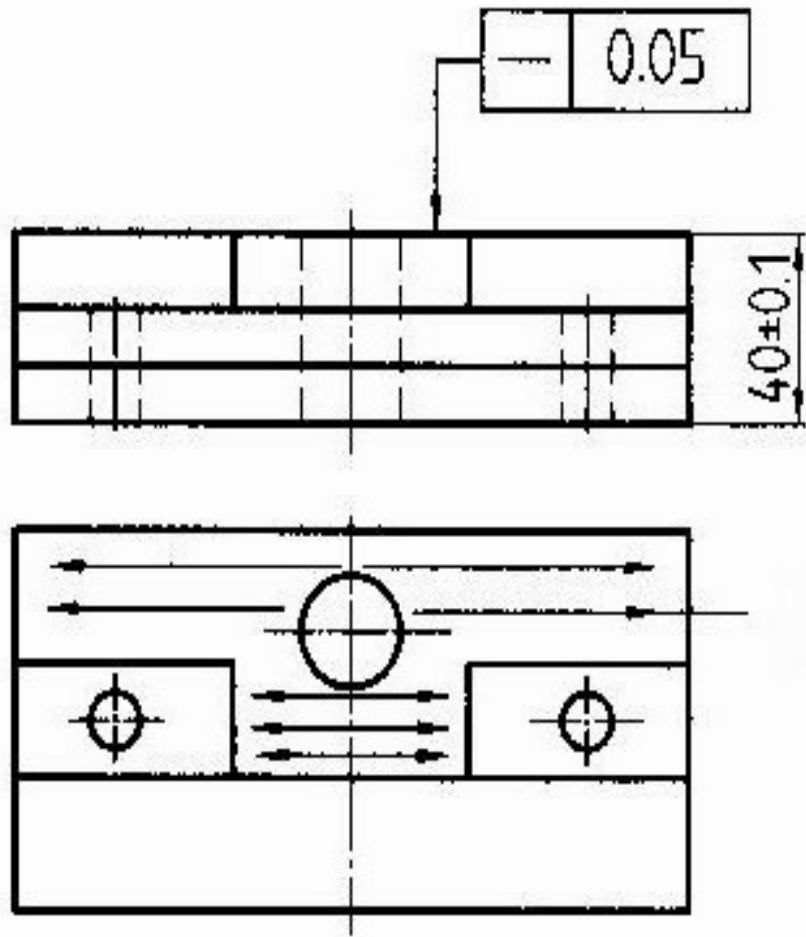


Any portion of length 100 of the generator of the cylinder is required to lie between two parallel straight lines, 0.04 apart, lying in an axial plane. See 2.5.3

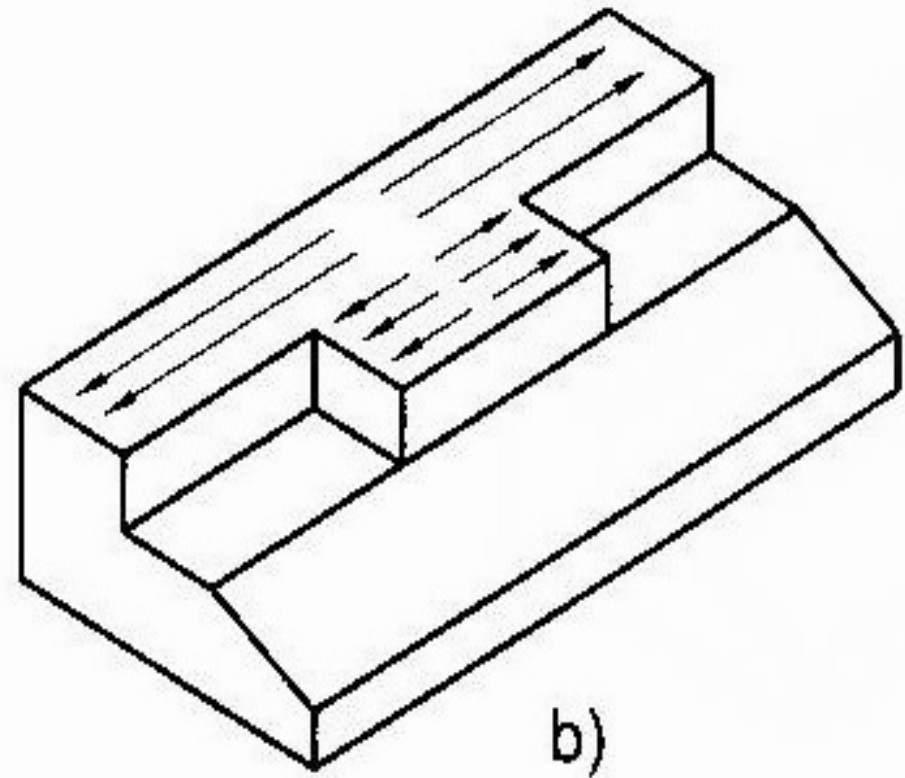
d. Straightness of lines in two directions on a surface



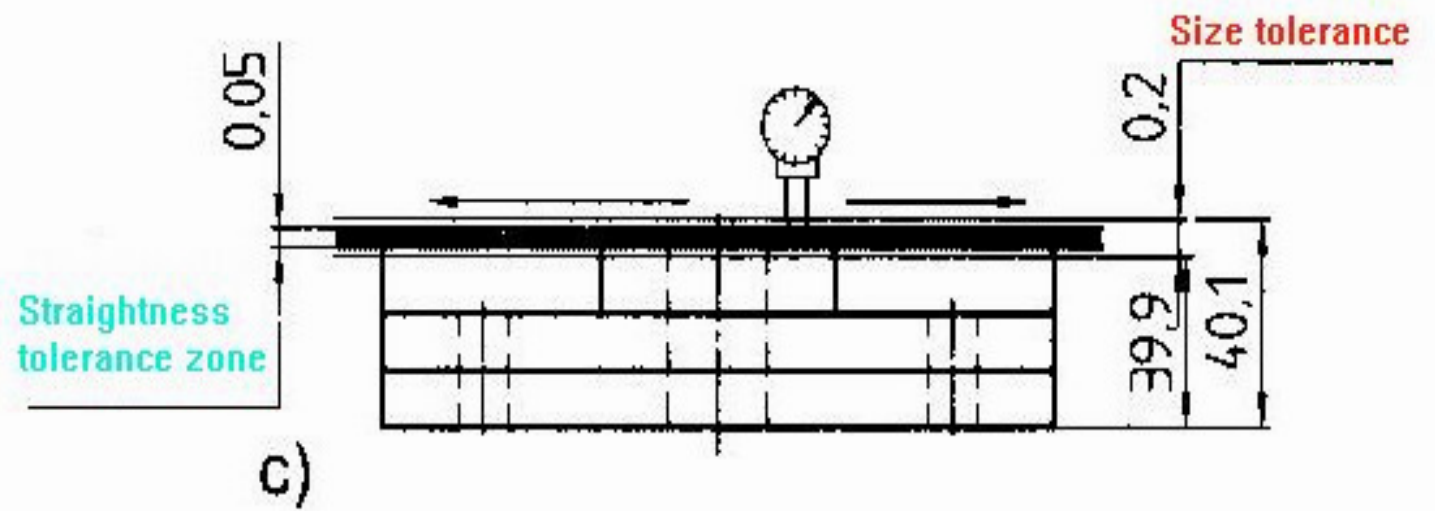
If two different straightness tolerances are applied in two directions on the same surface, the straightness tolerance zone of this surface is 0.05 in that direction shown on the left-hand view and 0.1 in that direction shown on the right-hand view



a)

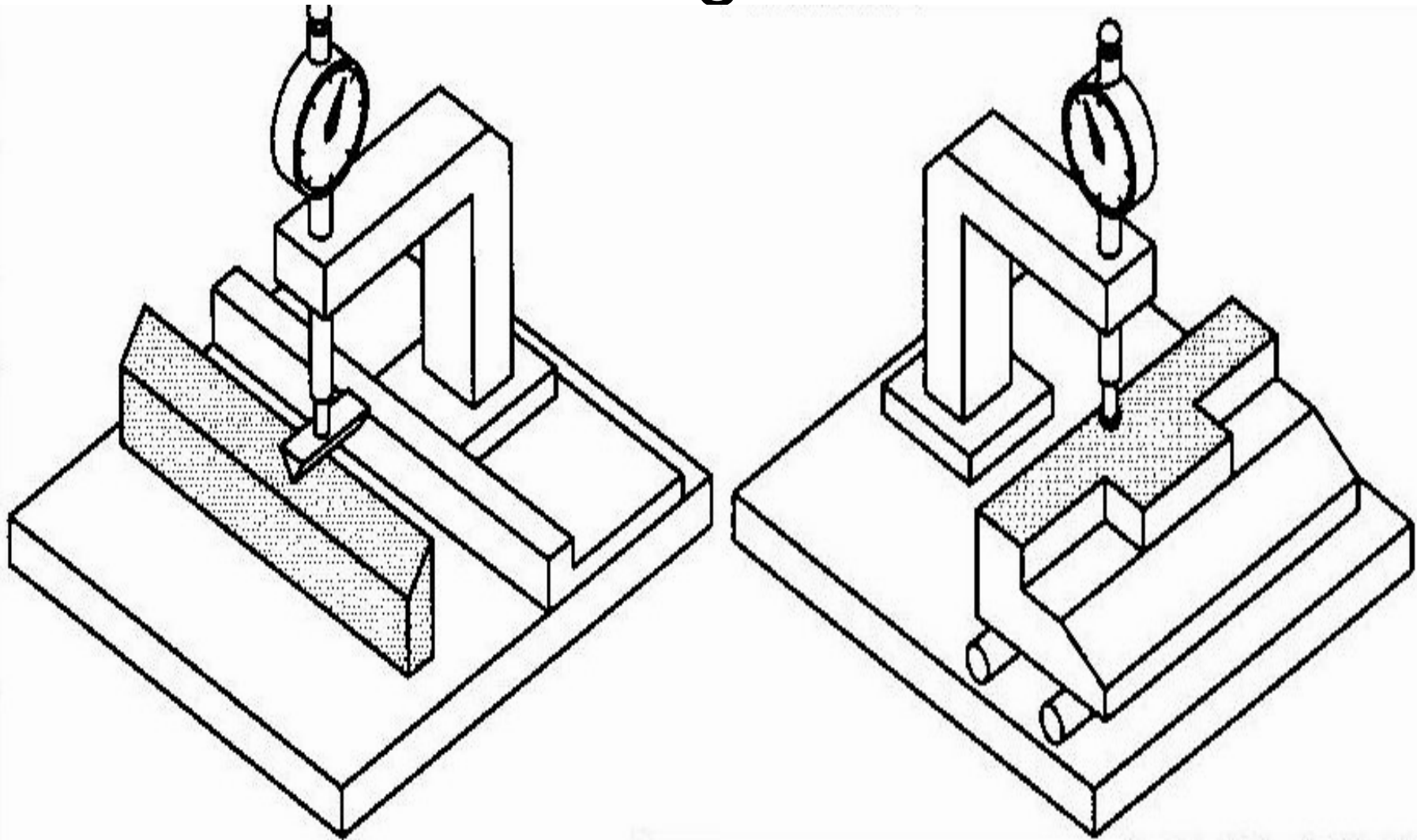


b)

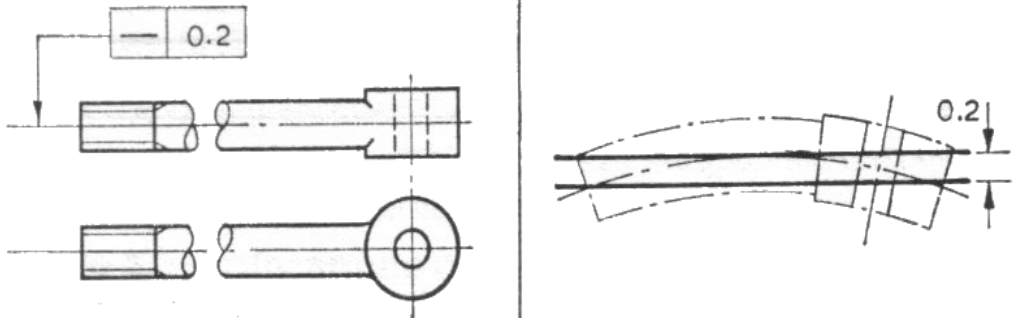
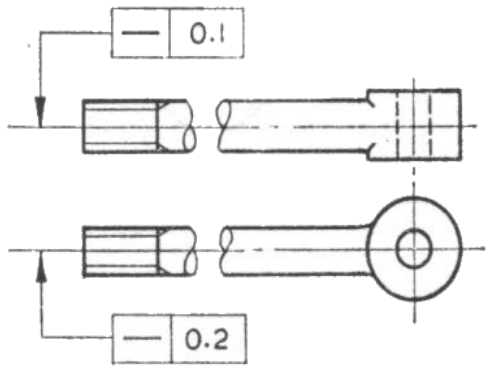


c)

Measurement of Straightness

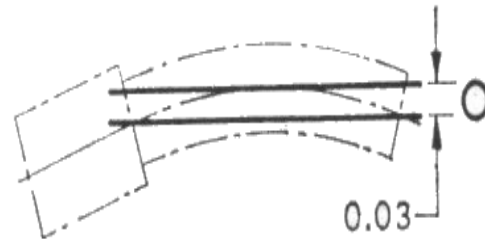
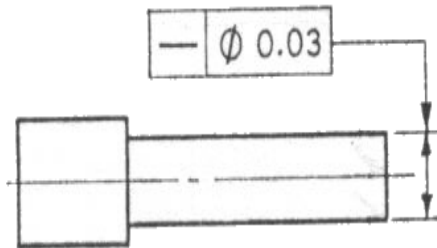


Tolerances of straightness (*continued*)

Examples	Interpretations
<p>(2) Straightness of a line in one plane</p> <p><i>a.</i></p> 	<p>In the plane of projection of the upper view, the axis of the whole tie rod is required to lie between two parallel straight lines 0.2 apart in that plane</p>
<p><i>b.</i> Straightness of a line in two planes</p> 	<p>The axis of the bar is required to be contained within a parallelepipedic zone of width 0.1 in the vertical plane and 0.2 in the horizontal plane</p>

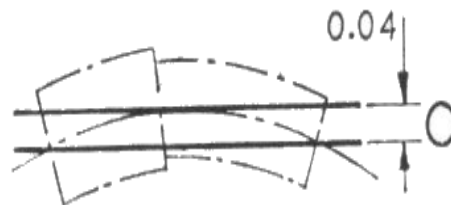
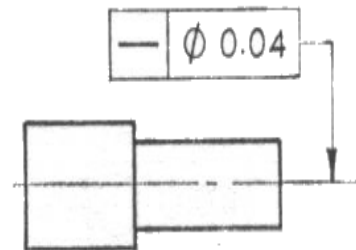
(3) Straightness of a line (e.g. the axis of a solid of revolution)

a.

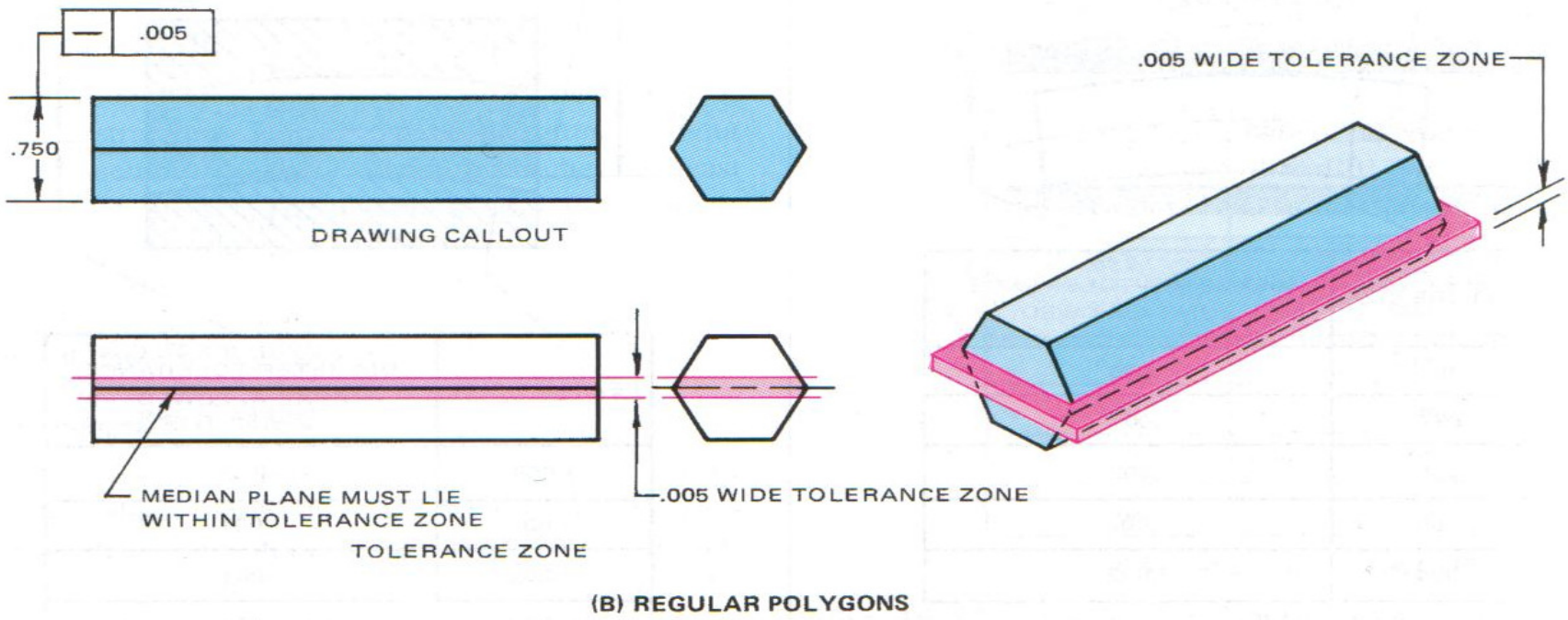
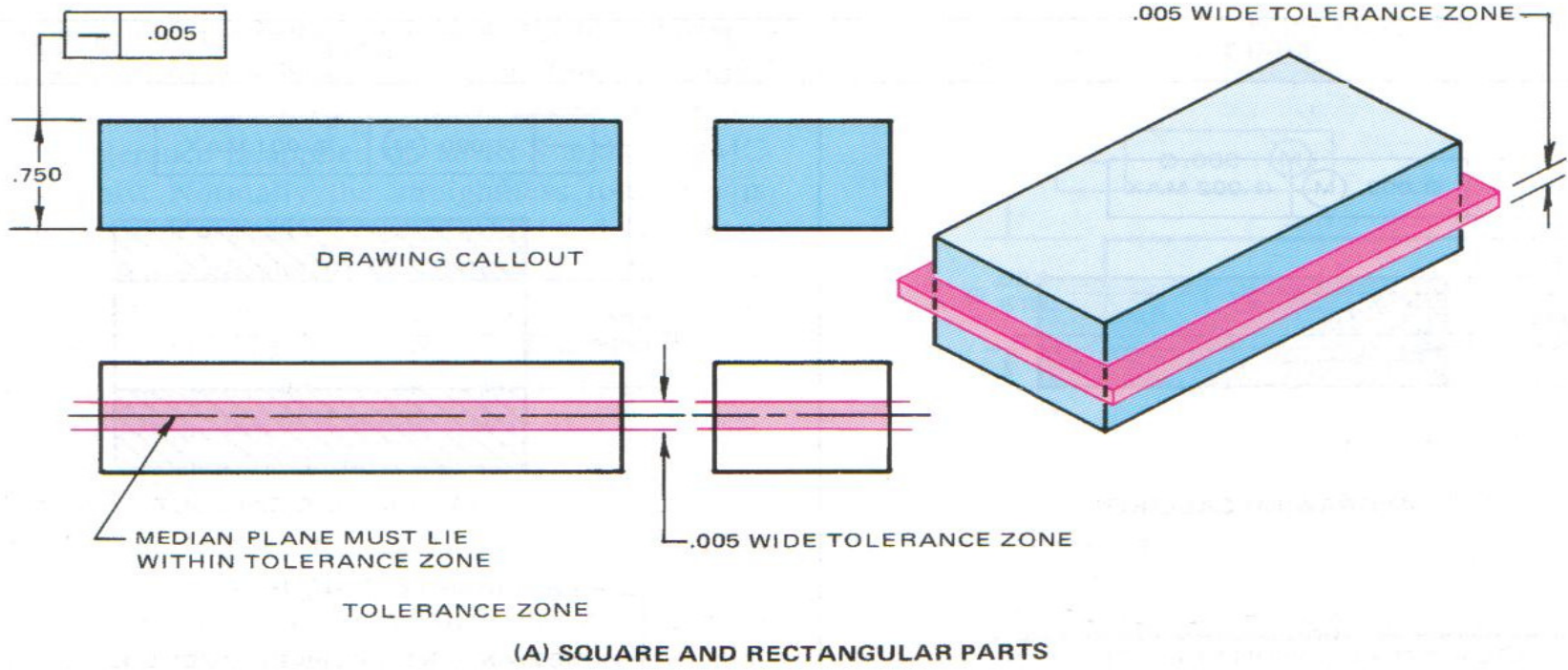


The axis of that part of the piece to be controlled is required to be contained in a cylindrical zone 0.03 diameter

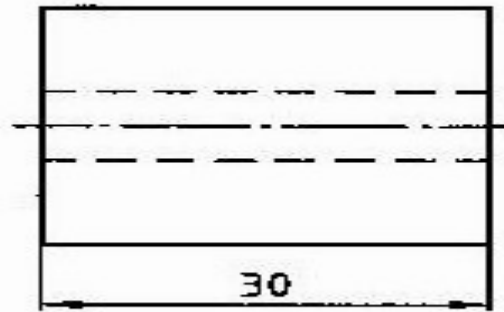
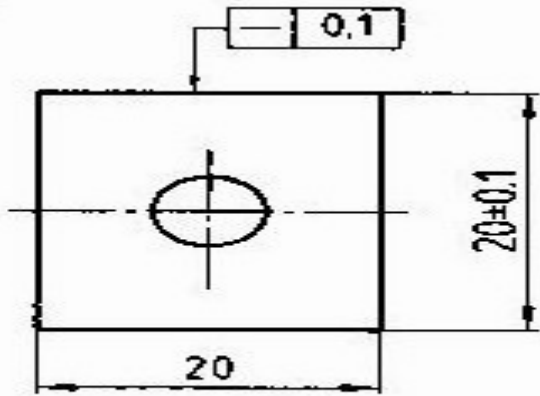
b.



The axis of the whole piece is required to be contained in a cylindrical tolerance zone of 0.04 diameter



Straightness of a median plane—RFS.



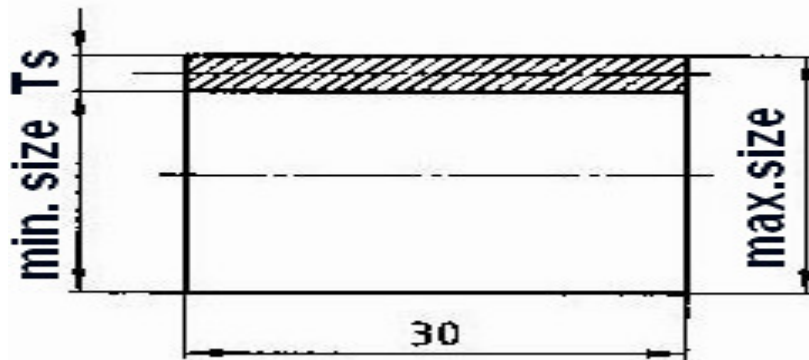
a)

$$T_s = +0,1 - (-0,1) = 0,2$$

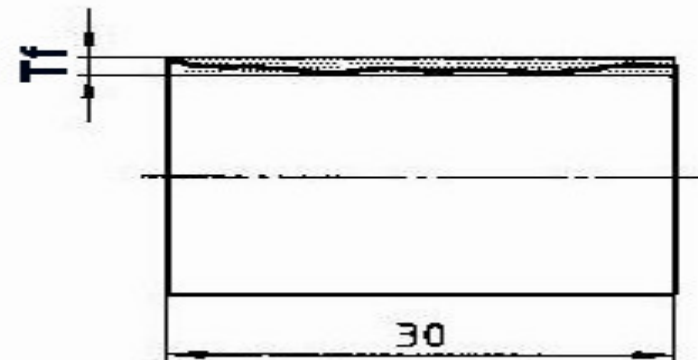
$$T_f = 0,1$$

Ts : Size tolerance

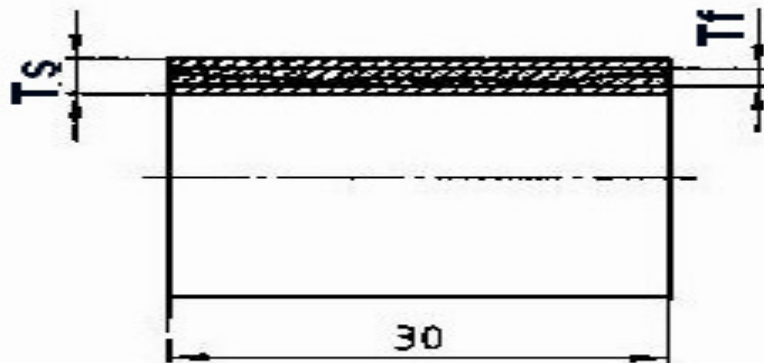
Tf : Form tolerance



b)



c)

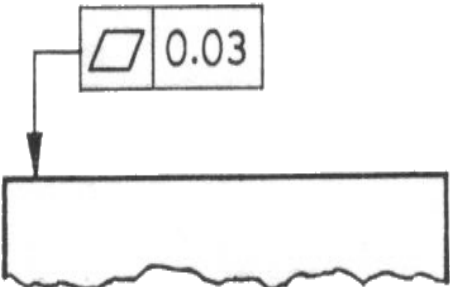
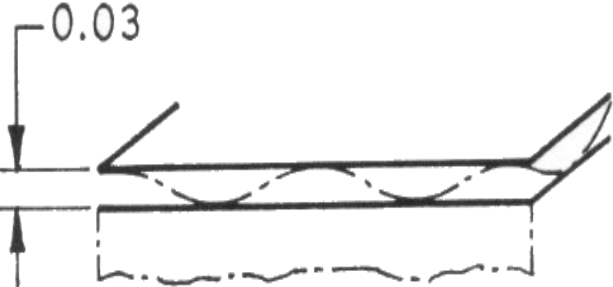


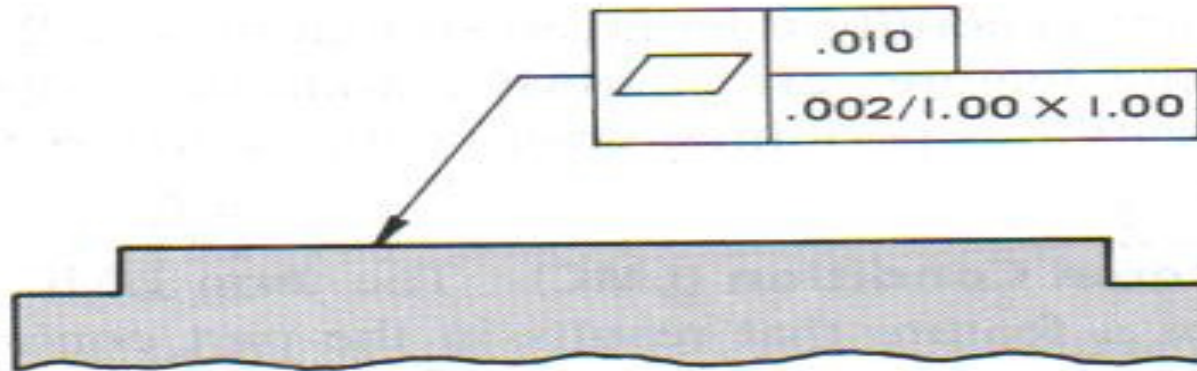
d)

Ts > Tf

Tolerances of flatness. When a flatness tolerance is used to control the flatness of a surface the tolerance zone is the space between two parallel planes and the tolerance value is the distance between the planes.

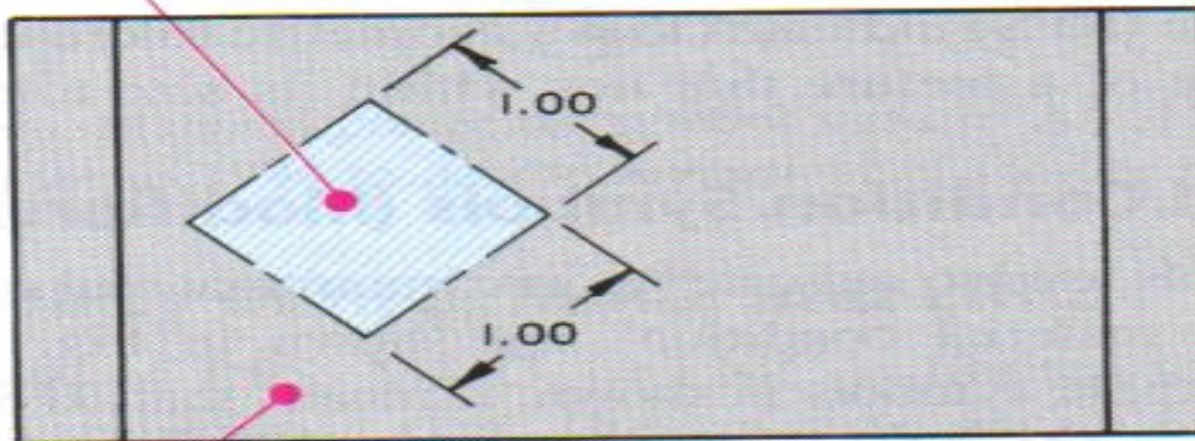
Tolerances of flatness

Examples	Interpretations
<p data-bbox="262 950 283 982"><i>a.</i></p> 	<p data-bbox="1344 779 1848 950">The indicated surface is required to lie between two parallel planes 0.03 apart</p> 



(A) DRAWING CALLOUT

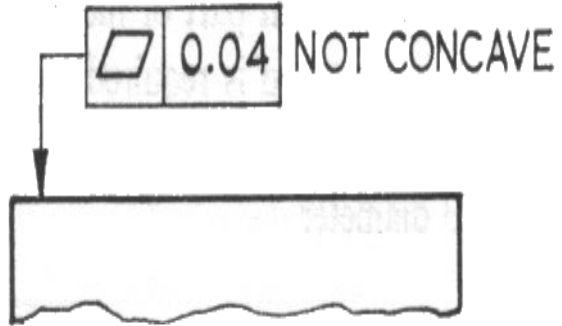
MAXIMUM FLATNESS TOLERANCE OF
 $.002$ FOR ANY 1.00 SQUARE SURFACE



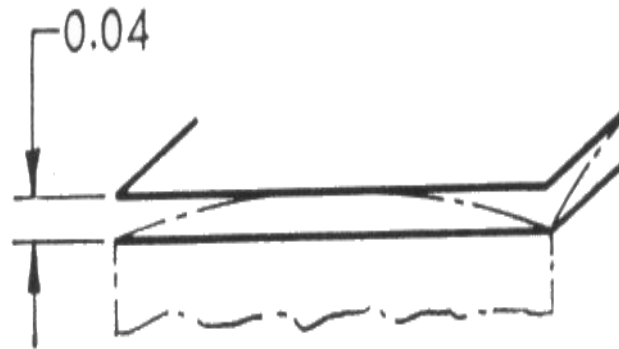
MAXIMUM FLATNESS TOLERANCE OF
 $.010$ FOR ENTIRE SURFACE AREA

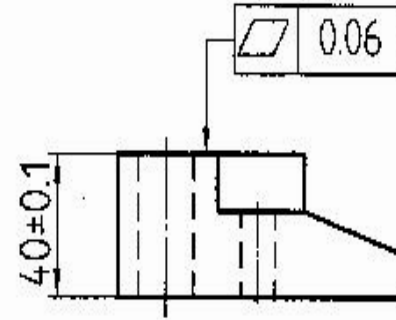
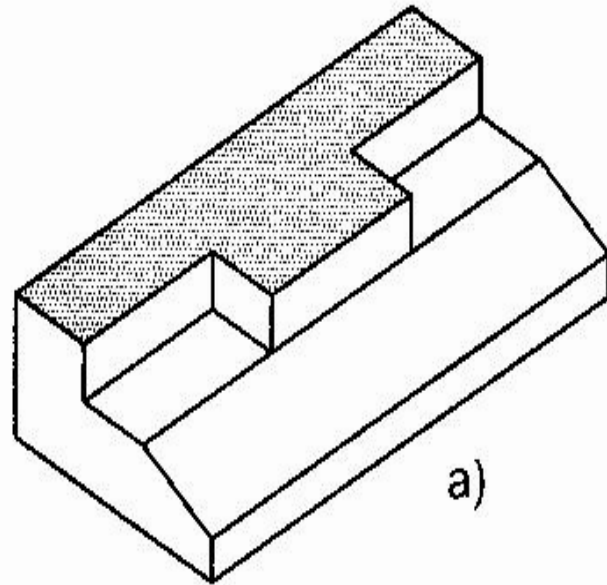
(B) INTERPRETATION

b.

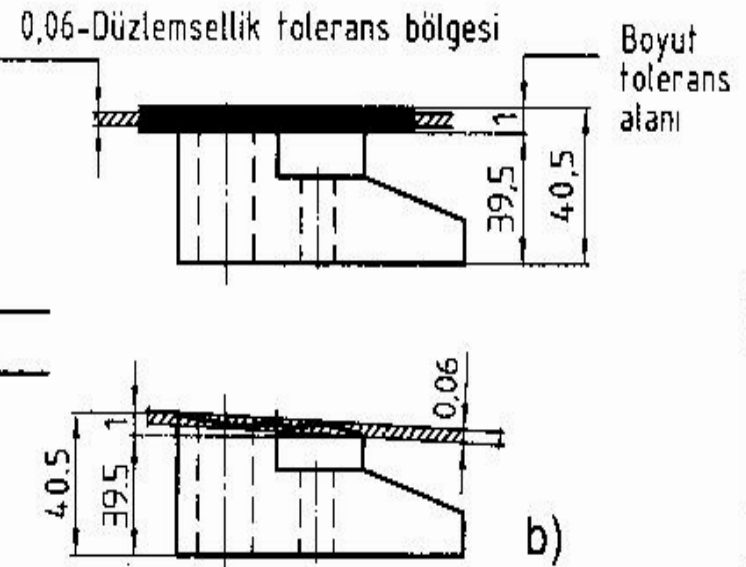
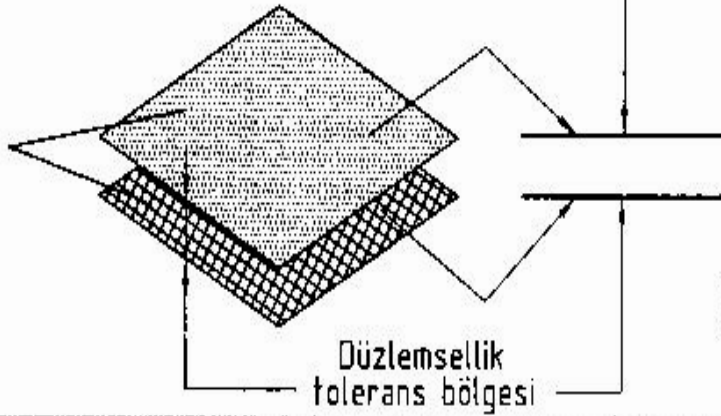


The indicated surface is required to lie between two parallel planes 0.04 apart and is not to be concave





Düzlemsellik tolerans bölgesi sınır düzlemleri



Tolerances of roundness

A roundness tolerance may be used to control the errors of form of a circle in the plane in which it lies. In the case of a solid of revolution the tolerance controls the roundness of the circle formed by the intersection of the surface with a plane; for a cylinder or cone the plane is perpendicular to the axis and for a sphere it normally, or unless otherwise specified, intersects the sphere in a section of maximum diameter.

A roundness tolerance is not concerned with the position of the circle, e.g. its concentricity with a datum axis. In the case of a solid of revolution, the roundness of each cross section is an individual assessment.

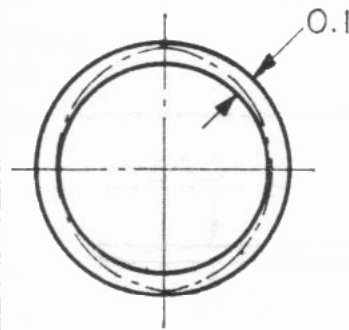
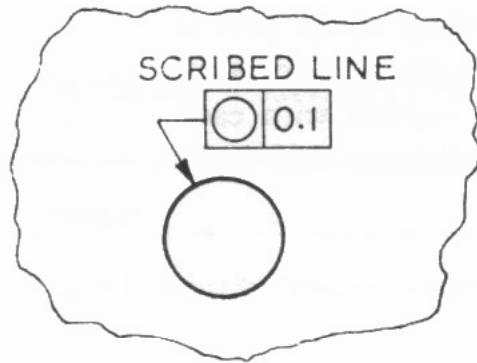
A roundness tolerance zone is the annular space between two co-planar circles concentric with each other, having a radial separation equal to the specified tolerance value.

Tolerances of roundness

Examples

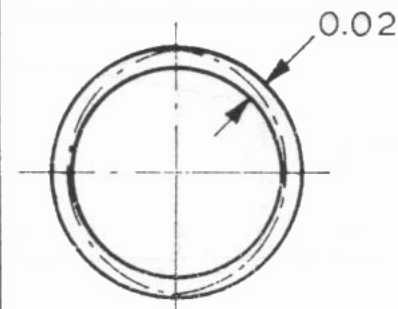
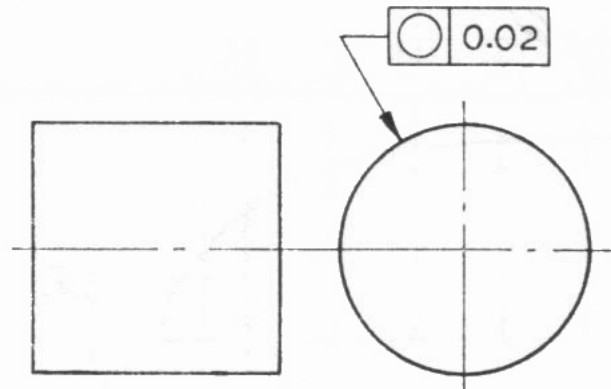
Interpretations

a.



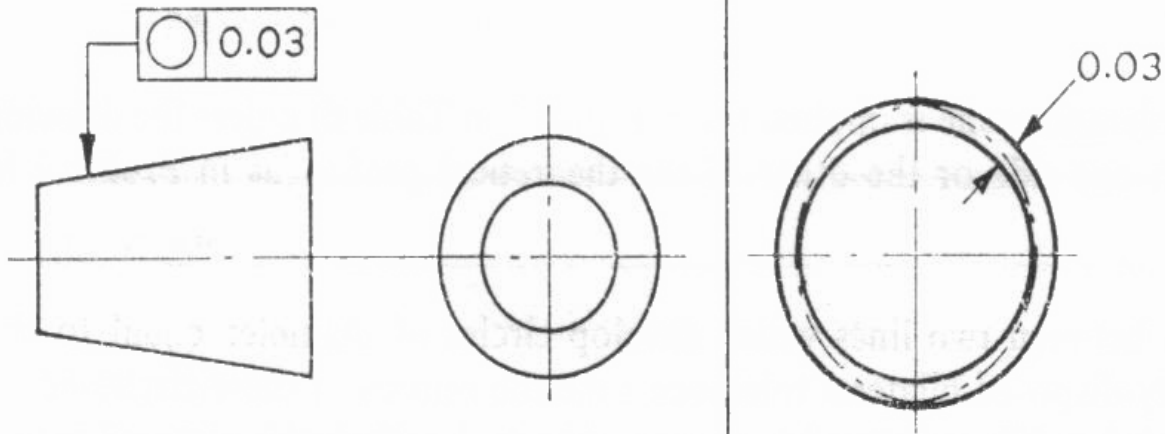
The considered line on the surface is required to lie between two circles concentric with each other, a radial distance 0.1 apart, on the surface

b.



The periphery at any cross section perpendicular to the axis is required to lie between two circles concentric with each other, a radial distance 0.02 apart, in the plane of the section

c.



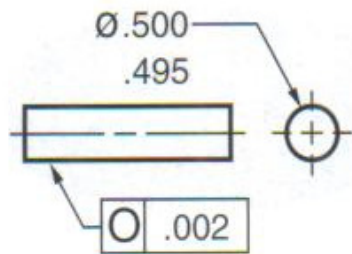
The periphery at any cross section perpendicular to the axis is required to lie between two circles concentric with each other, a radial distance 0.03 apart, in the plane of the section

d.

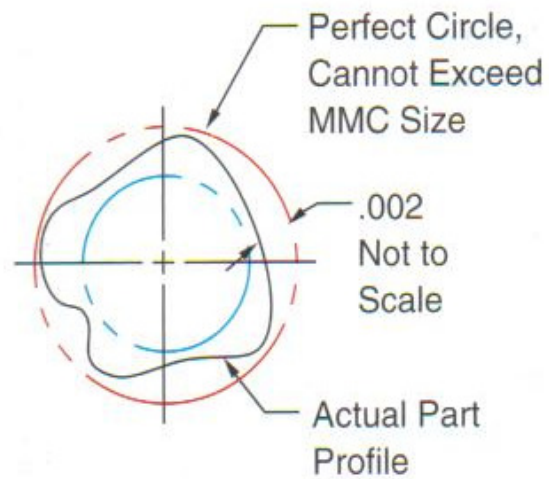


The periphery of any section of maximum diameter is required to lie between two circles concentric with each other, a radial distance 0.04 apart, in the plane of the section

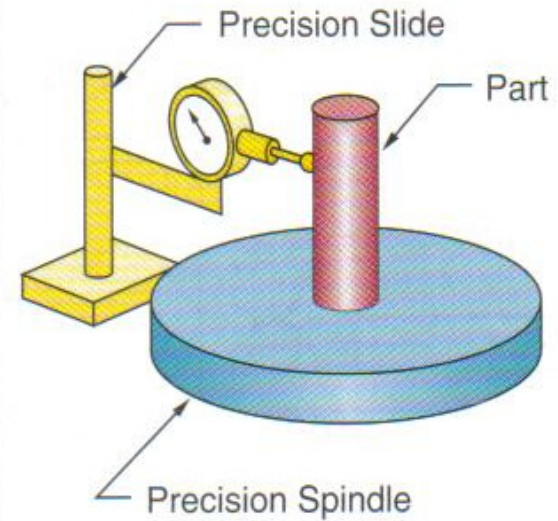
Circularity



Drawing



Tolerance Zone



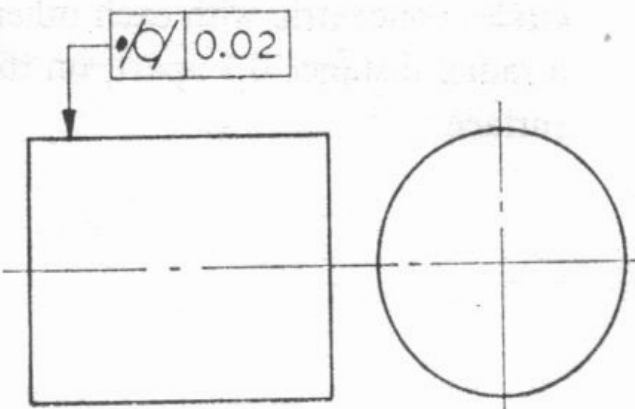
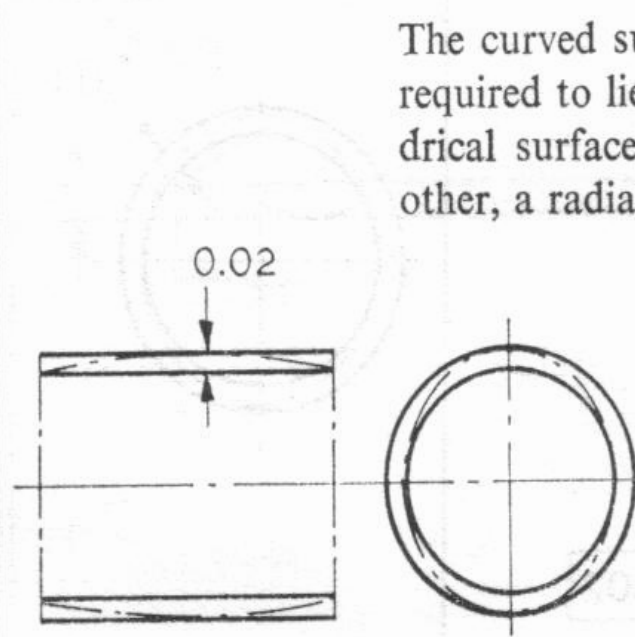
Inspection Method
(check only one slice at a time)

Tolerances of cylindricity

Cylindricity is a combination of roundness, straightness and parallelism applied to the surface of a cylinder. The plane (end) surfaces of a cylindrical part are not controlled by a cylindricity tolerance.

NOTE. Although the control of roundness, straightness and parallelism by means of a cylindricity tolerance may appear to be a convenient technique, the checking of cylindricity in accordance with its definition may present considerable difficulties. It is recommended that the individual characteristics comprising cylindricity be tolerated separately as appropriate to the part concerned.

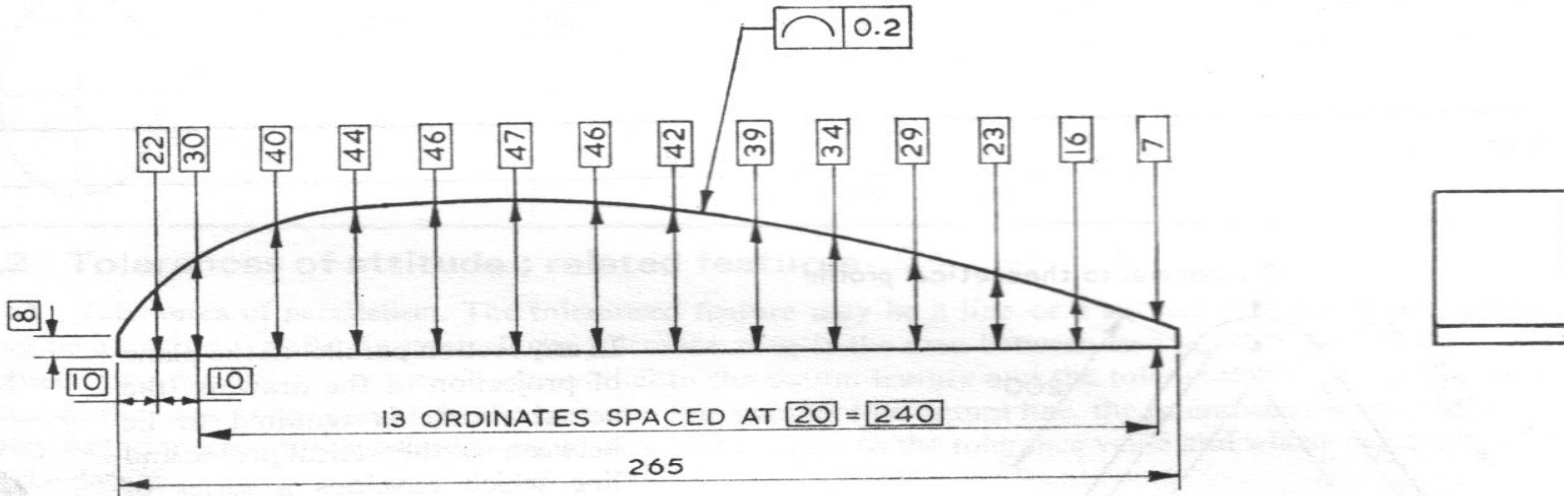
A cylindricity tolerance zone is the annular space between two cylinders coaxial with each other, having a radial separation equal to the specified tolerance value.

Example	Interpretation
 <p>The drawing shows a cylinder in two views: a front view (rectangle) and a top view (circle). A feature control frame is attached to the front view, containing the cylindricity symbol (a circle with a vertical line) and the tolerance value 0.02.</p>	<p>The curved surface of the part is required to lie between two cylindrical surfaces coaxial with each other, a radial distance 0.02 apart</p>  <p>The interpretation diagram shows the same cylinder with a tolerance zone indicated by two concentric circles. A vertical double-headed arrow between these circles is labeled 0.02, representing the radial distance between the two cylindrical surfaces.</p>

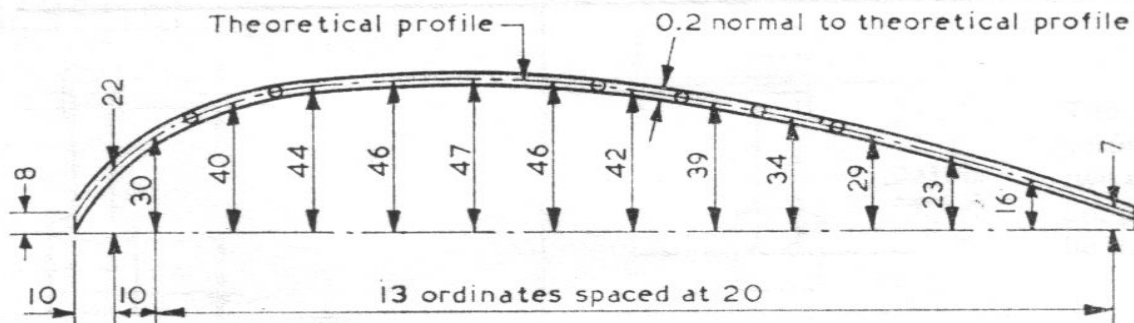
Profile tolerance of a line

Example

Profile 1. Equally-disposed bilateral tolerance



Interpretation

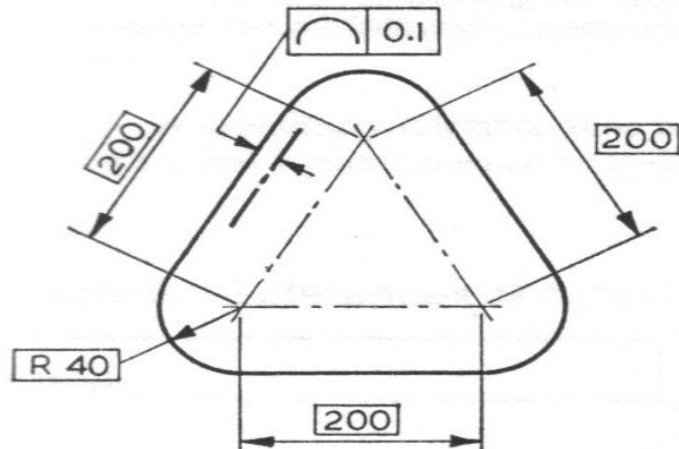


In any section parallel to the plane of projection of the drawing, the actual profile is required to lie between two lines which envelop a series of circles of diameter 0.2 with their centres on the theoretical profile

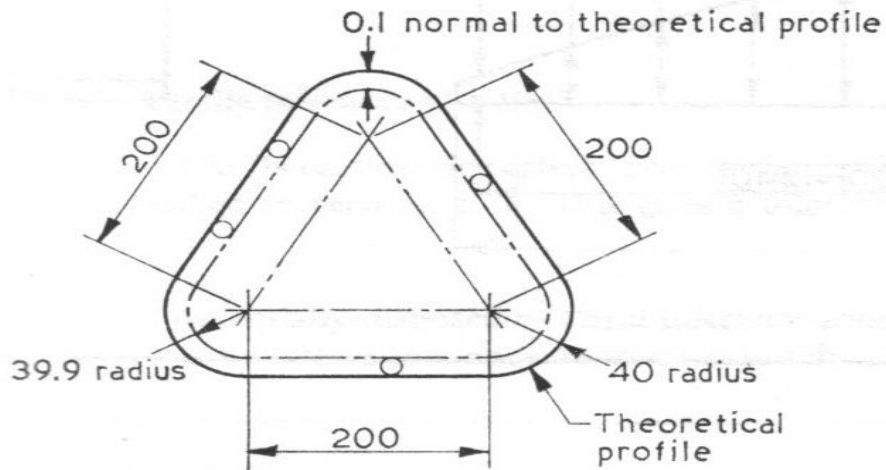
Profile tolerance of a line

Example

Profile 2. Unilateral tolerance

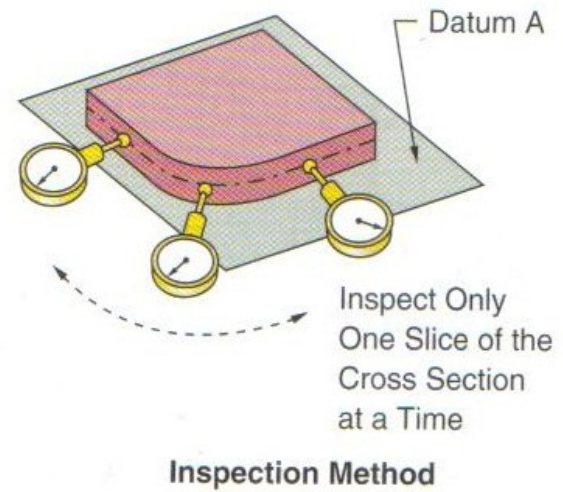
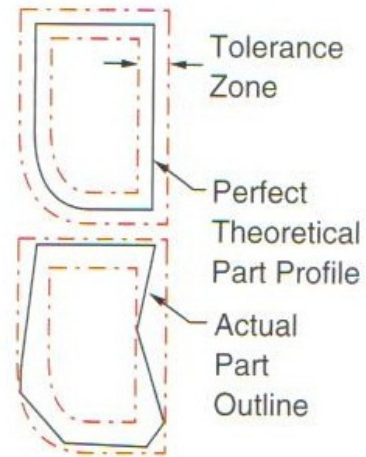
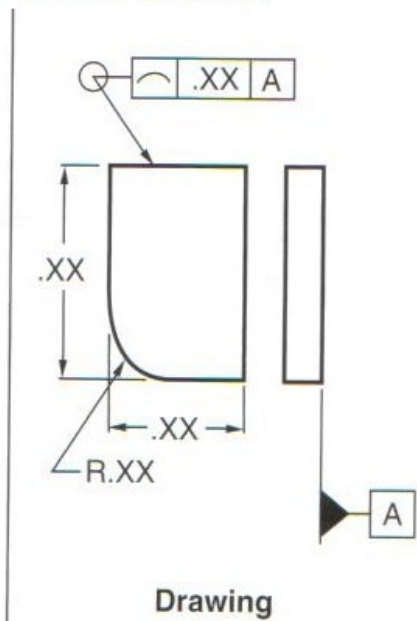


Interpretation

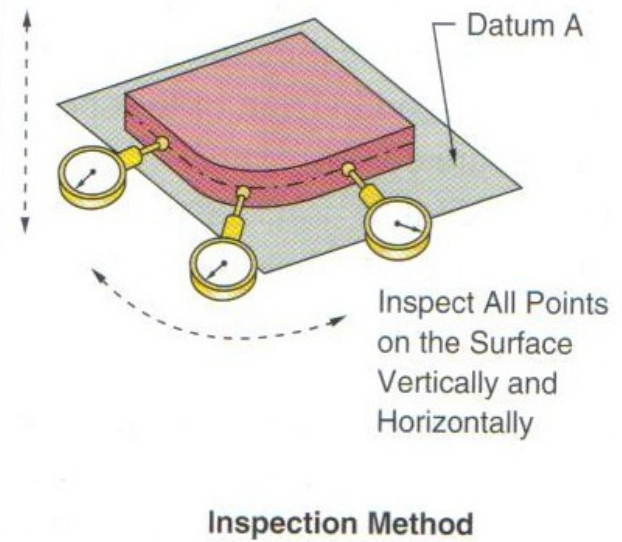
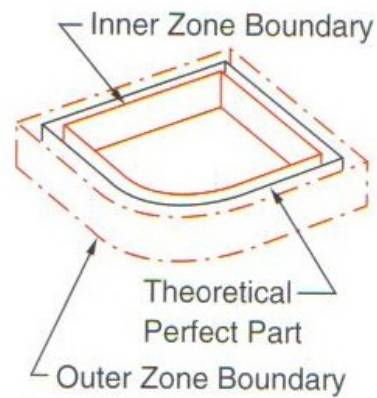
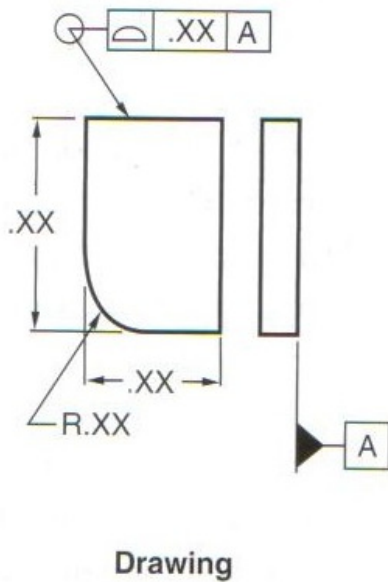


In any section parallel to the plane of projection of the drawing, the actual profile is required to lie between the theoretical profile and line which envelops a series of circles 0.1 diameter, touching and inside the theoretical profile

Profile of a line



Profile of a surface

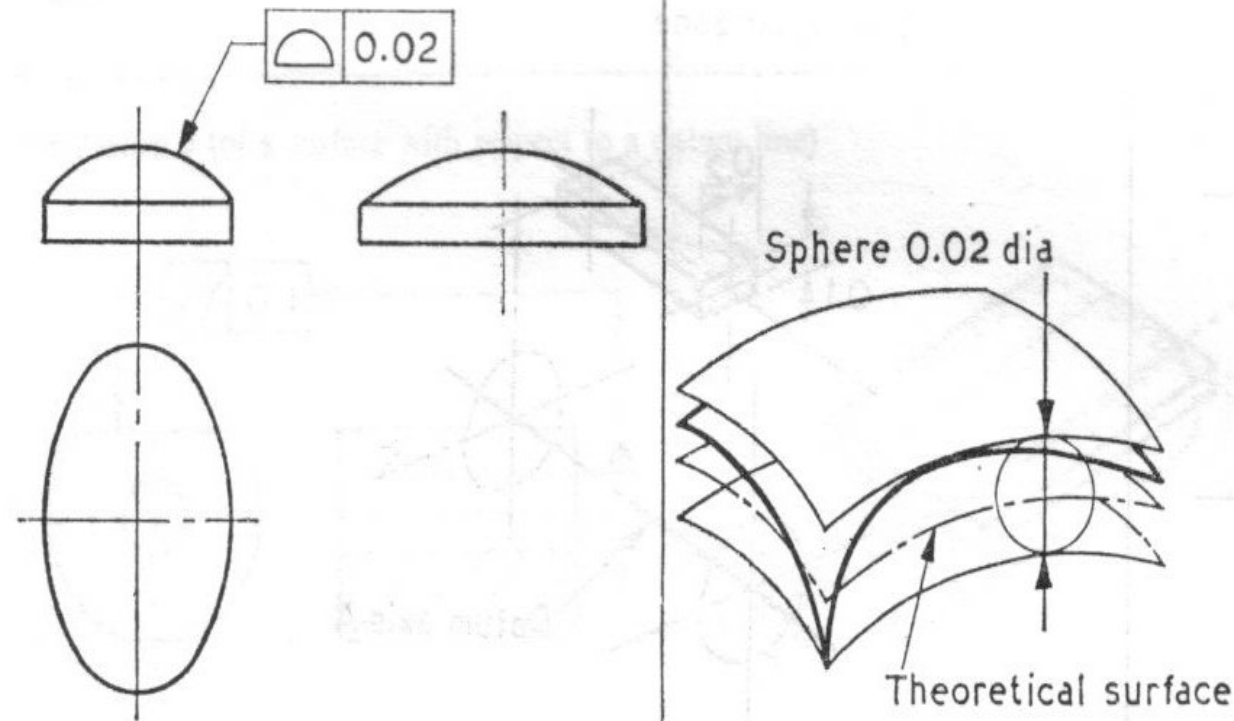


Profile tolerance of a surface

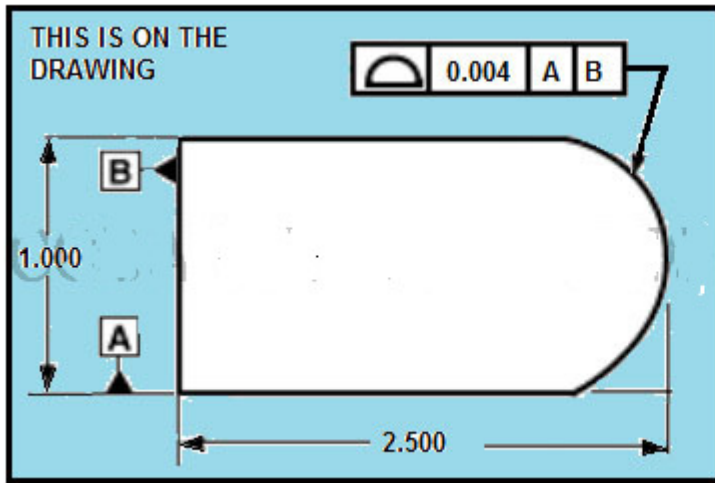
Example

Interpretation

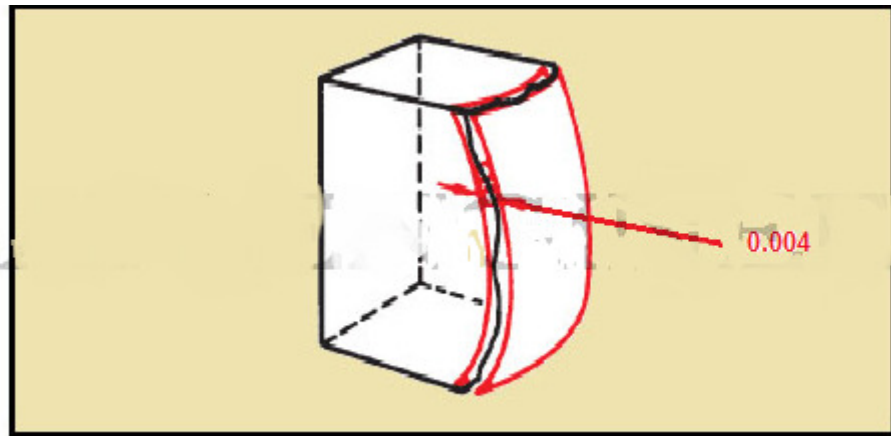
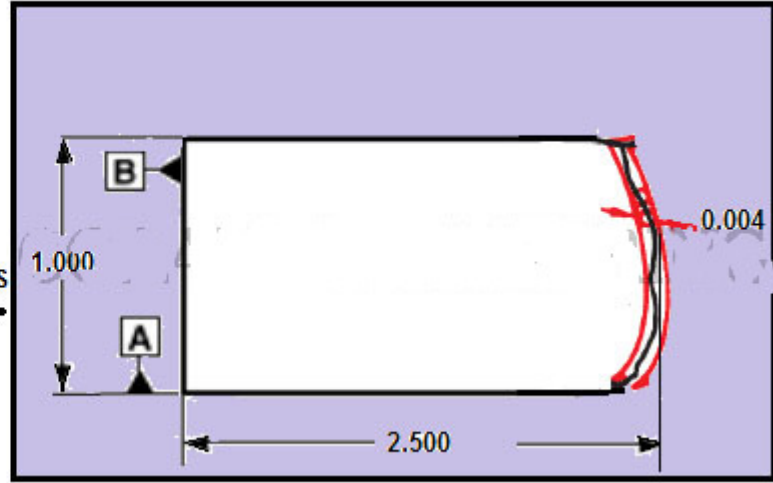
Surface shape. (an equally-disposed bilateral tolerance)

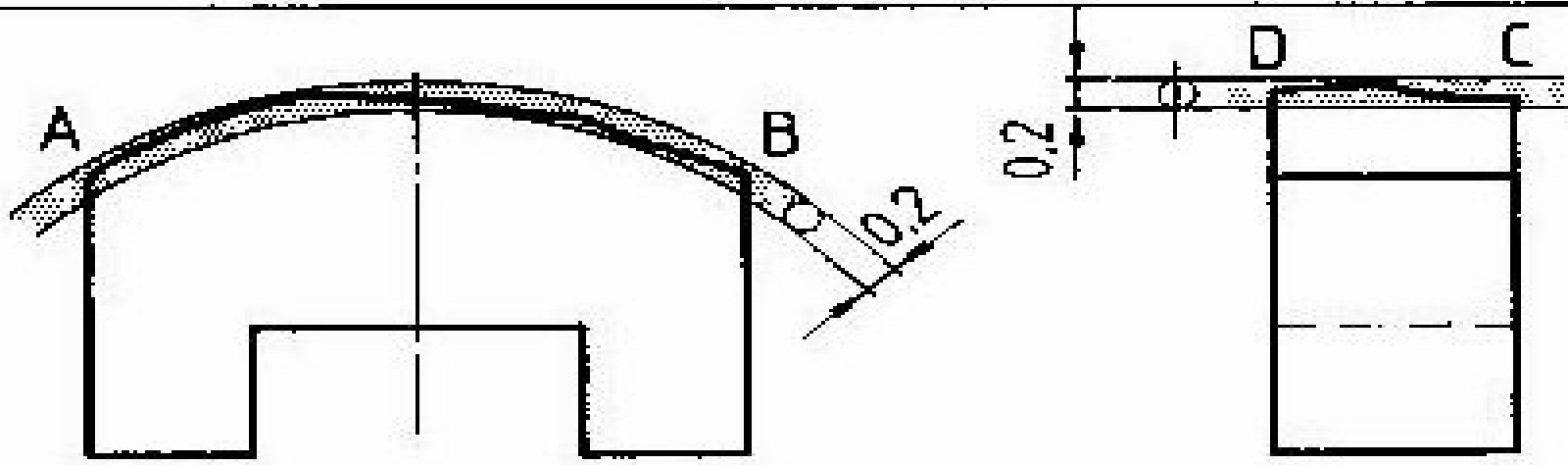
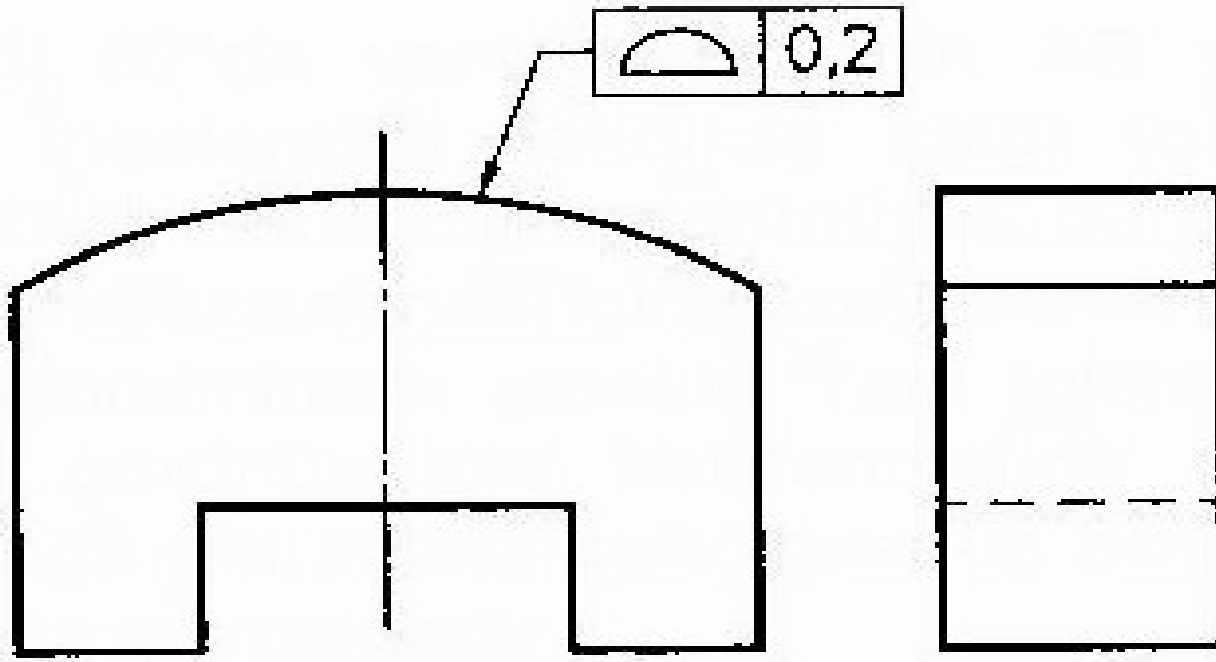


The curved surface of the part is required to lie between two surfaces which envelop a series of spheres, 0.02 diameter, with their centres on the surface having the correct geometrical shape



MEANS

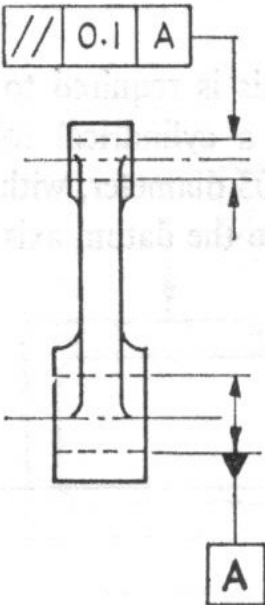
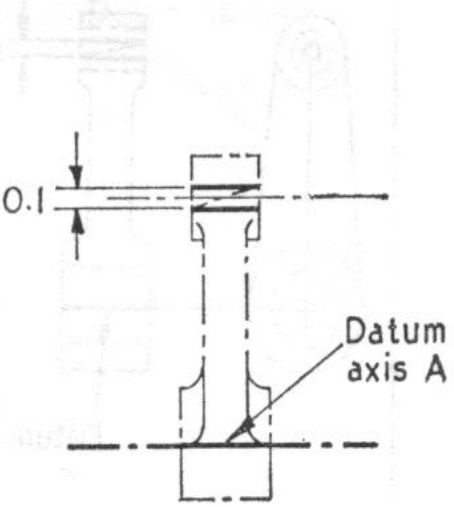




Tolerances of attitude ; related features

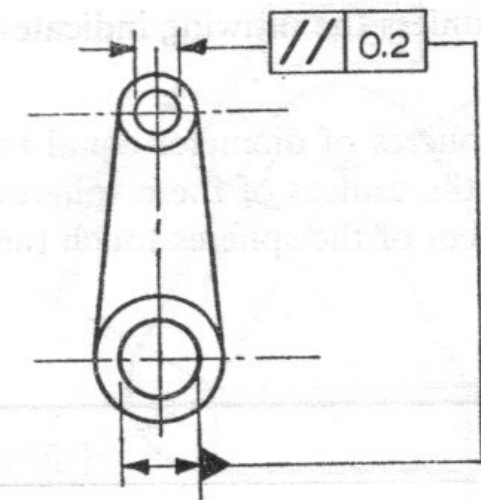
Tolerances of parallelism. The tolerated feature may be a line or a surface and the datum feature may be a line or a plane. In general, the tolerance zone is the area between two parallel lines or the space between two parallel planes which are parallel to the datum feature and the tolerance value is the distance between the lines or the planes. In the case of a line parallel to a datum line, the tolerance zone may alternatively be the space within a cylinder whose diameter is equal to the tolerance value and whose axis is parallel to the datum.

Tolerances of parallelism

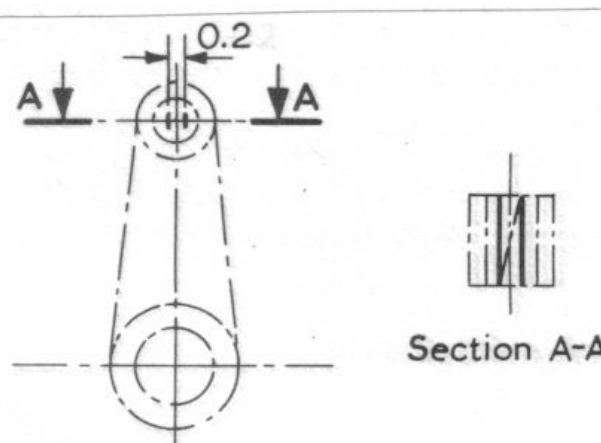
Example	Interpretation
<p><i>Parallelism 1 (of a line with respect to a datum line)</i></p> <p>a.</p> 	 <p>The axis of the upper cylindrical surface is required to lie between two straight lines, 0.1 apart, which are parallel to the datum axis and lie in the vertical plane through it</p>

Examples

b.

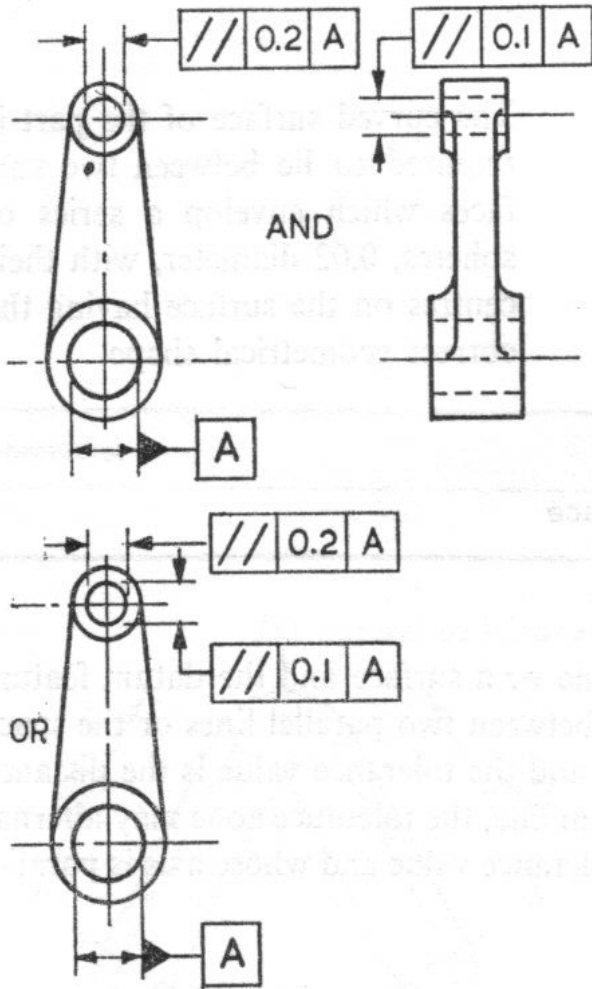


Interpretations

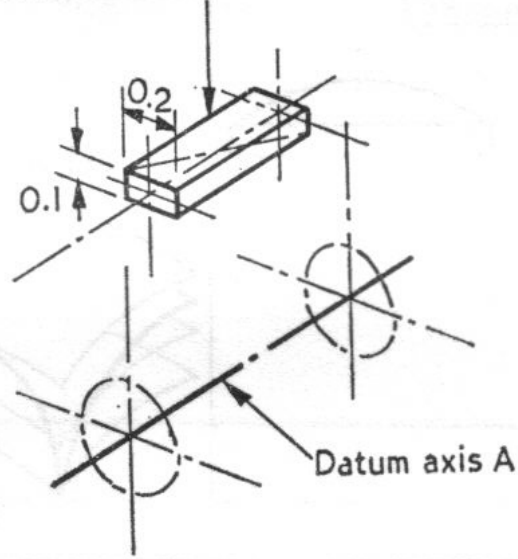


The upper axis is required to lie between two straight lines, 0.2 apart, which are parallel to the datum axis and lie in the horizontal plane

c.

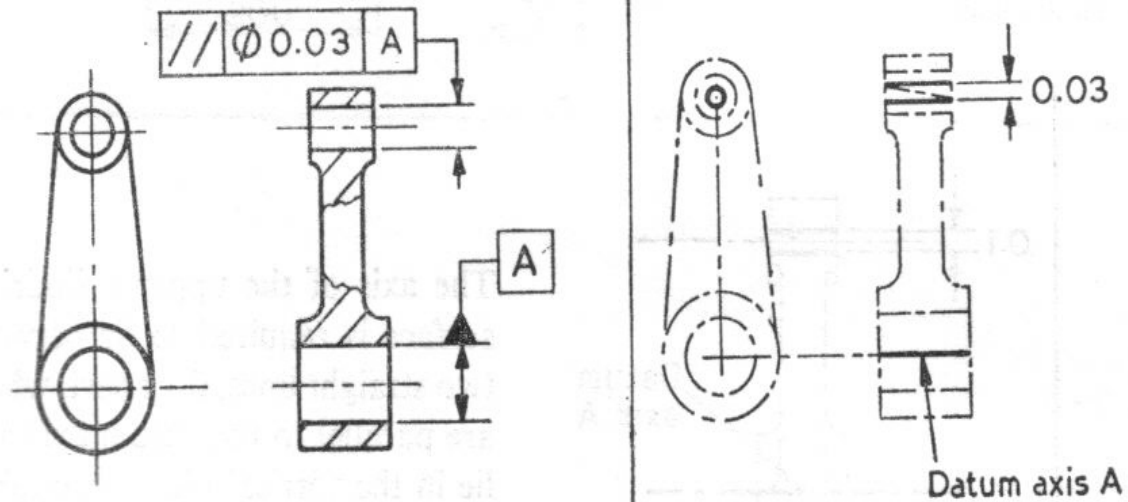


Tolerance zone



The upper axis is required to be contained in a parallelepiped having a width of 0.2 in the horizontal plane and a width of 0.1 in the vertical plane, its sides being parallel to the datum axis A

d.

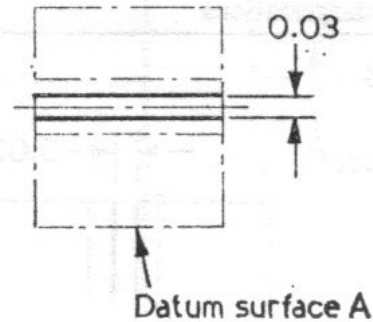
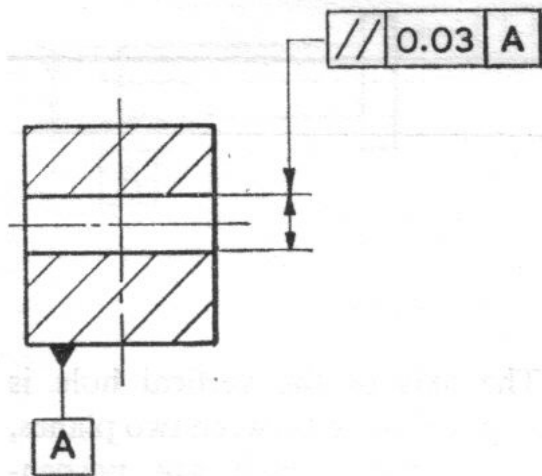


The upper axis is required to be contained in a cylindrical tolerance zone, 0.03 diameter, with its axis parallel to the datum axis

Examples

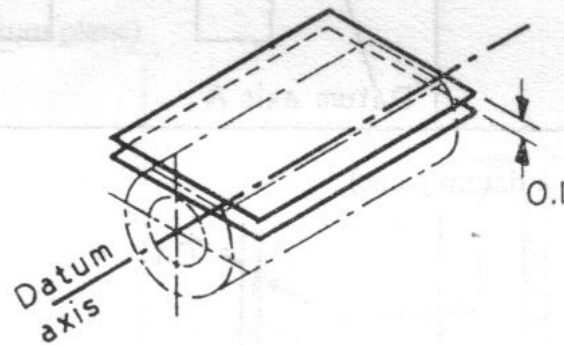
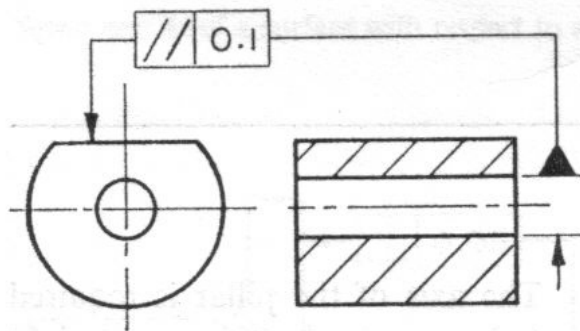
Interpretations

Parallelism 2 (of a line with respect to a datum plane)



The axis of the hole is required to lie between two planes, 0.03 apart, parallel to the datum plane

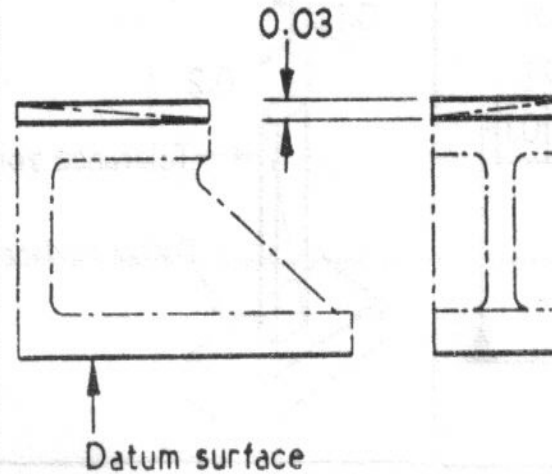
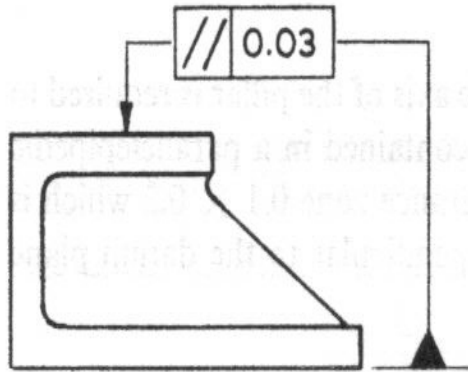
Parallelism 3 (of a surface with respect to a datum line)



The surface of the part is required to lie between two parallel planes, 0.1 apart, parallel to the datum axis of the hole

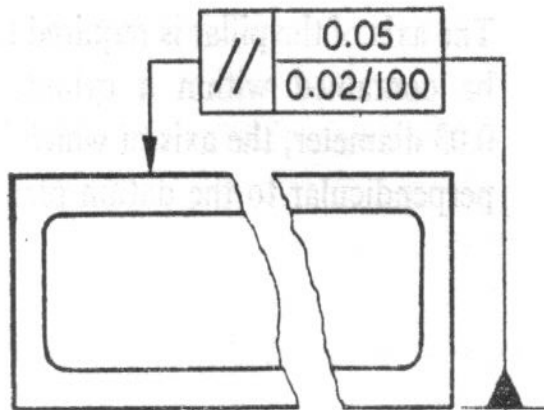
Parallelism 4 (of a surface with respect to a datum plane)

a.

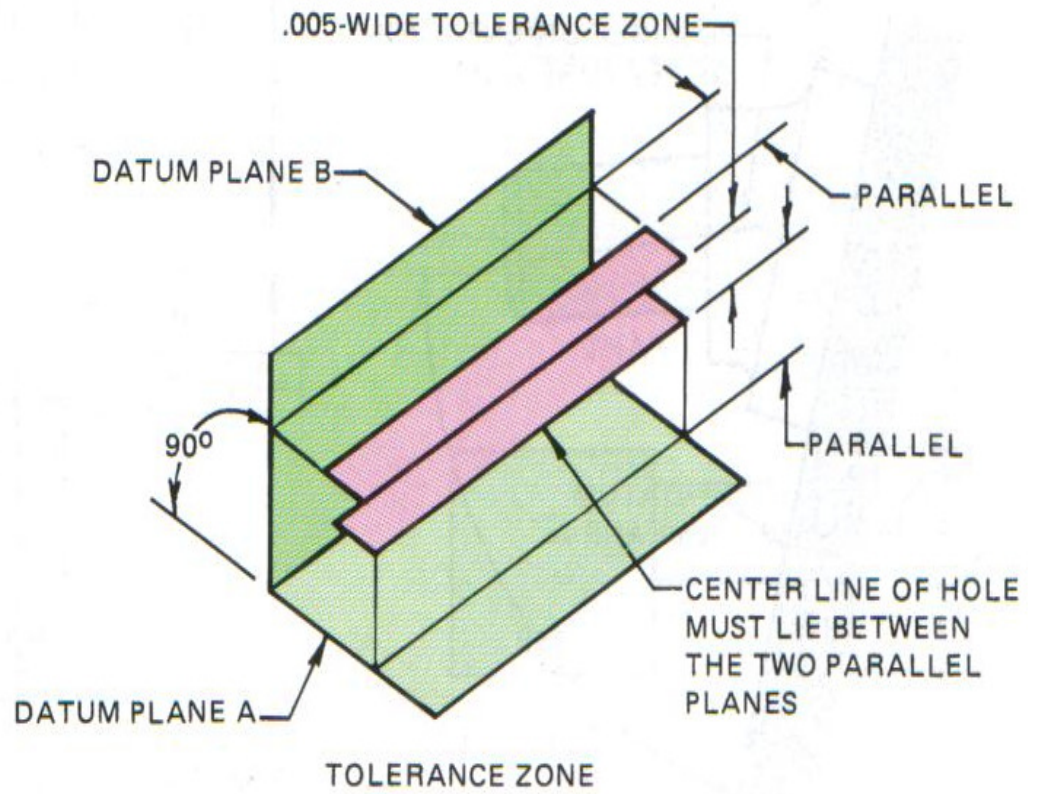
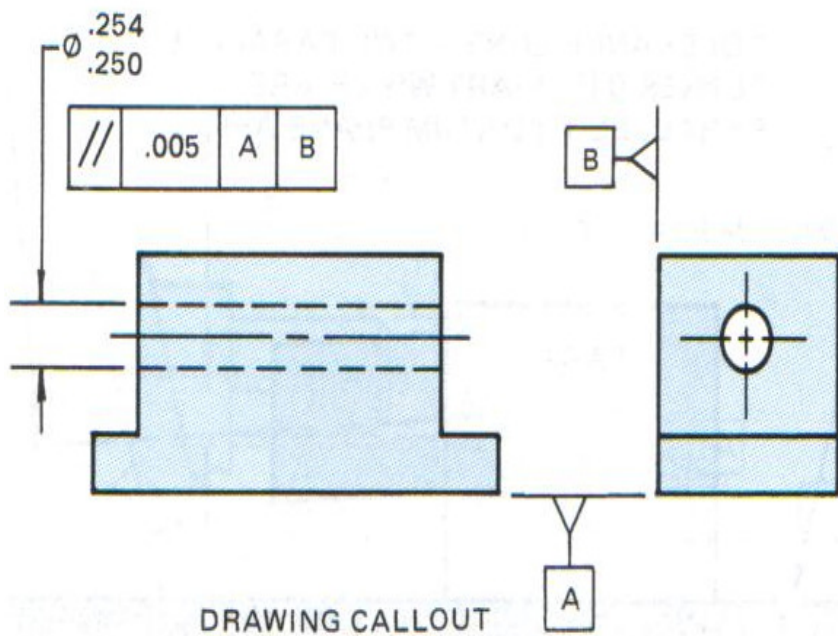


The top surface of the part is required to lie between two planes, 0.03 apart, parallel to the datum plane

b.



The top surface of the part is required to lie between two planes, 0.05 apart, parallel to the datum plane and all the points in a line of length 100 anywhere in the top surface of the part are required to lie between two planes, 0.02 apart, parallel to the datum plane.



PARALLELISM TOLERANCE

Tolerances of squareness. The tolerated feature may be a line or a surface and the datum feature may be a line or a plane. In general, the tolerance zone is the area between two parallel lines or the space between two parallel planes which are perpendicular to the datum feature and the tolerance value is the distance between the lines or the planes. In the case of a line with respect to a datum plane, the tolerance zone may alternatively be the space within a cylinder of diameter equal to the tolerance value; in this case the tolerance value is preceded by the symbol \varnothing .

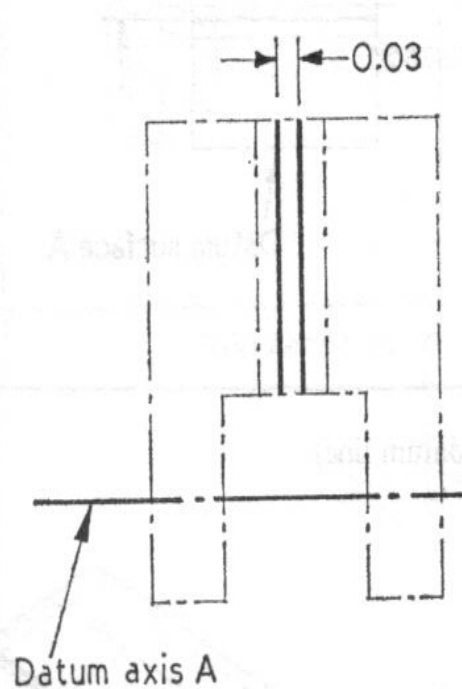
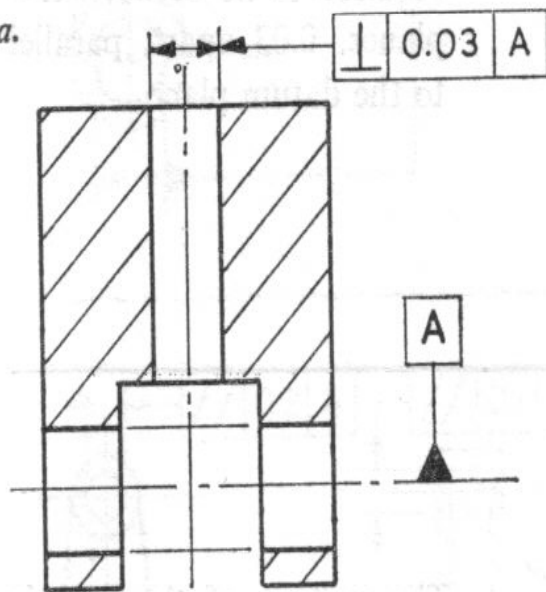
Tolerances of squareness

Examples

Interpretations

Squareness 1 (of a line with respect to a datum line)

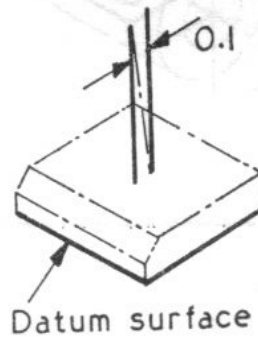
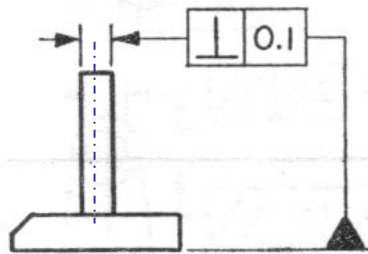
a.



The axis of the vertical hole is required to lie between two planes, 0.03 apart, which are perpendicular to the common axis of the two horizontal holes

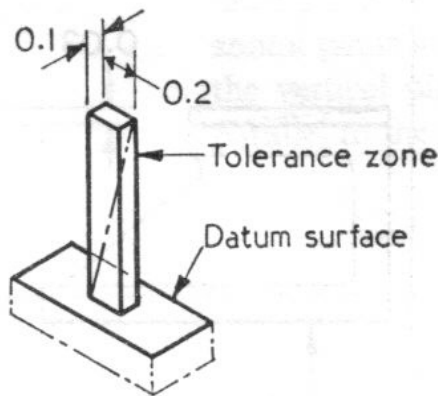
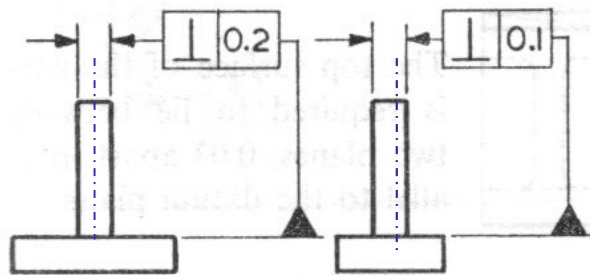
Squareness 2 (of a line with respect to a datum plane)

a.



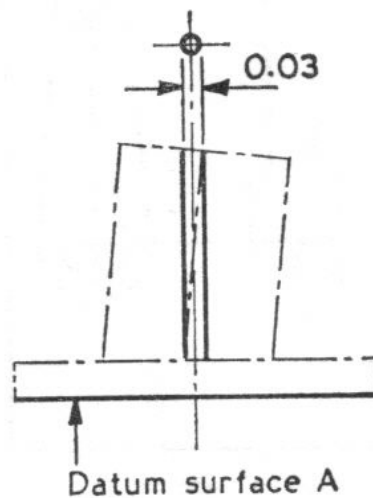
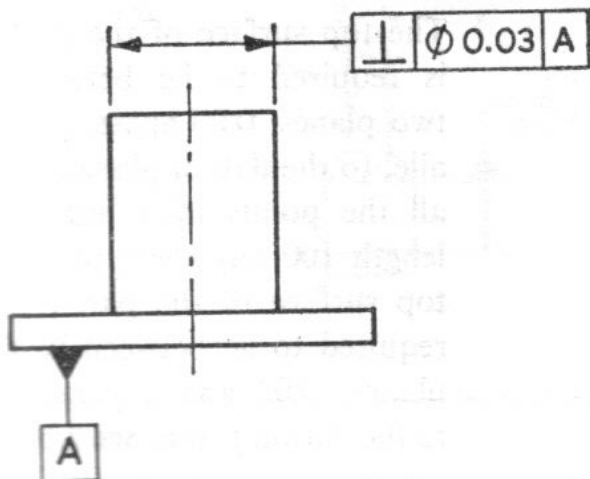
The axis of the pillar is required to be contained within two straight lines 0.1 apart, perpendicular to the datum surface and lying in the plane shown on the drawing

b.



The axis of the pillar is required to be contained in a parallelepipedic tolerance zone 0.1×0.2 which is perpendicular to the datum plane

c.

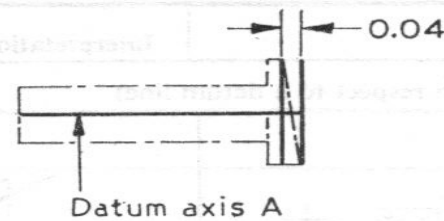
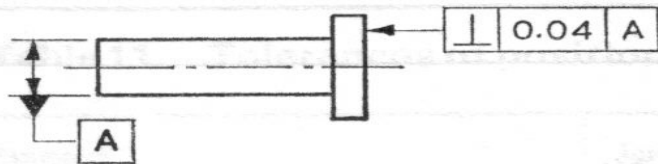


The axis of the pillar is required to be contained within a cylinder, 0.03 diameter, the axis of which is perpendicular to the datum plane

Examples

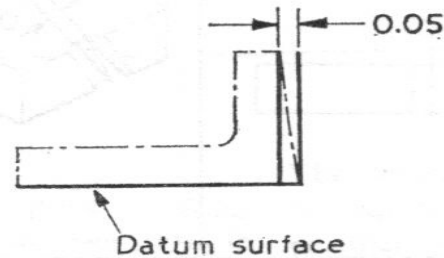
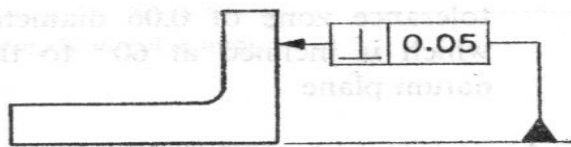
Interpretations

Squareness 3 (of a surface with respect to a datum line)



The right-hand end-face of the part is required to lie between two planes, 0.04 apart, which are perpendicular to the axis of the cylindrical portion on the left of the drawing

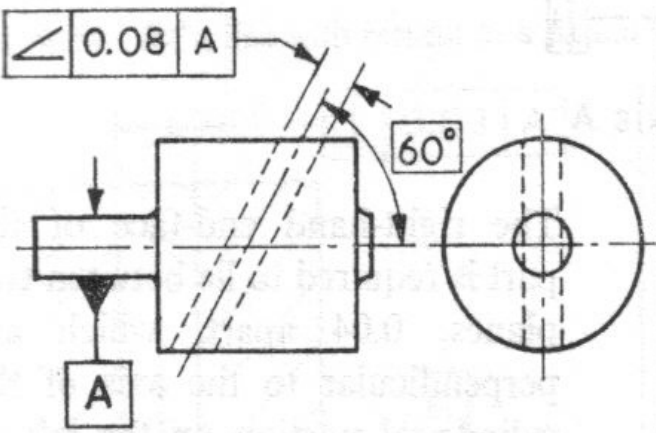
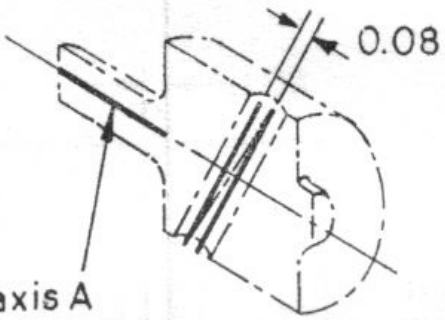
Squareness 4 (of a surface with respect to a datum plane)



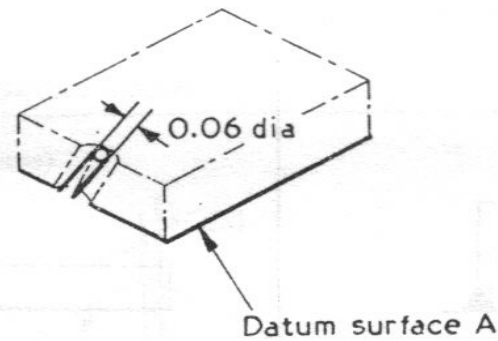
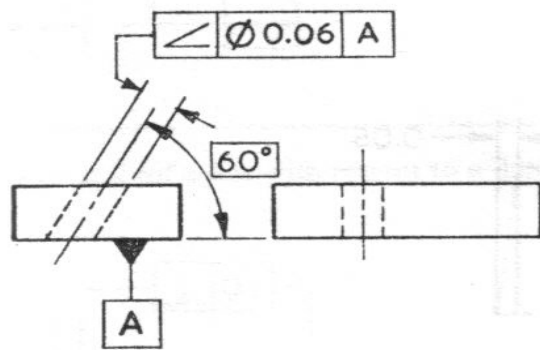
The right-hand face of the part is required to lie between two parallel planes, 0.05 apart, which are perpendicular to the datum plane

Tolerances of angularity. The toleranced feature may be a line or a surface and the datum feature may be a line or a plane. The tolerance zone is the area between two parallel lines or the space between two parallel planes which are inclined at the specified angle to the datum feature and the tolerance value is the distance between the lines or the planes.

Table 10. Tolerances of angularity

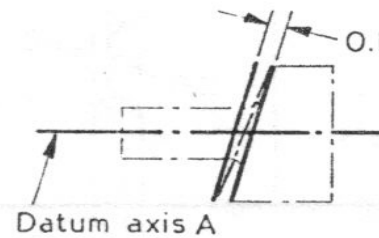
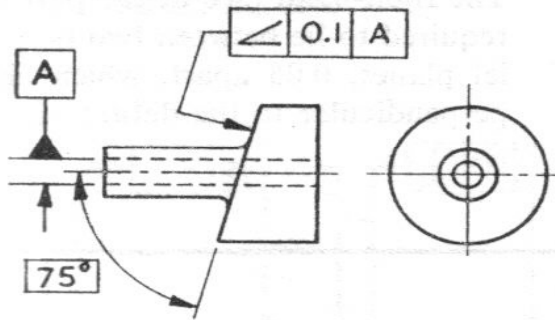
Examples	Interpretations
<p><i>Angularity 1 (of a line with respect to a datum line)</i></p> 	 <p>The axis of the inclined hole is required to lie between two parallel straight lines, 0.08 apart, which are inclined at 60° to the datum axis</p>

Angularity 2 (of a line with respect to a datum plane)



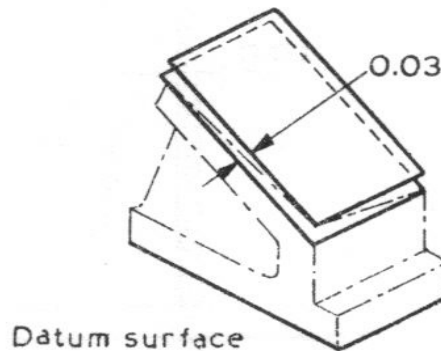
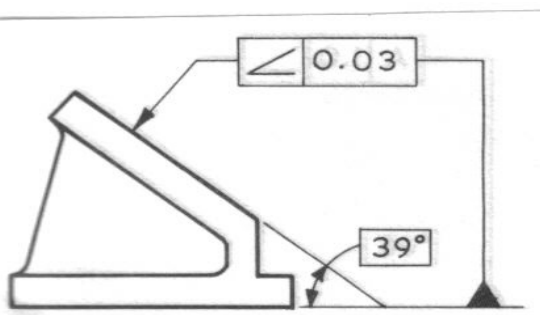
The axis of the inclined hole is required to lie within a cylindrical tolerance zone of 0.06 diameter which is inclined at 60° to the datum plane

Angularity 3 (of a surface with respect to a datum line)

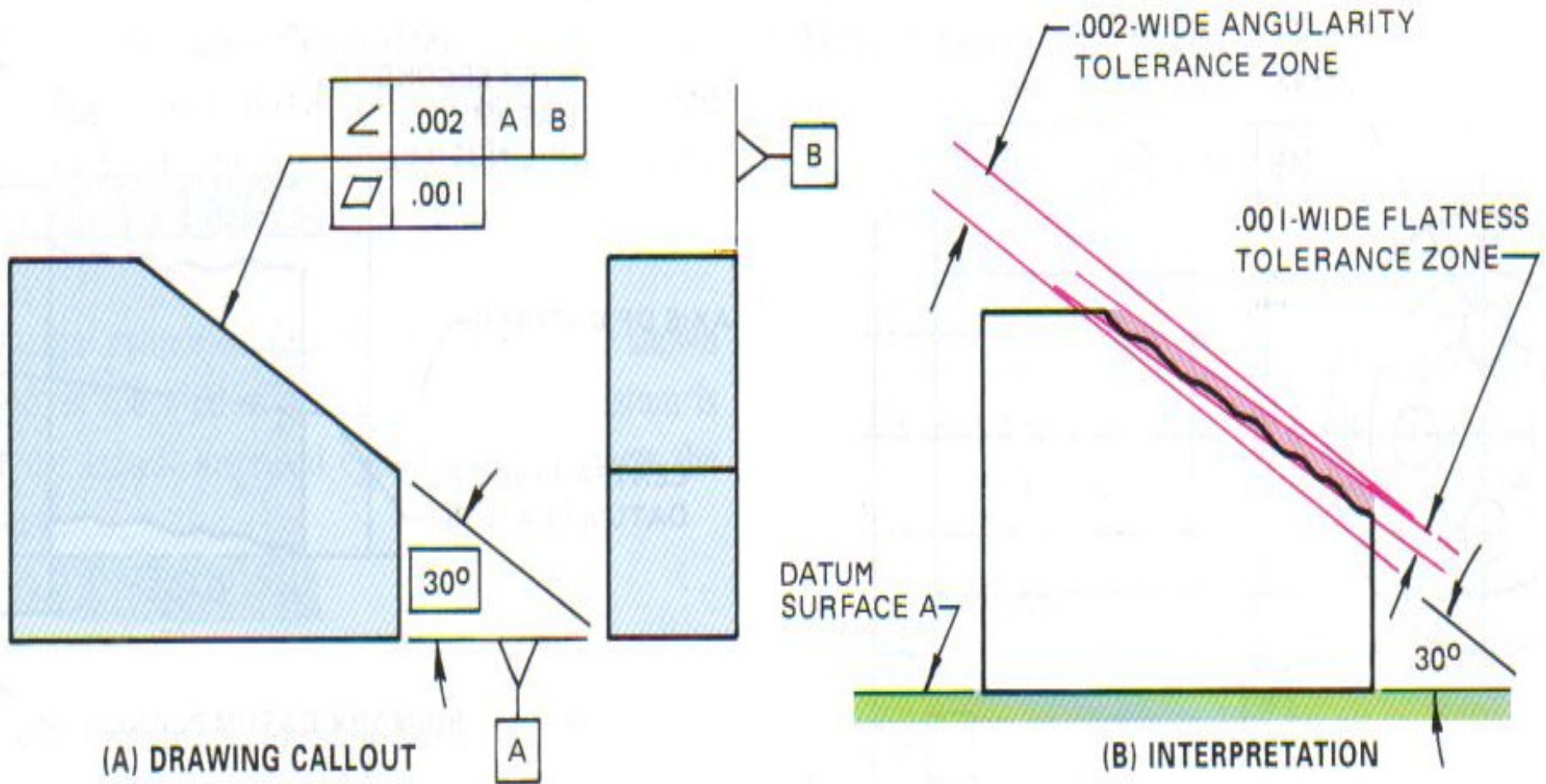


The inclined surface of the part is required to lie between two planes, 0.1 apart, which are inclined at 75° to the datum axis

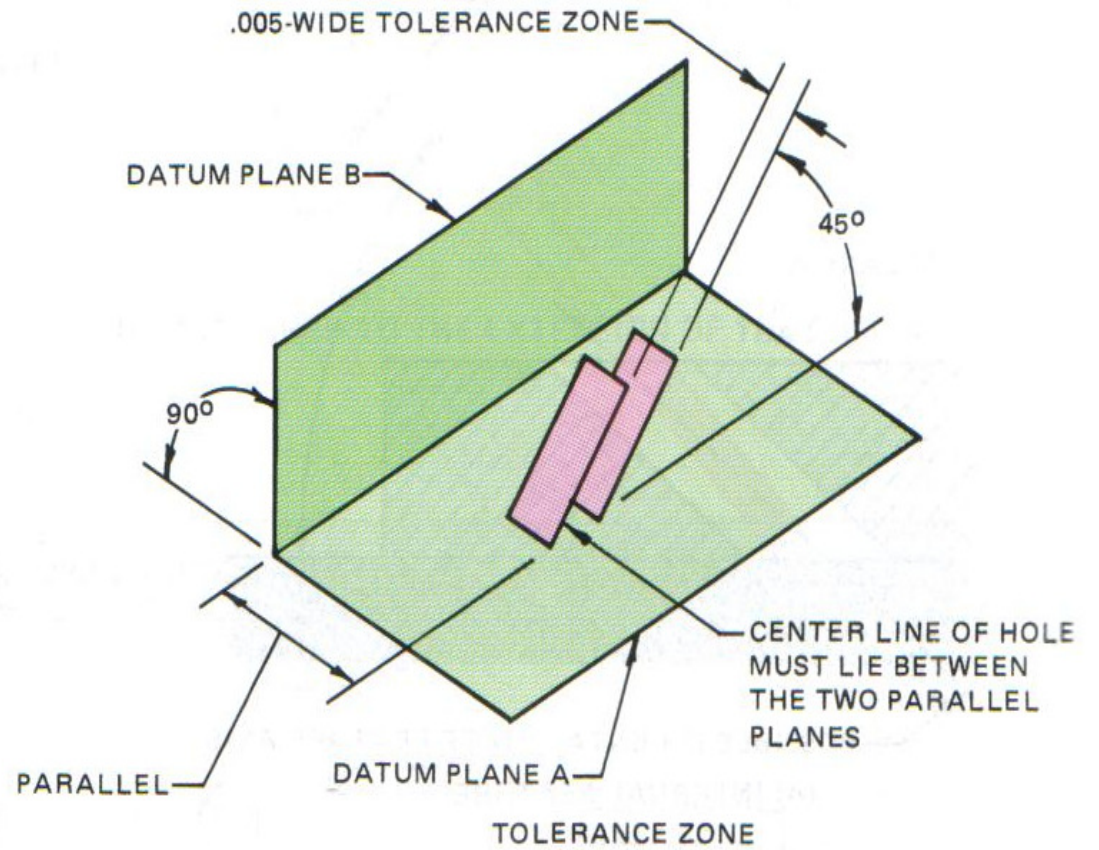
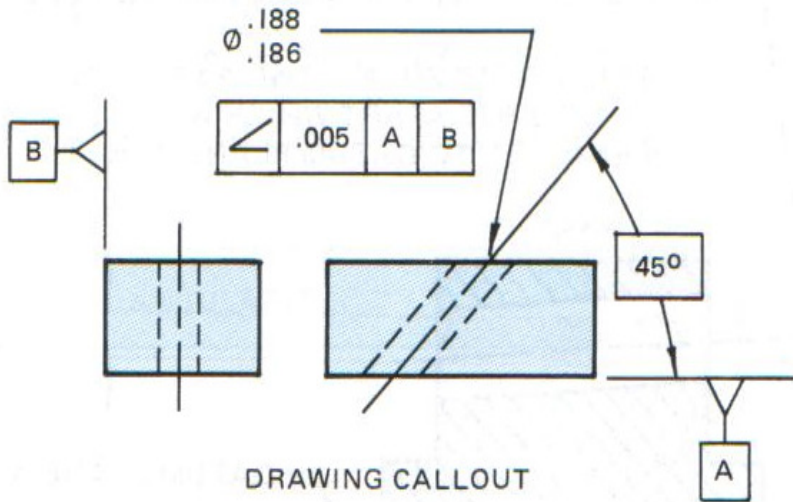
Angularity 4 (of a surface with respect to a datum plane)



The inclined surface of the part is required to lie between two planes 0.03 apart, which are inclined at 39° to the datum plane



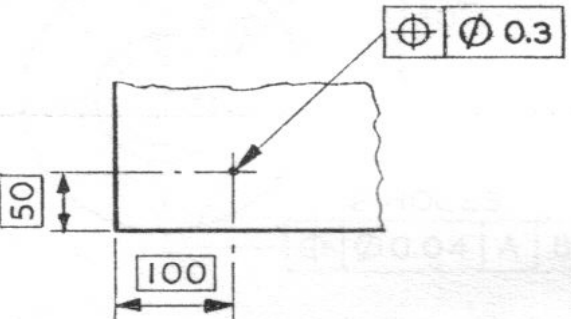
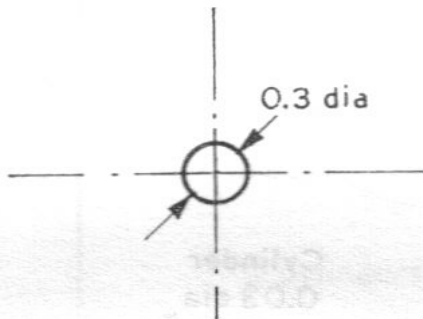
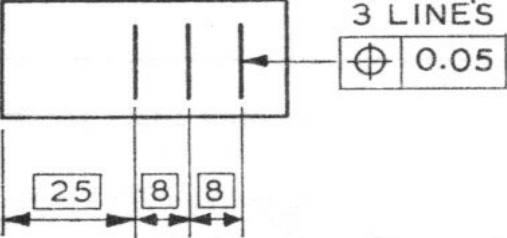
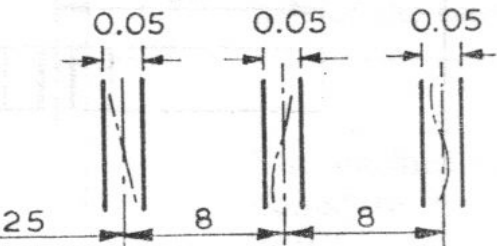
Applying both an angularity and a flatness tolerance to a flat surface.



ANGULARITY TOLERANCE

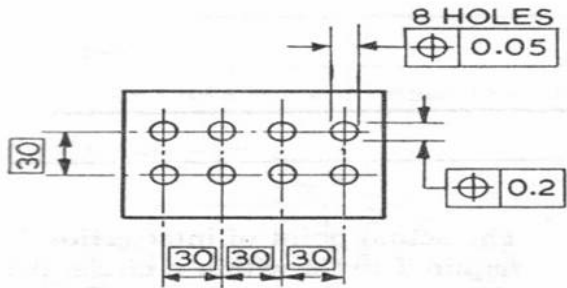
Tolerances of position. A tolerance of position limits the deviation of the position of a feature from its specified true position.

Tolerances of position

Examples	Interpretations
<p><i>Position 1 (of a point)</i></p> 	 <p>The actual point of intersection is required to lie within a circle, 0.3 diameter, in the plane of the surface, which has its centre at the specified true point of intersection. In a case where the point is located by three dimensions (instead of two dimensions in a surface as shown in the example) the tolerance zone is a sphere</p>
<p><i>Position 2 (of a line)</i></p> <p>a.</p> 	 <p>The actual position of each line is required to lie between two parallel straight lines on the surface, 0.05 apart, which are symmetrically disposed about the specified true position of the line</p>

Examples

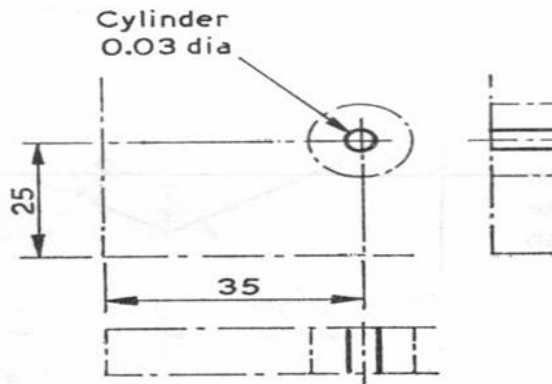
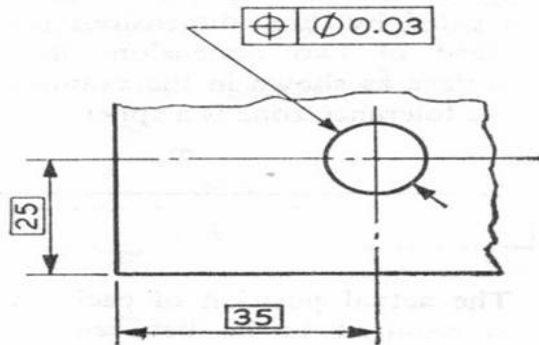
b.



Interpretations

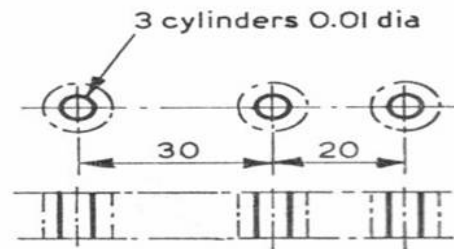
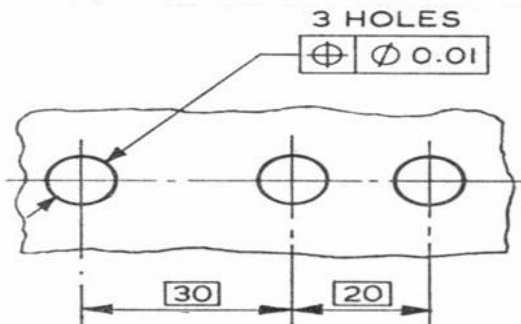
The axis of each of the 8 holes is required to be contained within a parallelepiped, of size 0.2 and 0.05, symmetrically disposed about the specified true position of the axis of the hole*.

c.



The axis of the hole is required to be contained within a cylinder, 0.03 diameter, with its axis in the specified true position of the axis of the hole*

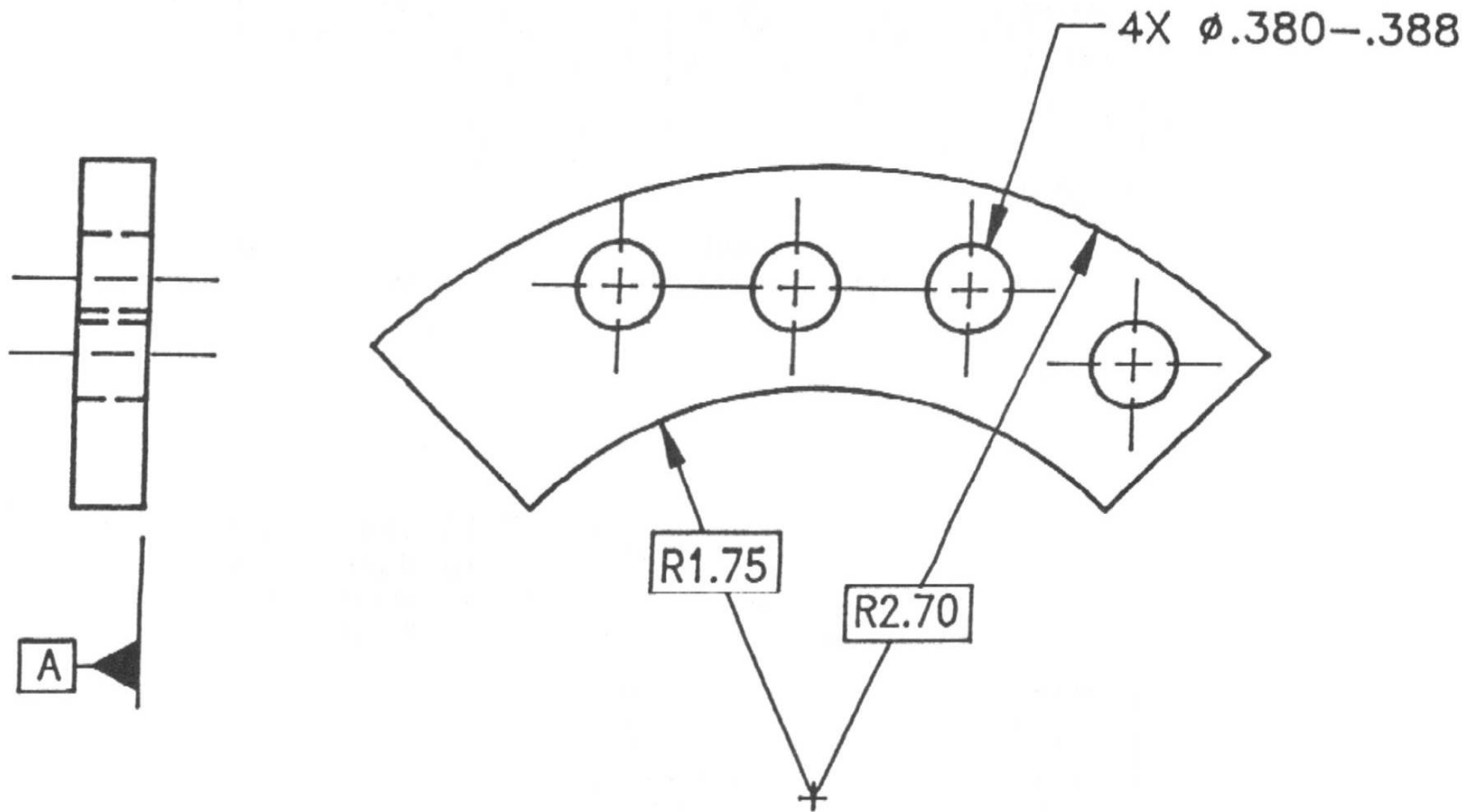
d.

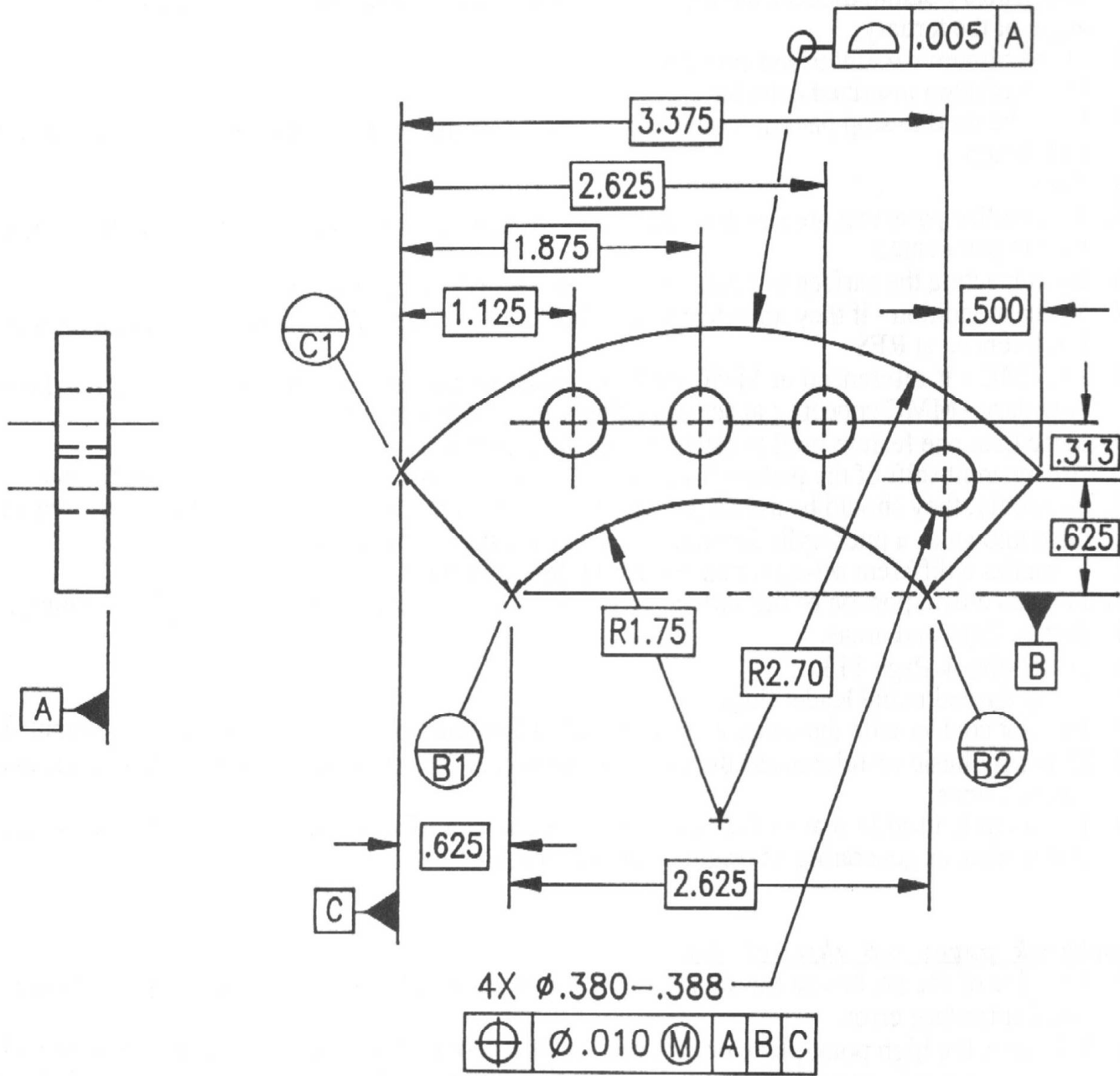


The axis of each hole is required to be contained within a cylinder, 0.01 diameter, with its axis in the specified true position of the axis of the hole*

Use of Profile and Position on Irregular-Shaped Parts

- Profile the outside of this part all around to within .005.
 - Locate the four holes to a datum reference frame that uses a planar surface for a perpendicularity datum and targets for location.
- [Note: Dimensions should be included but do not have to be accurate or per scale. The virtual condition of the mating shafts for the four .380 - .388 holes is .370.]

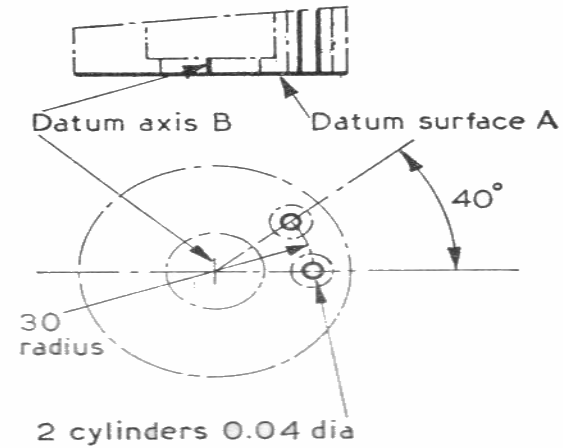
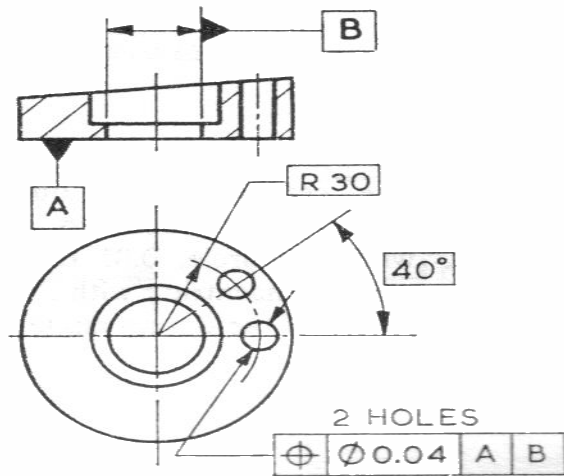




Examples

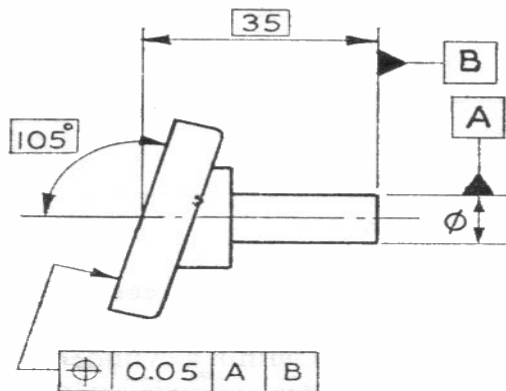
Interpretations

e.



The axes of the two holes are required to be contained within cylinders diameter 0.04, with their axes in the specified true positions of the holes in relation to the datum surface A, and the axis of the central hole B

Position 3 (of a surface)

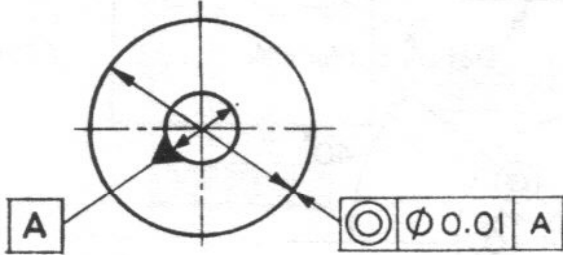
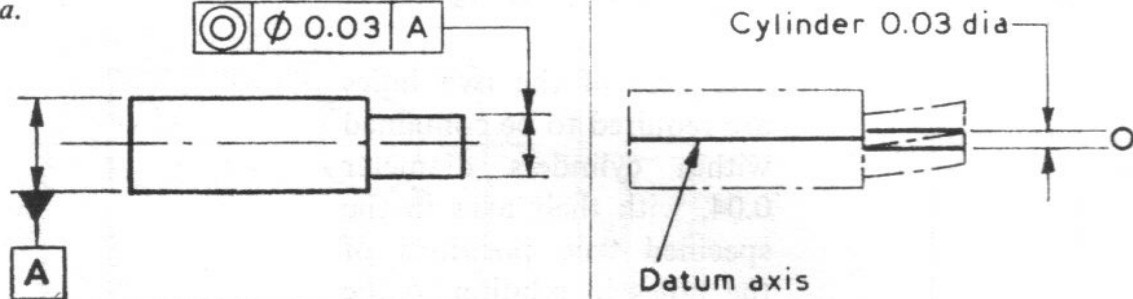


The inclined surface is required to lie between two parallel planes, 0.05 apart, which are symmetrically disposed about the specified true position of the surface in relation to the axis of the right-hand portion and the end

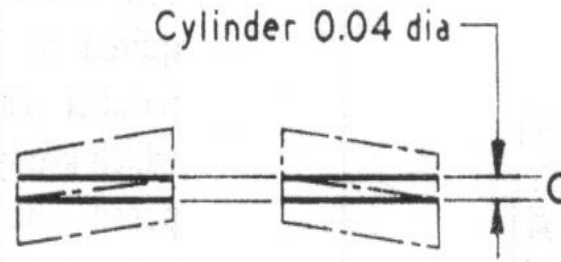
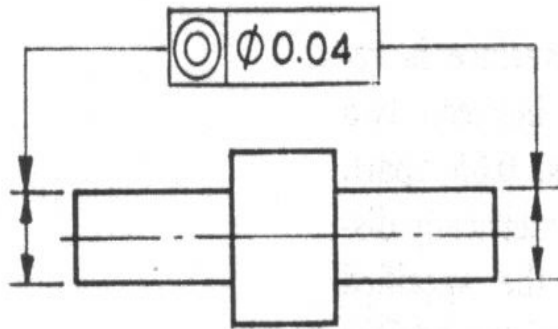
3/16/

Tolerances of concentricity. A concentricity tolerance is a particular case of a positional tolerance in which the toleranced feature and the datum feature are circles or cylinders. The tolerance limits the deviation of the position of the centre or axis of the toleranced feature from its true position, i.e. the centre or axis of the datum feature. The tolerance value is the diameter of the tolerance zone.

Tolerances of concentricity

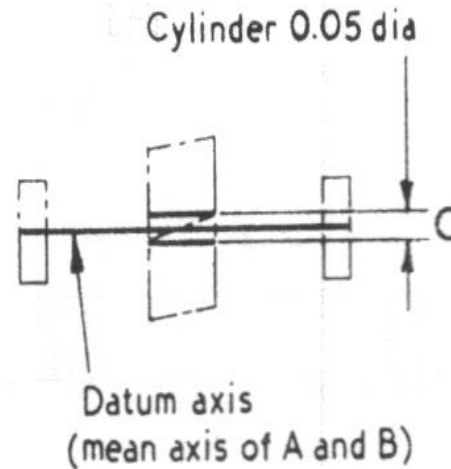
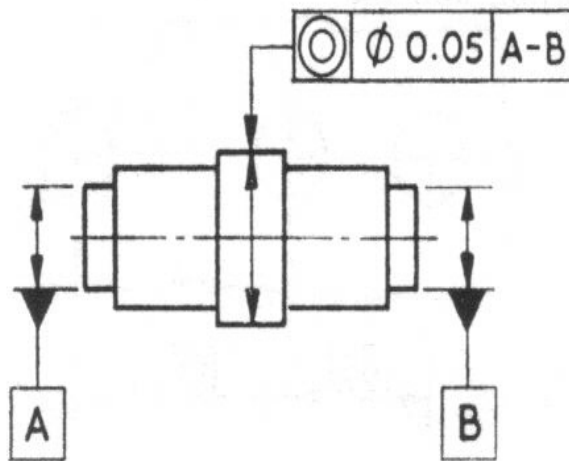
Examples	Interpretations
<p data-bbox="212 516 569 548"><i>Concentricity 1 (of a point)</i></p> 	<p data-bbox="1415 643 1856 837">The centre of the outer circle is required to lie within a circle, 0.01 diameter, concentric with the centre of the datum circle A</p>
<p data-bbox="212 938 548 971"><i>Concentricity 2 (of a line)</i></p> <p data-bbox="212 1008 247 1032">a.</p> 	<p data-bbox="1415 1036 1856 1279">The axis of the right-hand cylindrical portion is required to be contained within a cylinder, 0.03 diameter, co-axial with the left-hand portion</p>

b.



The axes of the left-hand and right-hand cylindrical portions are required to be contained within one cylinder, 0.04 diameter

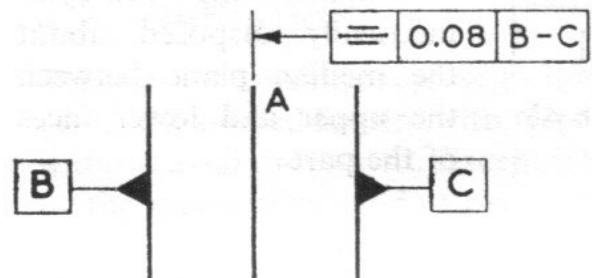
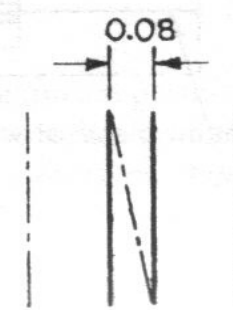
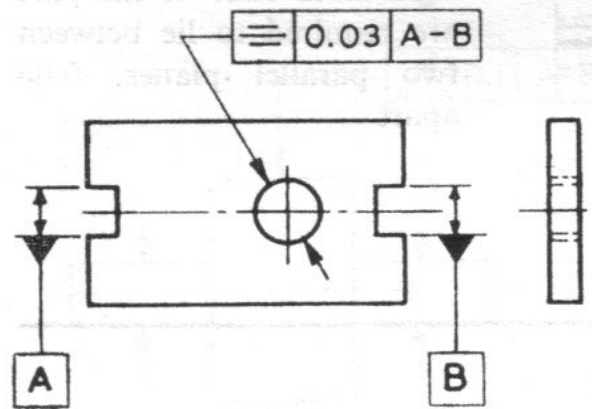
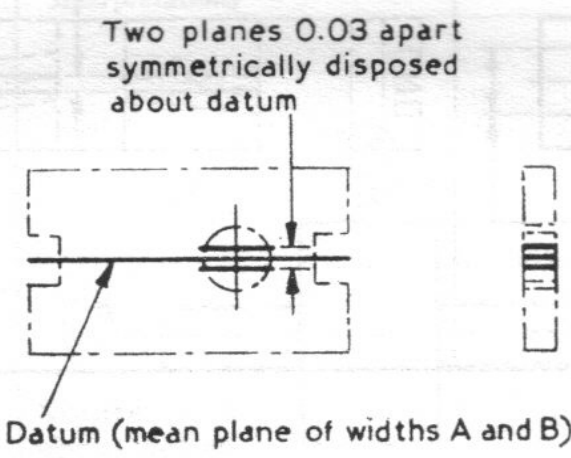
c.



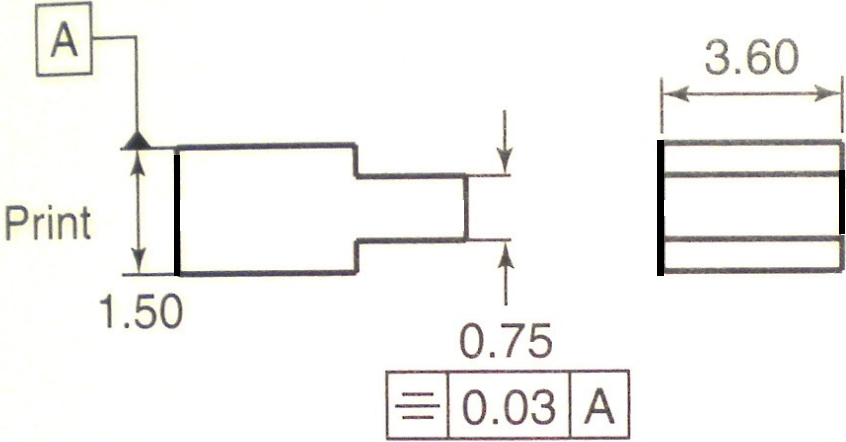
The axis of the central portion is required to be contained within a cylinder, 0.05 diameter, co-axial with the mean axis of the end projections of the part

Tolerances of symmetry. A symmetry tolerance is a particular case of a positional tolerance in which the position of the feature is specified by its symmetrical relationship to a datum

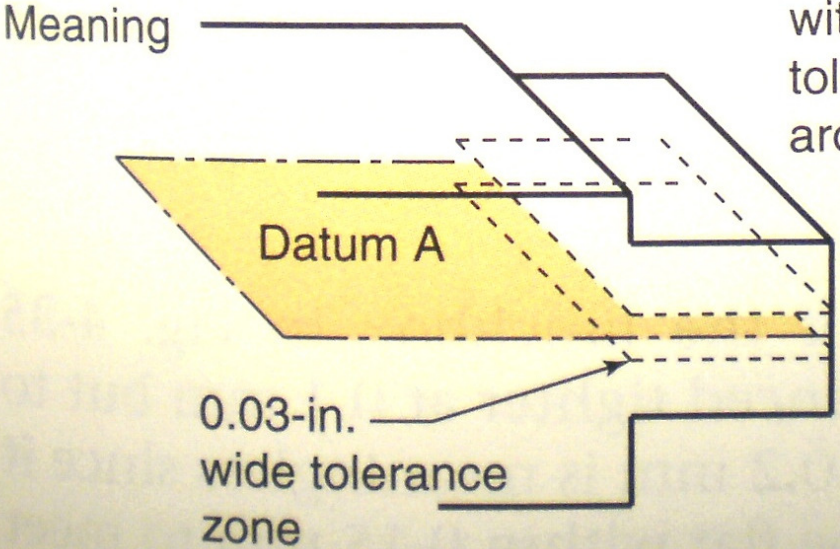
Tolerances of symmetry

Examples	Interpretations
<p><i>Symmetry 1 (of a line)</i></p> <p>a.</p> 	 <p>The line A is required to lie between two parallel straight lines, 0.08 apart, which are symmetrically disposed about the line situated symmetrically between the datum lines B and C</p>
<p>b.</p> 	 <p>Two planes 0.03 apart symmetrically disposed about datum</p> <p>Datum (mean plane of widths A and B)</p> <p>The axis of the hole is required to lie between two parallel planes, 0.03 apart, which are symmetrically disposed about the common median plane of the slots in the ends of the part</p>

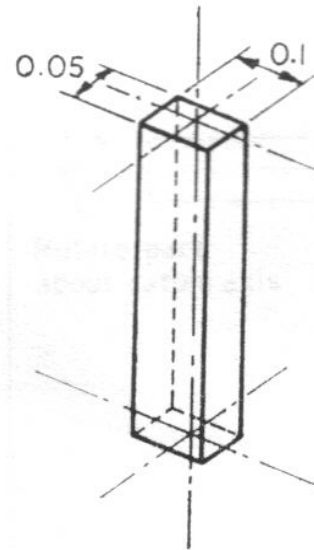
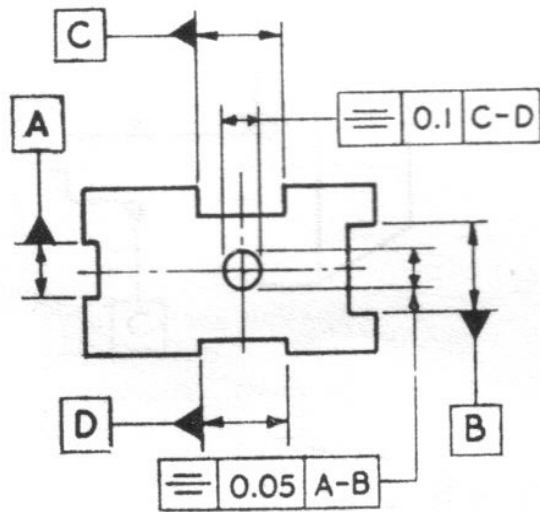
Control of Symmetry



The 0.75 tab's center-plane must fall within a 0.030-in. tolerance zone built around Datum A



c.



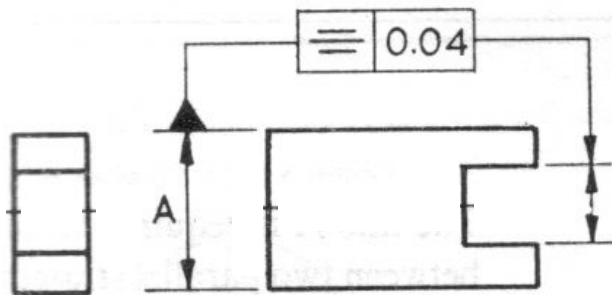
The axis of the hole is required to lie in a parallelepiped, its sides parallel to the longer sides of the part, 0.1 apart, and symmetrically disposed about the common median plane of the slots in the left-hand and right-hand ends of the part and its sides parallel to the shorter sides of the part, 0.1 apart, and symmetrically disposed about the common median plane of the slots in the top and bottom sides

Examples

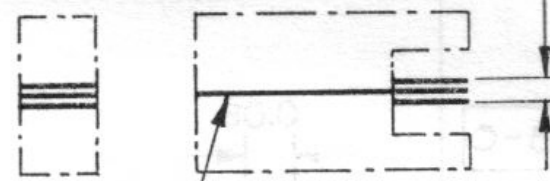
Interpretations

Symmetry 2 (of a median plane)

a.

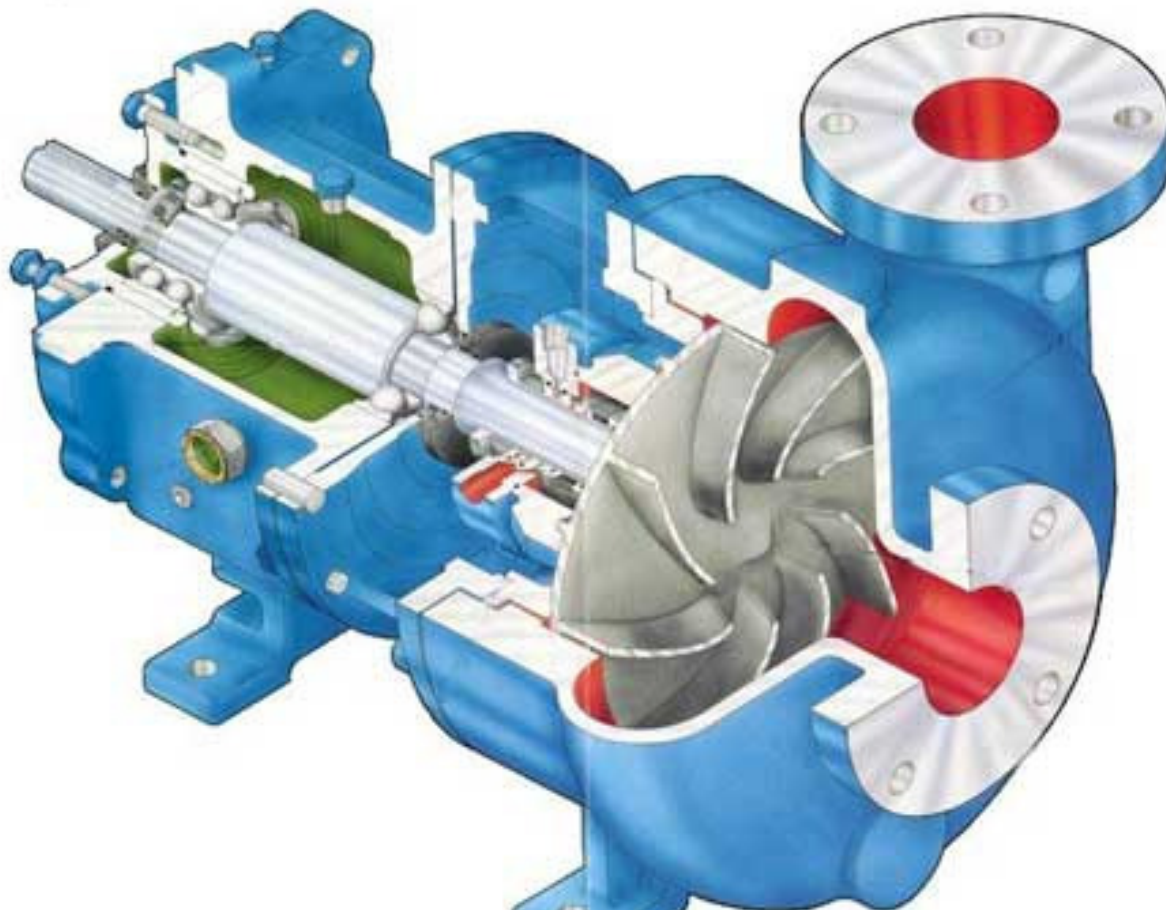
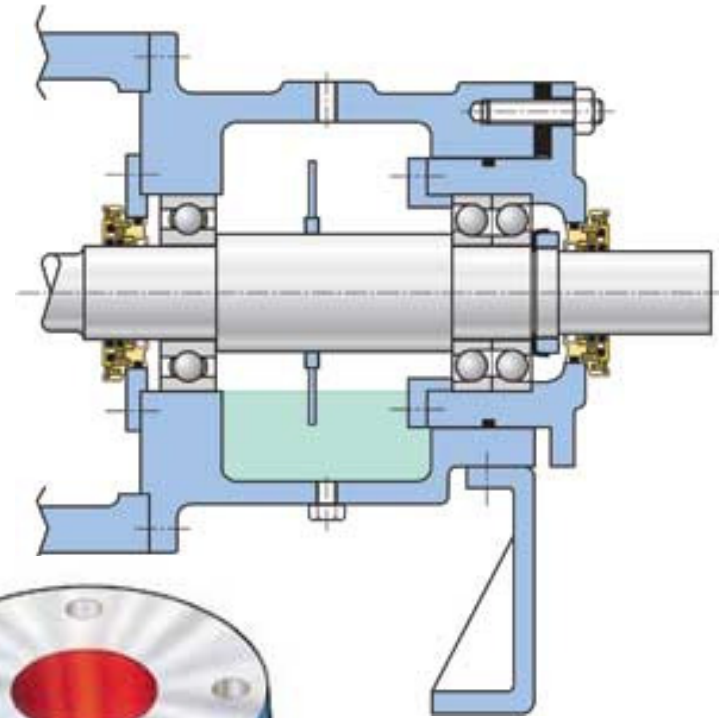
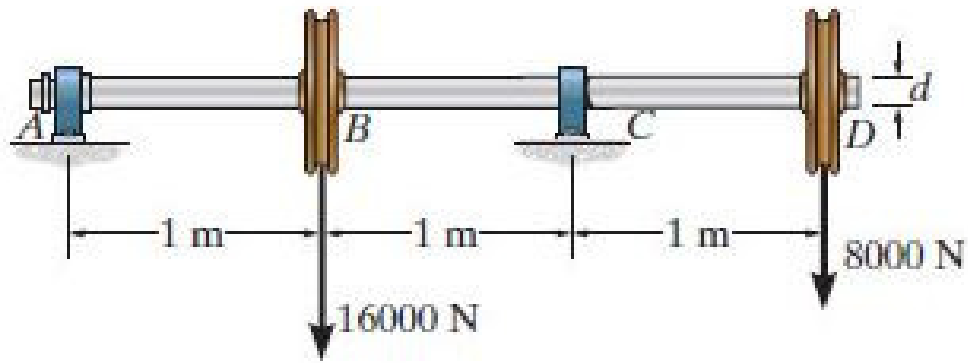


Two planes 0.04 apart symmetrically disposed about the datum



Datum (mean plane of width A)

The median plane of the slot in the right-hand end of the part is required to lie between two parallel planes, 0.04 apart, which are symmetrically disposed about the median plane between the upper and lower faces of the part

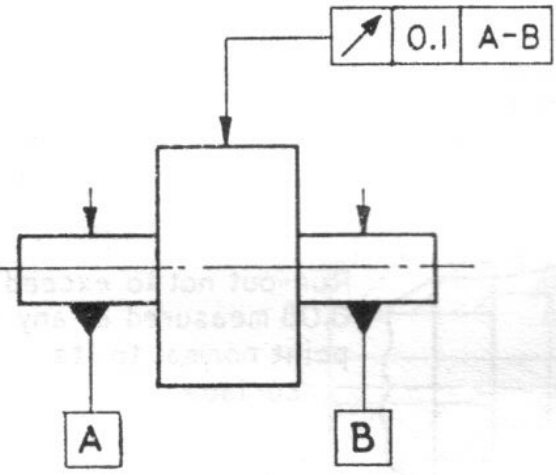
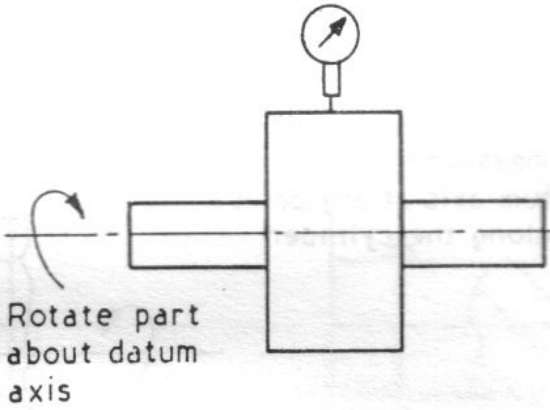


Run-out

Definition

The run-out tolerance represents the maximum permissible variation of position (i.e. full indicator movement) of the considered feature with respect to a fixed point during one complete revolution about the datum axis without axial movement. Except when otherwise stated this variation is measured in the direction indicated by the arrow at the end of the leader line which points to the tolerated feature.

Tolerances of run-out

Examples	Interpretations
<p>a.</p> 	 <p>Rotate part about datum axis</p> <p>Run-out not to exceed 0.1 measured perpendicular to datum axis at any point along the cylinder</p>

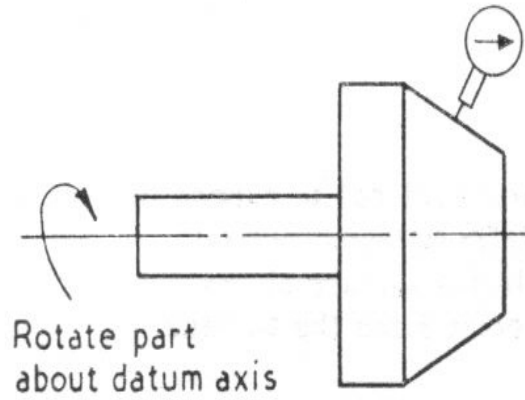
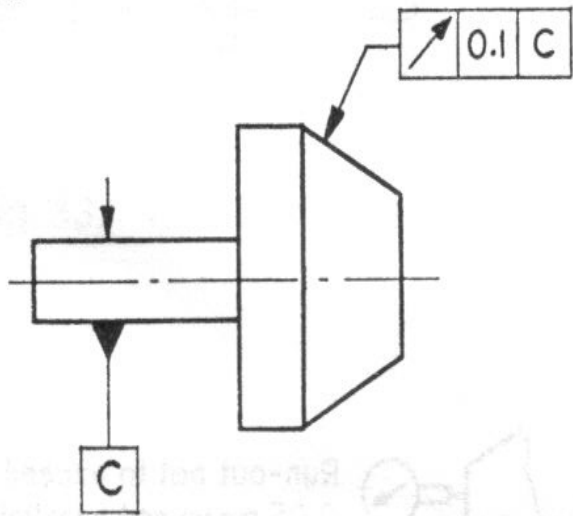


3/16/2019

Dr. Murat Sönmez

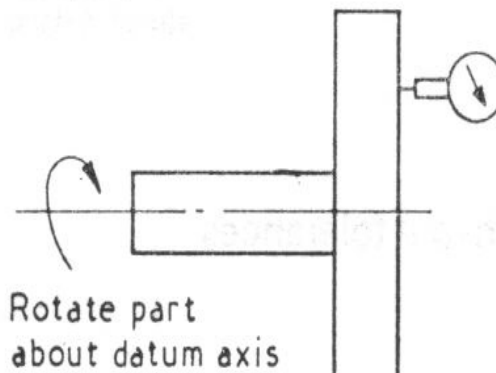
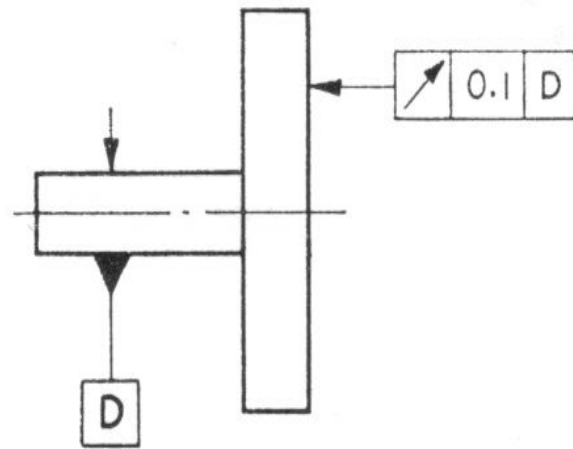
85

b.



Run-out not to exceed 0.1 measured at any point normal to the surface

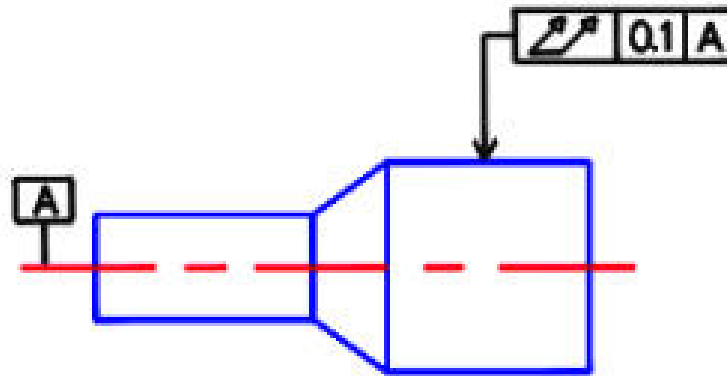
c.



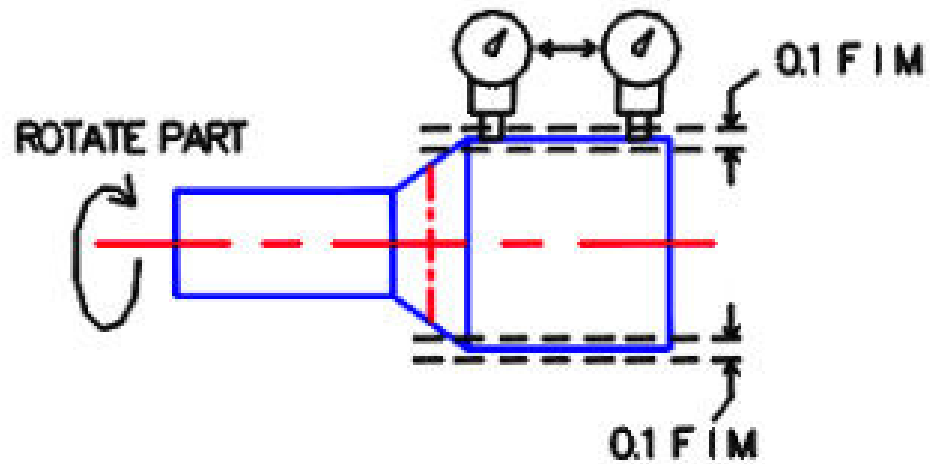
Run-out not to exceed 0.1 measured parallel to the datum axis at any radius

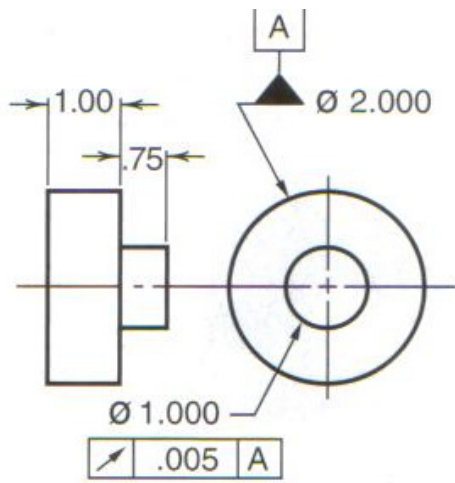


THIS ON A DRAWING

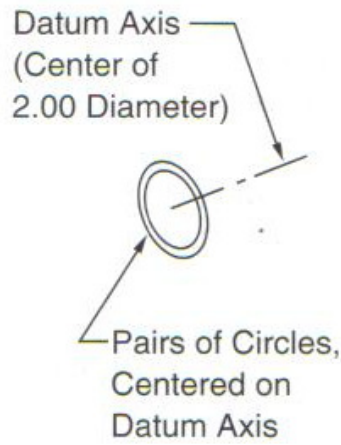


MEANS THIS

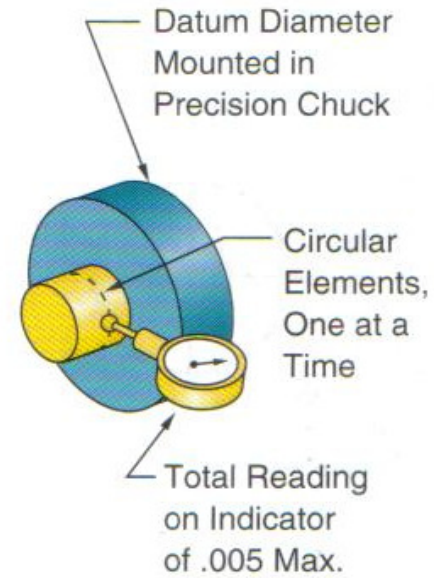




Drawing

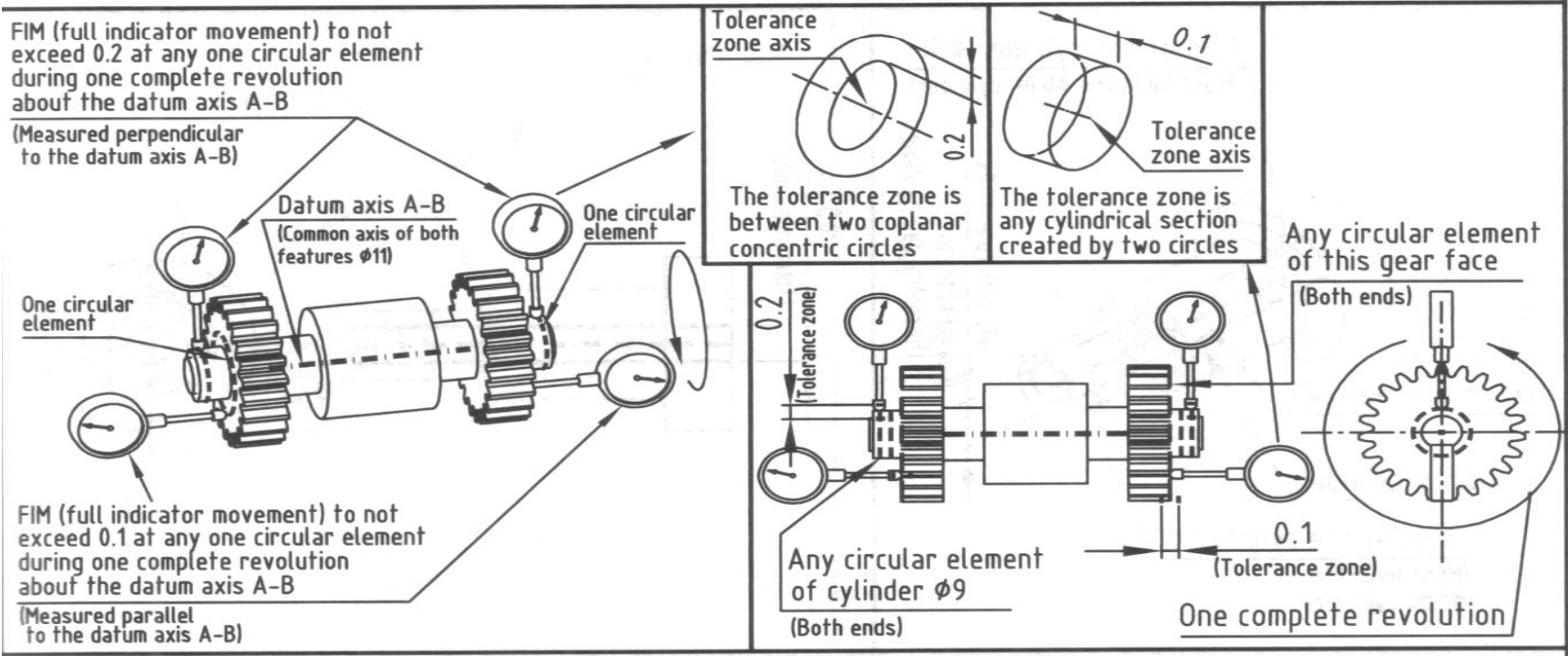
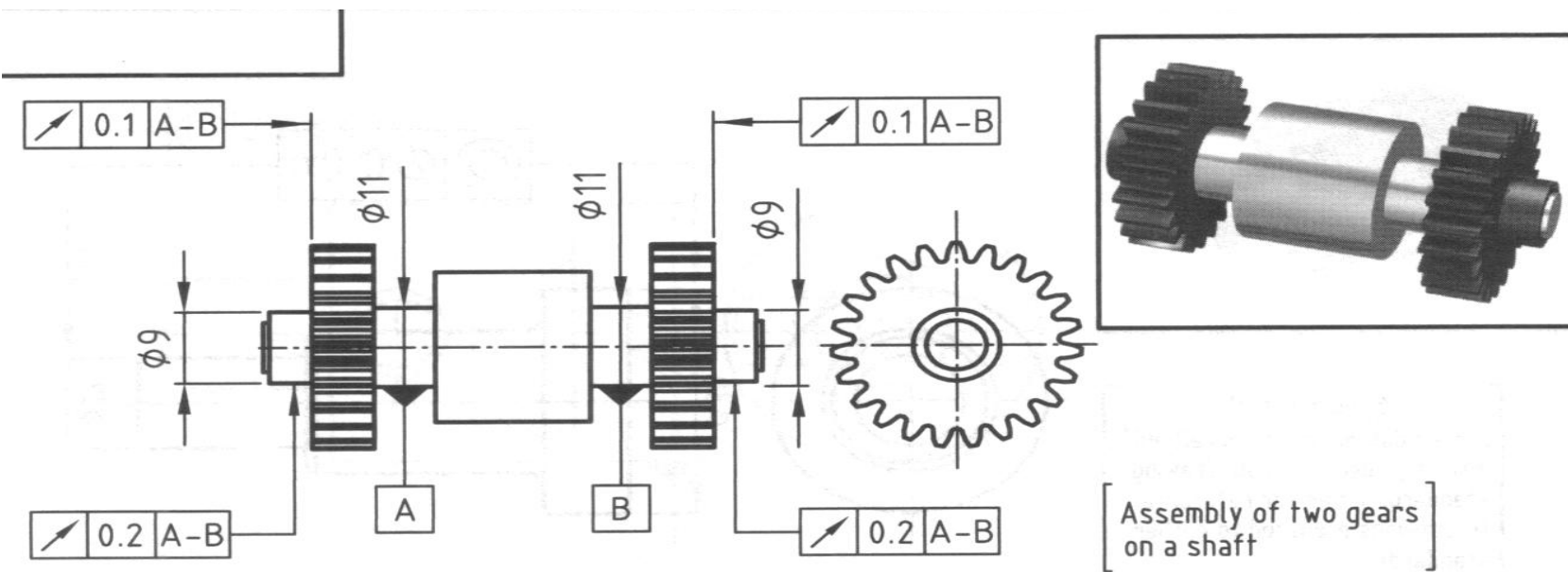


Tolerance Zone



Inspection Method

Circular runout



Run-out as a composite tolerance

Run-out may sometimes be applied as a composite tolerance in place of separate specifications of other geometrical tolerances, e.g. roundness or concentricity; however it should not be so used where the design requirement demands that these characteristics be separately controlled. When required, run-out tolerances may be specified for a part or feature as well as other geometrical tolerances.

Tolerance zone orientation

the width of the run-out tolerance zone lies in the direction of the arrow terminating the leader line. This will often, but not necessarily, be normal to the surface.

Run-out tolerance applied to an assembly

Fig. illustrates the application of run-out tolerance to an assembly of parts.

During one complete revolution of the assembly about the axis defined by the two journals E and F, the radial run-out of the peripheries of the couplings shall not exceed 0.1 and the axial run-out of the faces of the couplings shall not exceed 0.2.

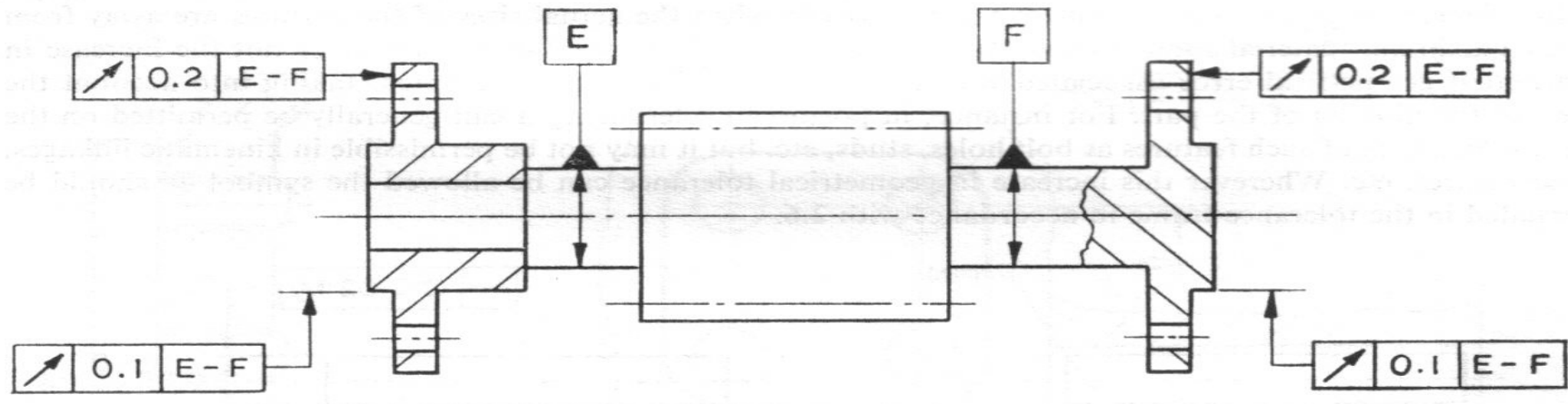
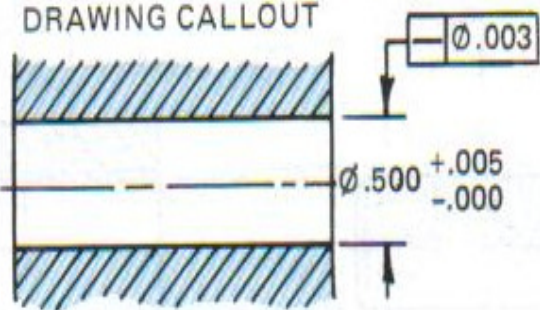
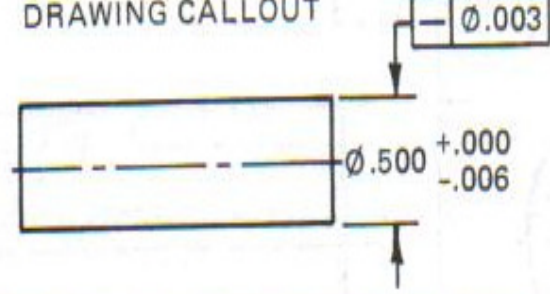
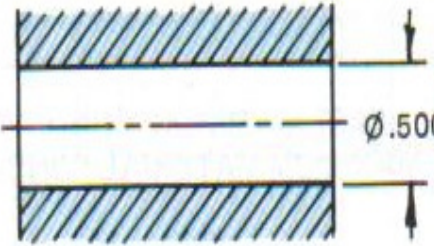

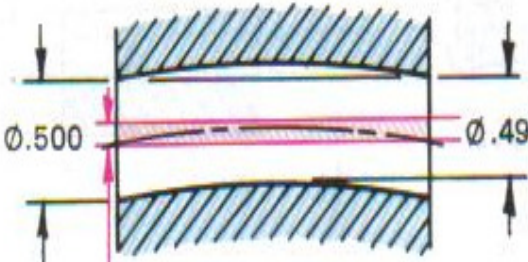
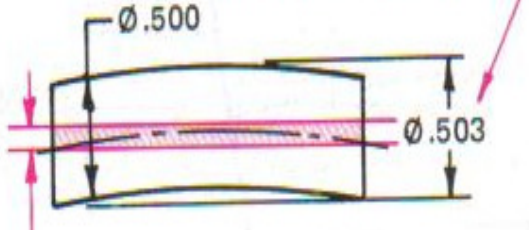
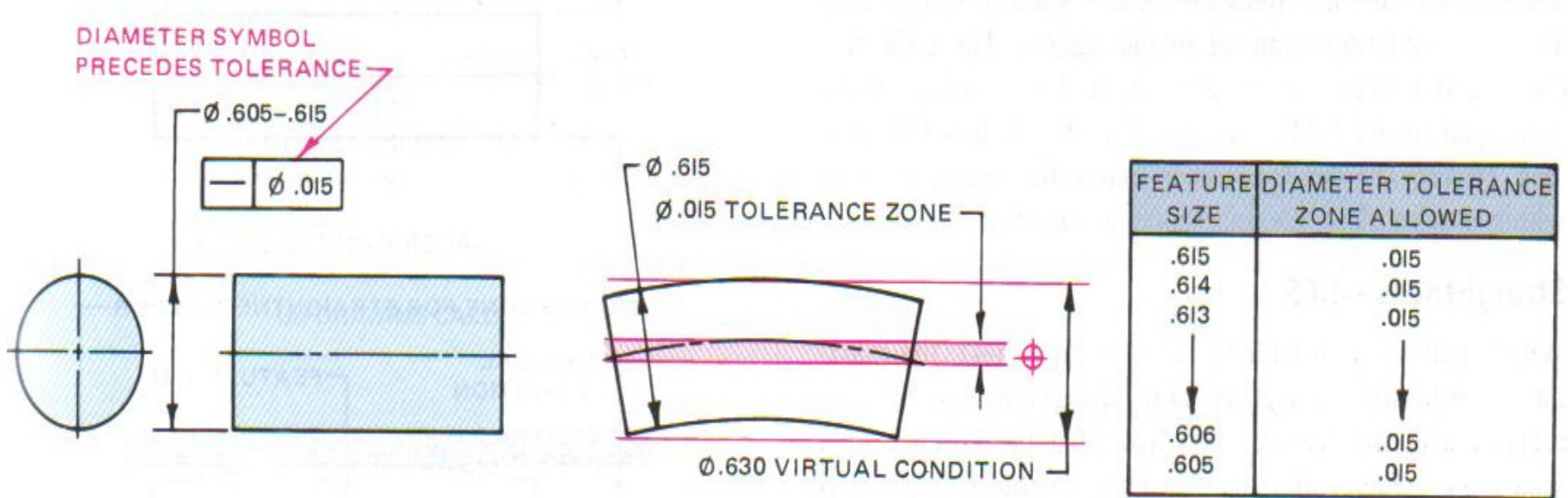


Fig. Run-out tolerance applied to an assembly

INTERNAL FEATURE	EXTERNAL FEATURE
<p>DRAWING CALLOUT</p>  <p>$\phi .500 \begin{matrix} +.005 \\ -.000 \end{matrix}$</p> <p>$\boxed{-\phi .003}$</p>	<p>DRAWING CALLOUT</p>  <p>$\phi .500 \begin{matrix} +.000 \\ -.006 \end{matrix}$</p> <p>$\boxed{-\phi .003}$</p>
<p>MAXIMUM MATERIAL CONDITION = MINIMUM PERMISSIBLE DIAMETER</p>  <p>$\phi .500$</p> <p>NOTE-LEAST MATERIAL CONDITION $\phi .505$</p>	<p>MAXIMUM MATERIAL CONDITION = LARGEST PERMISSIBLE DIAMETER</p>  <p>$\phi .500$</p> <p>NOTE-LEAST MATERIAL CONDITION $\phi .494$</p>
<p>VIRTUAL CONDITION</p>  <p>$\phi .500$</p> <p>$\phi .497$</p> <p>$\phi .003$ TOLERANCE ZONE</p>	<p>VIRTUAL CONDITION</p>  <p>$\phi .500$</p> <p>$\phi .503$</p> <p>$\phi .003$ TOLERANCE ZONE</p>

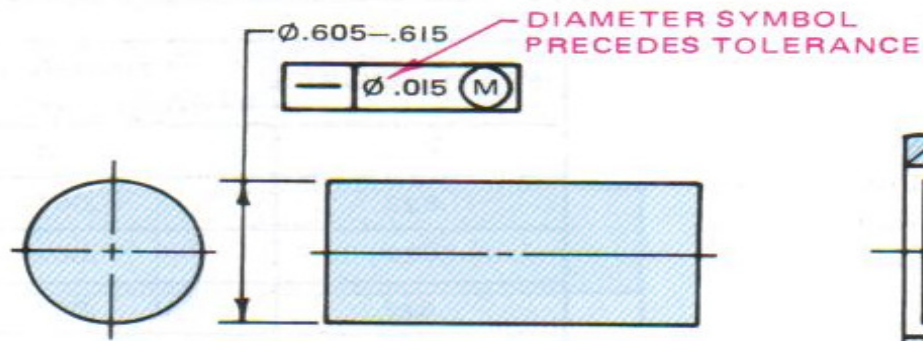
Maximum material and virtual conditions.



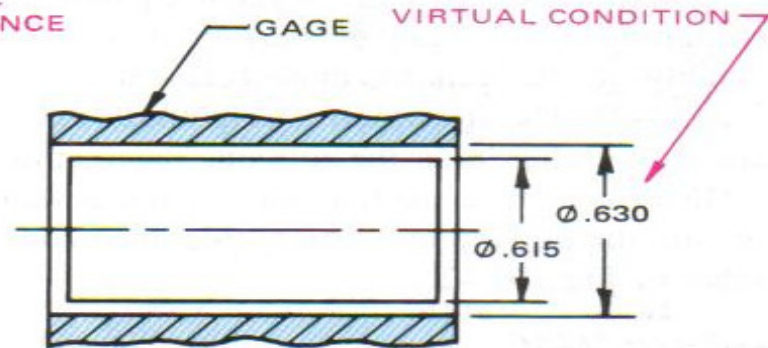
(A) DRAWING CALLOUT

Specifying straightness—RFS.

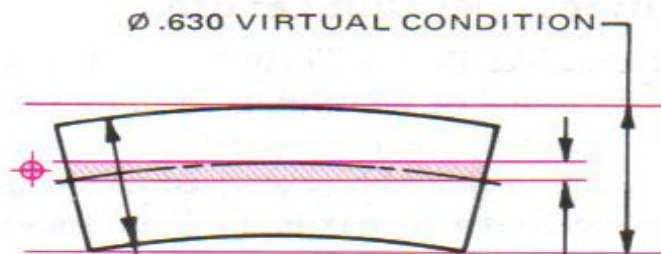
(B) INTERPRETATION



(A) DRAWING CALLOUT

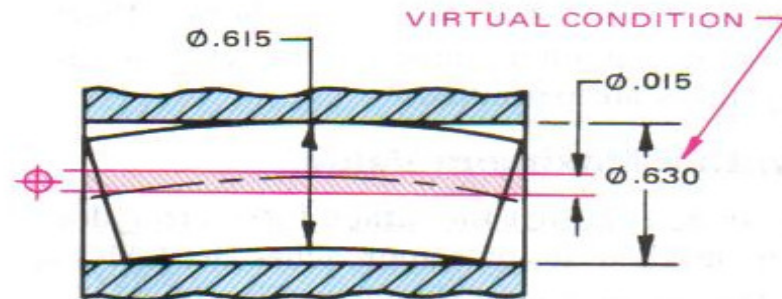


THE MAXIMUM DIAMETER OF THE PIN WITH PERFECT FORM IN A GAGE

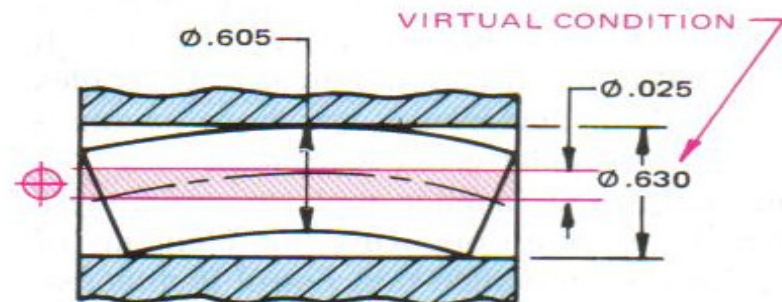


FEATURE SIZE	DIAMETER TOLERANCE ZONE ALLOWED
.615	.015
.614	.016
.613	.017
↓	↓
.606	.024
.605	.025

(B) INTERPRETATION

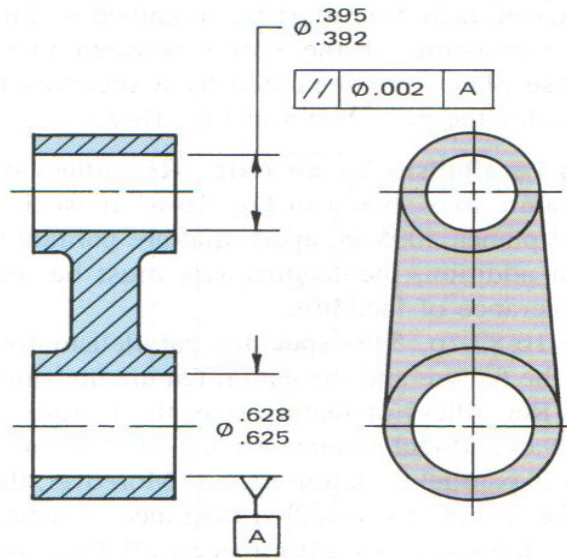


WITH PIN AT MAXIMUM DIAMETER (.615), THE GAGE WILL ACCEPT THE PIN WITH UP TO .015 IN. VARIATION IN STRAIGHTNESS

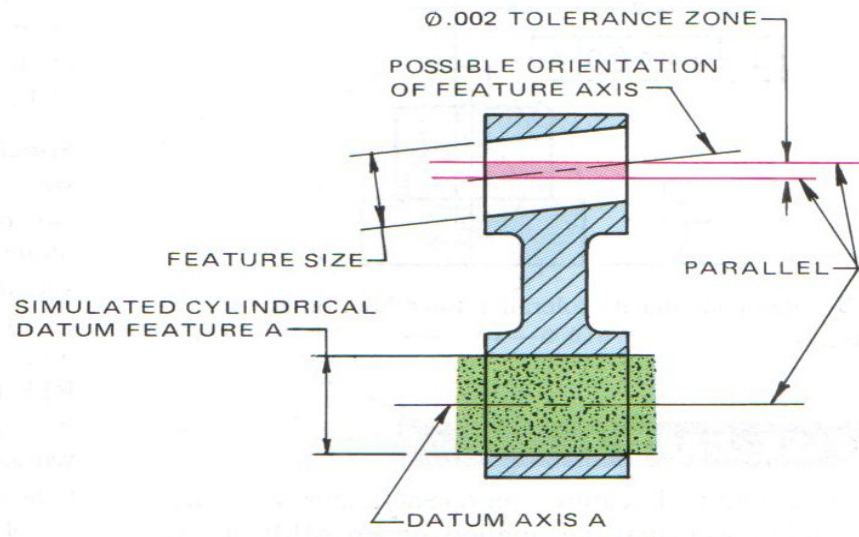


WITH PIN AT MINIMUM DIAMETER (.605), THE GAGE WILL ACCEPT THE PIN WITH UP TO .025 IN. VARIATION IN STRAIGHTNESS

(C) ACCEPTANCE BOUNDARY

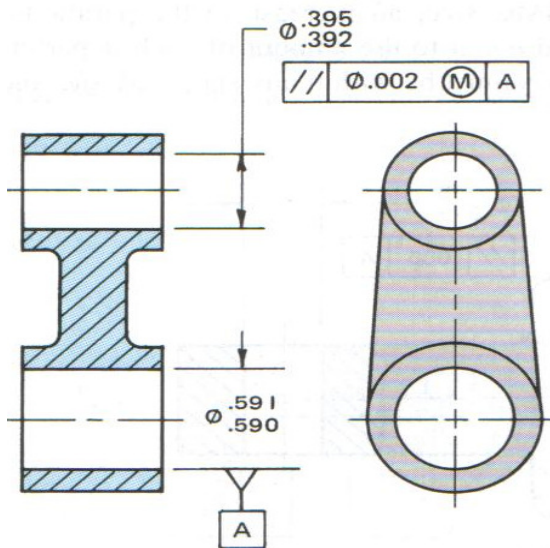


(A) DRAWING CALLOUT

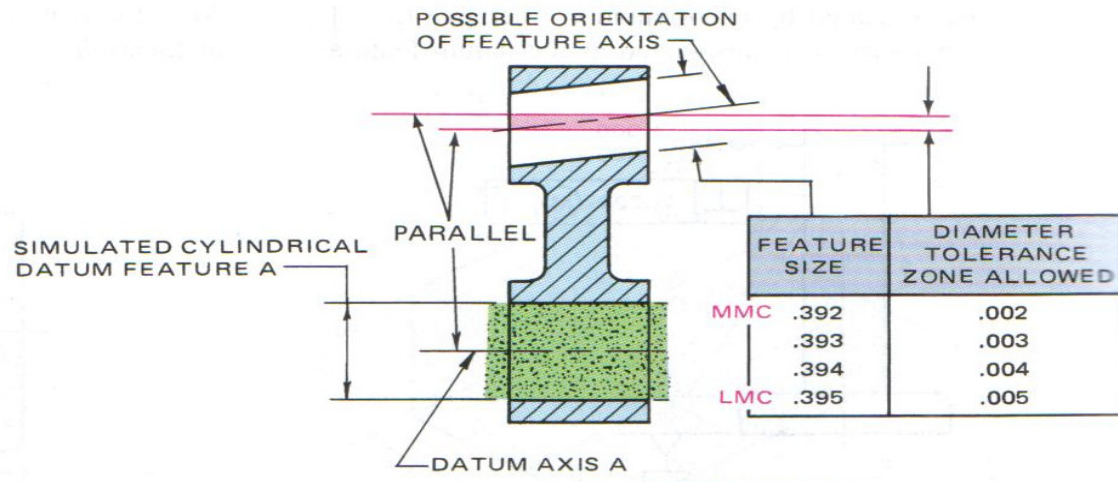


(B) INTERPRETATION

Specifying parallelism for an axis (both feature and datum feature RFS).

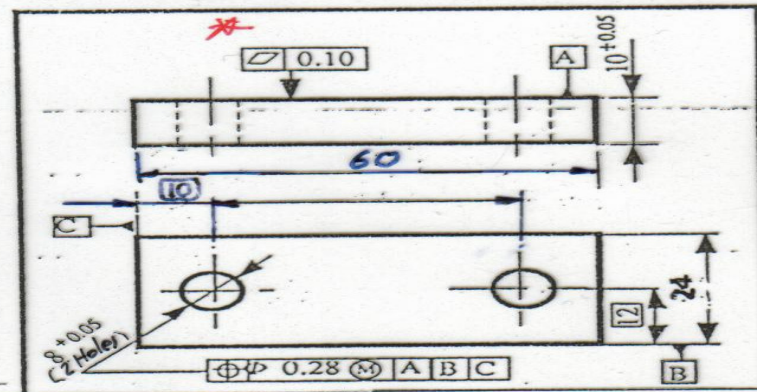
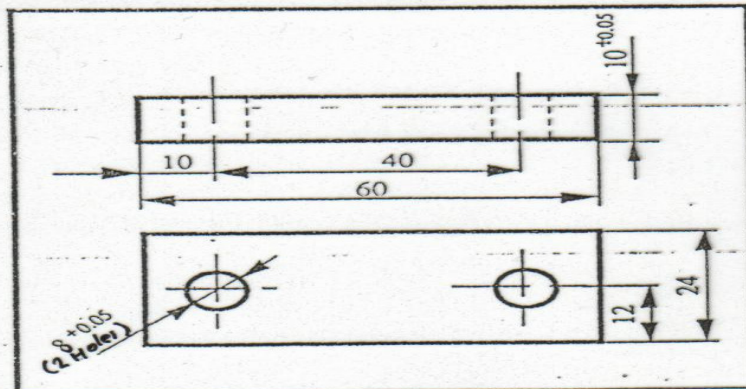


(A) DRAWING CALLOUT



(B) INTERPRETATION

Specifying parallelism for an axis (feature at MMC and datum feature RFS).



If dia. = 8.00 material becomes maximum. [mm]

the given position tolerance is to be satisfied in this case

If the actual size is greater than the minimum limit, the position tolerance must be determined as follows:

eg. actual size 8.03

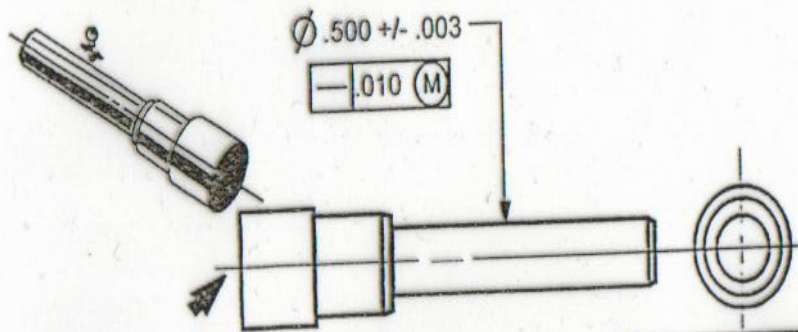
$$|8.03 - 8.00| = 0.03$$

$$\text{tolerance} = 0.28 + 0.03 = 0.31 \text{ [mm]}$$

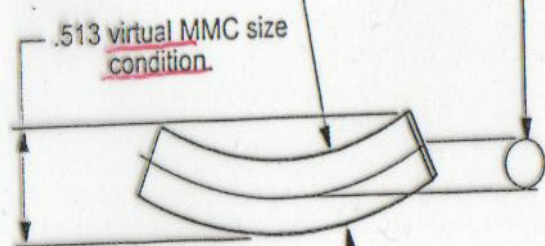
eg. actual size 8.05

$$|8.05 - 8.00| = 0.05$$

$$\text{tolerance} = 0.28 + 0.05 = 0.33 \text{ [mm]}$$

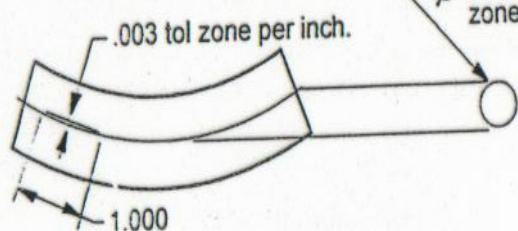
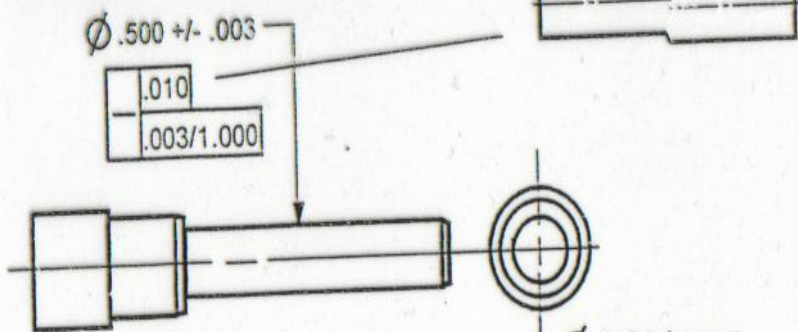


Straightness-Axis MMC.



Size	Tol Zone
.503 MMC	.010
.502	.011
.501	.012
.500	.013
.499	.014
.497	.016

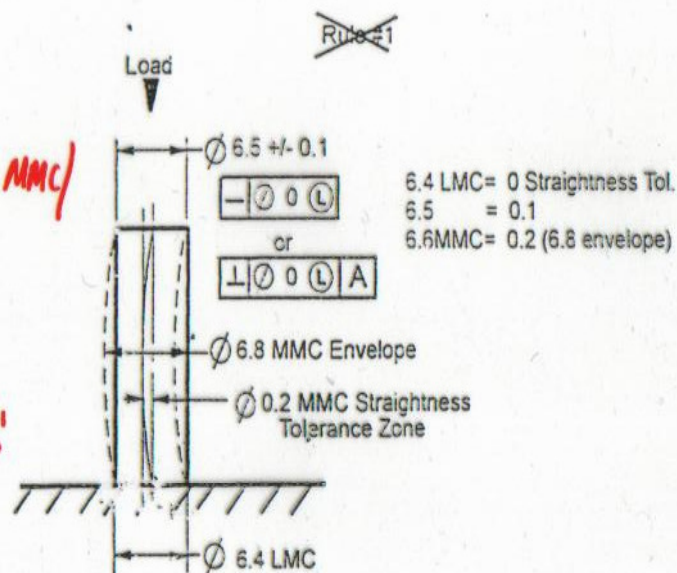
Straightness-Axis per unit length RFS.



Straightness - axis MMC and per unit length.

(Actual size - Size at MMC) + Geo. tol.

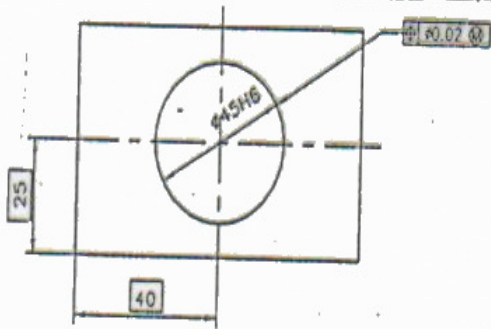
Virtual condition: is the boundary generated by the collective effects of MMC (or LMC) size and geo. tol.



Note: Where a straightness tolerance is used in conjunction with an orientation or position tolerance, the straightness tolerance value shall be no greater than the specified orientation (or position) tolerance value.

Straightness applied LMC.

EX: a) Measured diameter of the hole is 45.010. Determine the position tolerance



b). Determine the maximum value of the position tolerance permitted

a). $\phi 45 H6 = \phi 45_{0}^{0.016}$

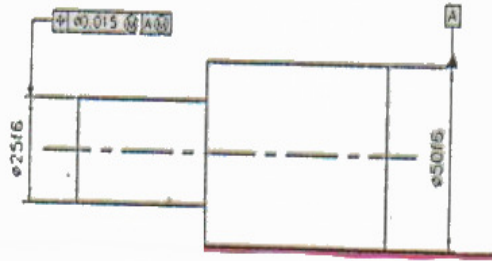
when the hole has been produced to minimum diameter, 45.000 (mm), the object will have maximum amount of material

b). The maximum value of the position tolerance is to be applied when the object has been produced to minimum amount of material (i.e. when the hole is in its maximum size) Therefore tolerance

$|45.010 - 45.000| = 0.01$ [mm] is to be added to the given position tolerance for the measured size of the hole the corresponding tolerance = $0.02 + 0.01 = 0.03$ [mm]

Therefore tolerance_{max} = $0.02 + |45.016 - 45.000| = 0.02 + 0.016 = 0.036$ [mm]

Ex: If the measured diameters are 26.970 & 49.965 , determine the position tolerance to be applied.

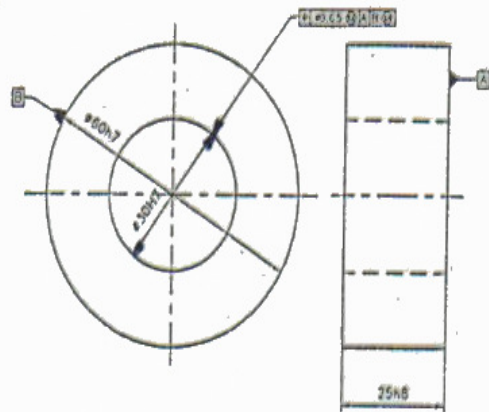


Solution $\phi 25 f6 = \phi 25 \begin{matrix} -0.020 \\ -0.033 \end{matrix}$, $\phi 50 f6 = \phi 50 \begin{matrix} -0.025 \\ -0.041 \end{matrix} \Rightarrow \begin{matrix} 49.975 \\ 49.959 \end{matrix}$

$\Rightarrow \begin{matrix} 24.980 \\ 24.967 \end{matrix}$

Position Tolerance = $0.015 + |24.970 - 24.980| + |49.965 - 49.975| = 0.035 \text{ (mm)}$

Ex:



Determine the maximum value of the position tolerance which may be in consideration.

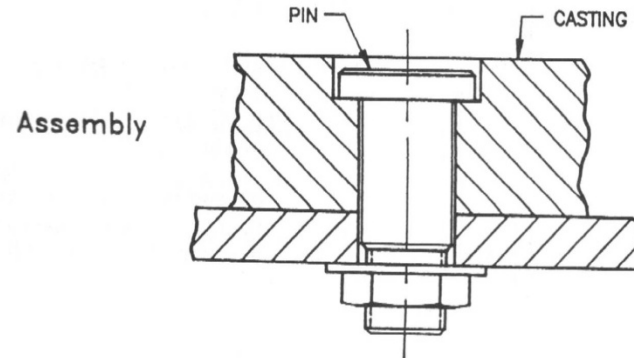
Solution: $\phi 30 H7 = \phi 30 \begin{matrix} 0.021 \\ 0.000 \end{matrix} \Rightarrow \begin{matrix} 30.021 \\ 30.000 \end{matrix}$

$\phi 60 h7 = \phi 60 \begin{matrix} 0.000 \\ -0.030 \end{matrix} \Rightarrow \begin{matrix} 60.000 \\ 59.970 \end{matrix}$

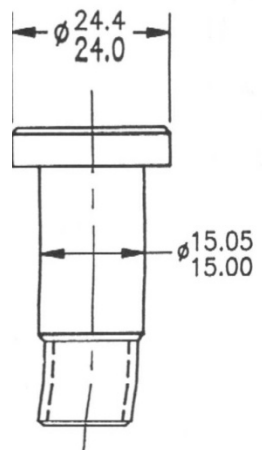
max. value of the position tolerance,

$= 0.05 + |30.021 - 30.000| + |59.970 - 60.000| = 0.101$

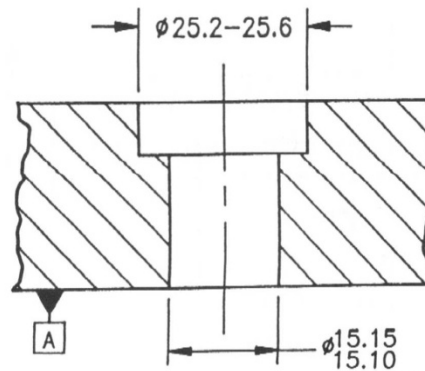
- Coaxiality
- Mating Part Design



Detail drawing callouts



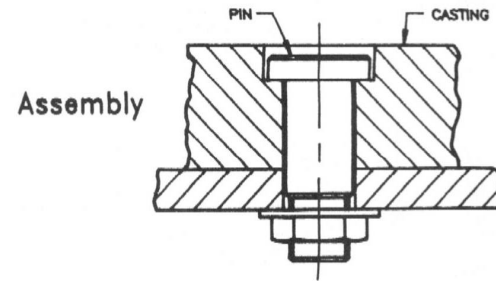
PIN



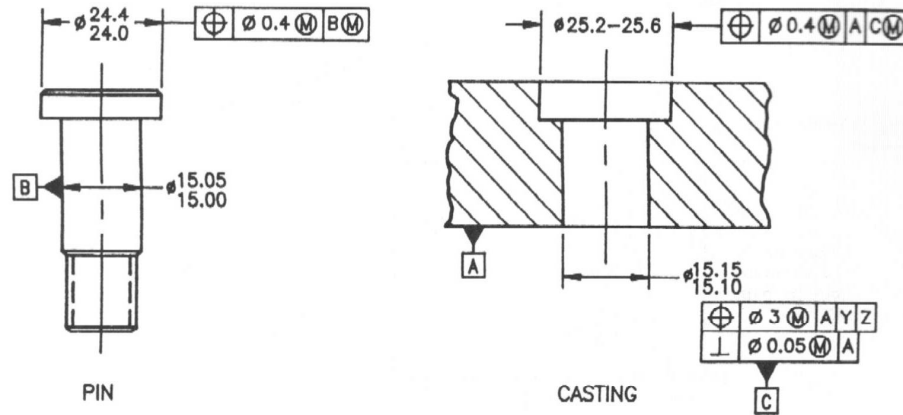
CASTING

\oplus	$\varnothing 3$	(M)	A	Y	Z
\perp					

- Assign appropriate coaxiality controls to assure these two parts will mate at assembly.
- Fill in the perpendicularity control.

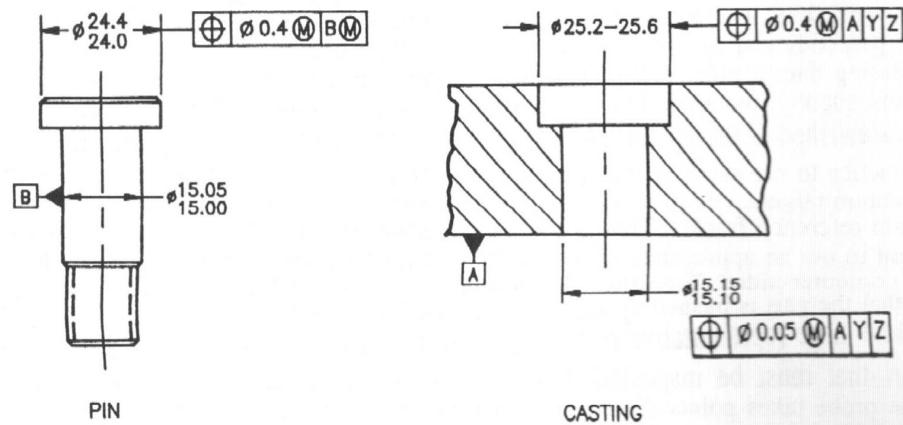


Example 1: Direct Tolerancing on Casting



VS

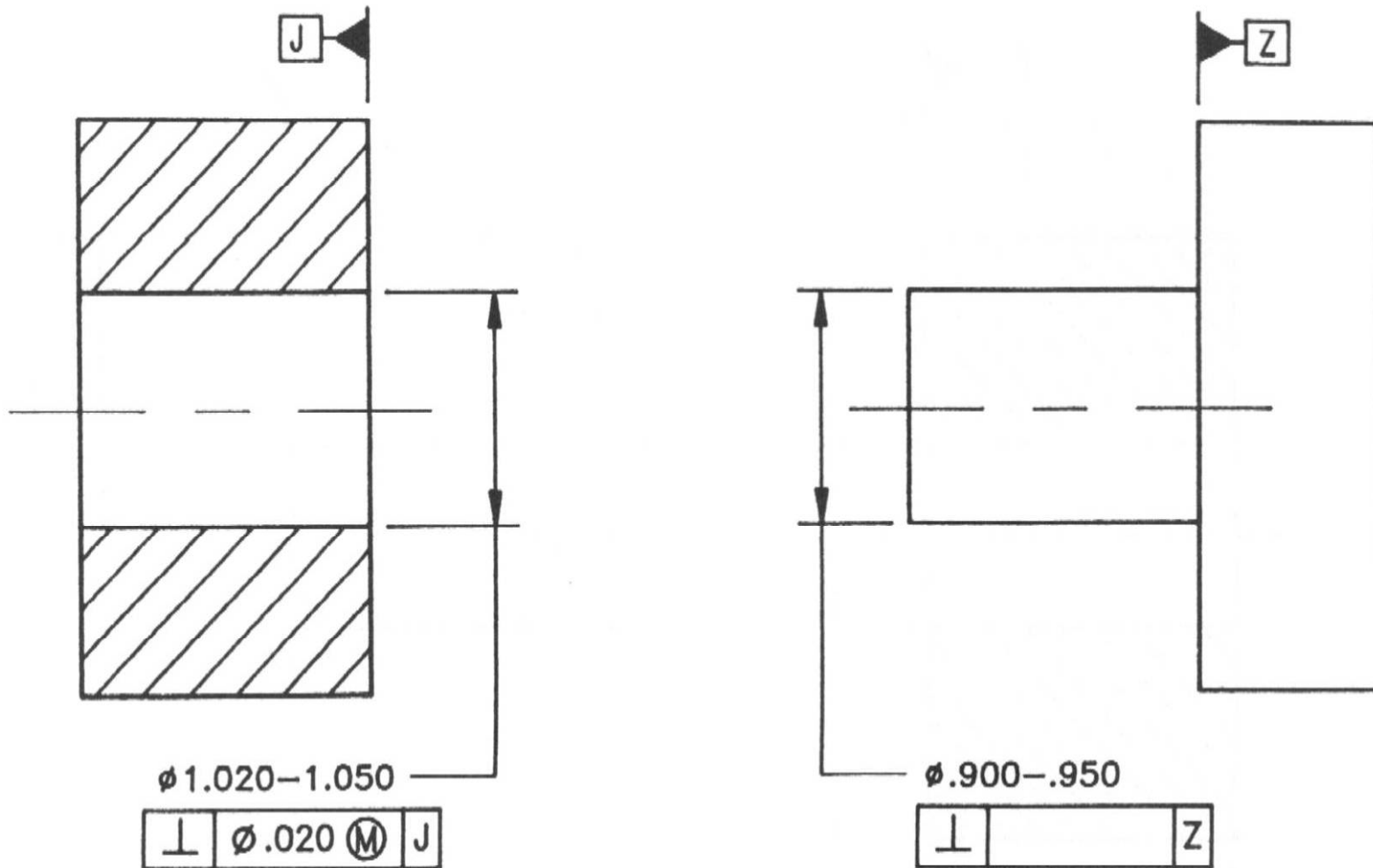
Example 2: Indirect Tolerancing on Casting

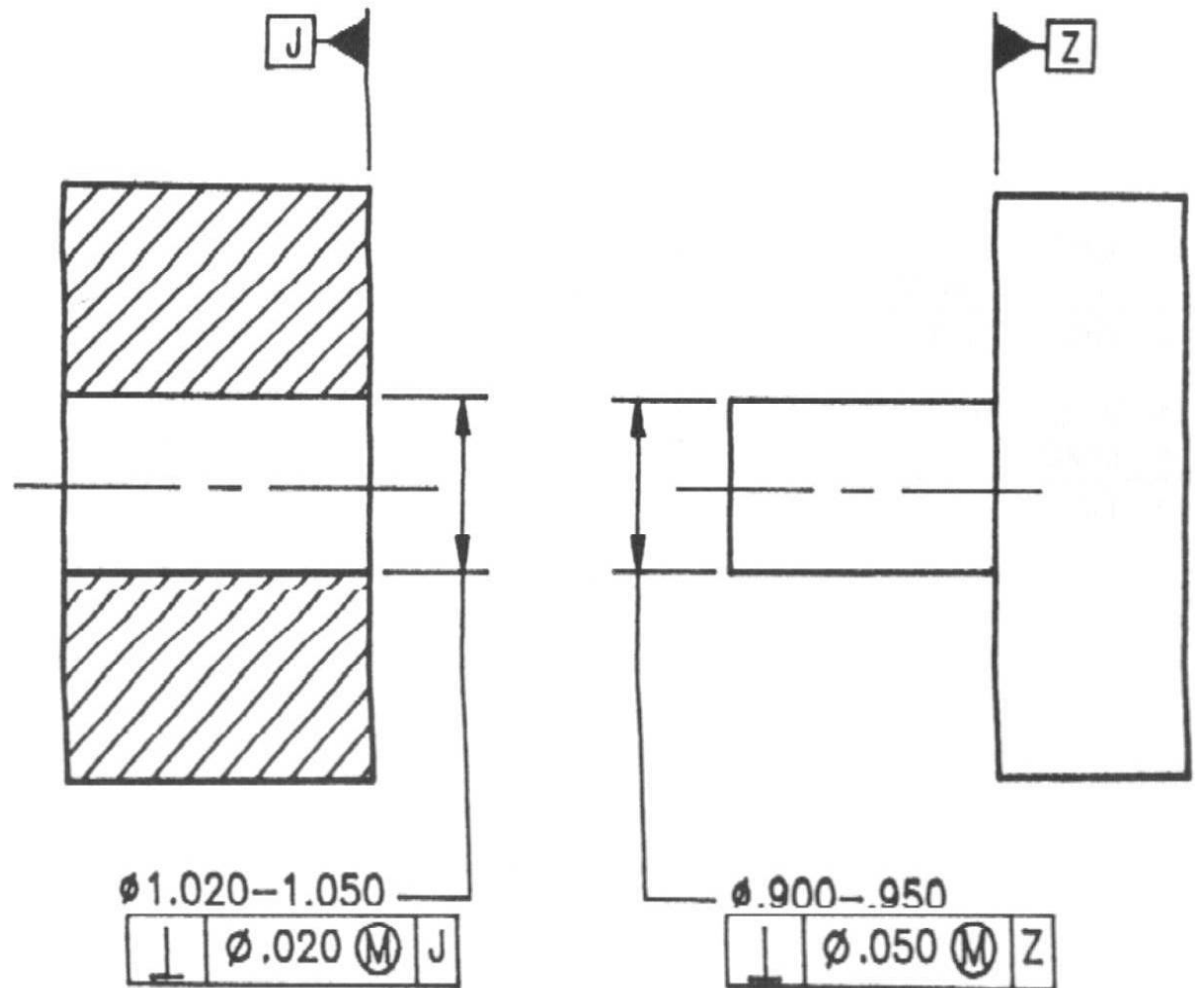


Fill in the rest of the shaft's feature control frame to assure:

- a) that it will mate with the hole.
- b) the most cost-effective design.

Mating Part Design



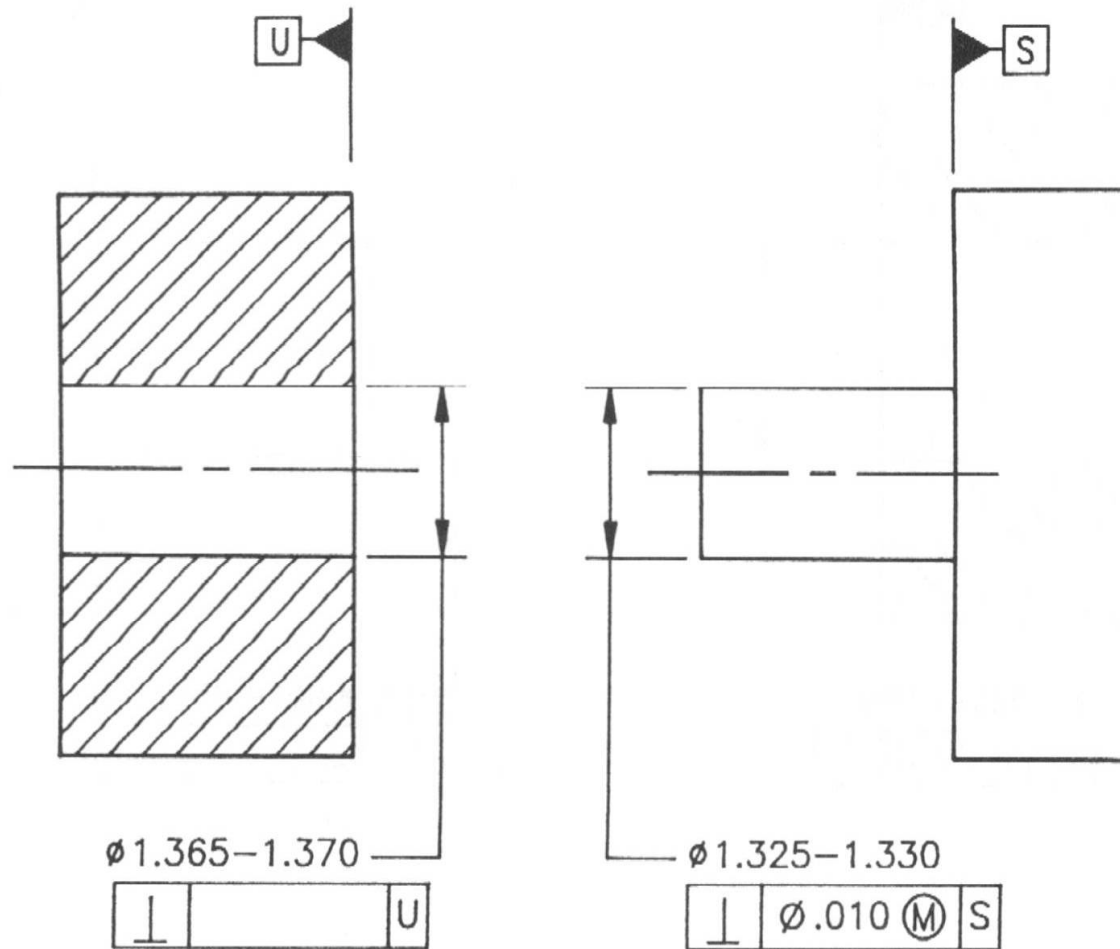


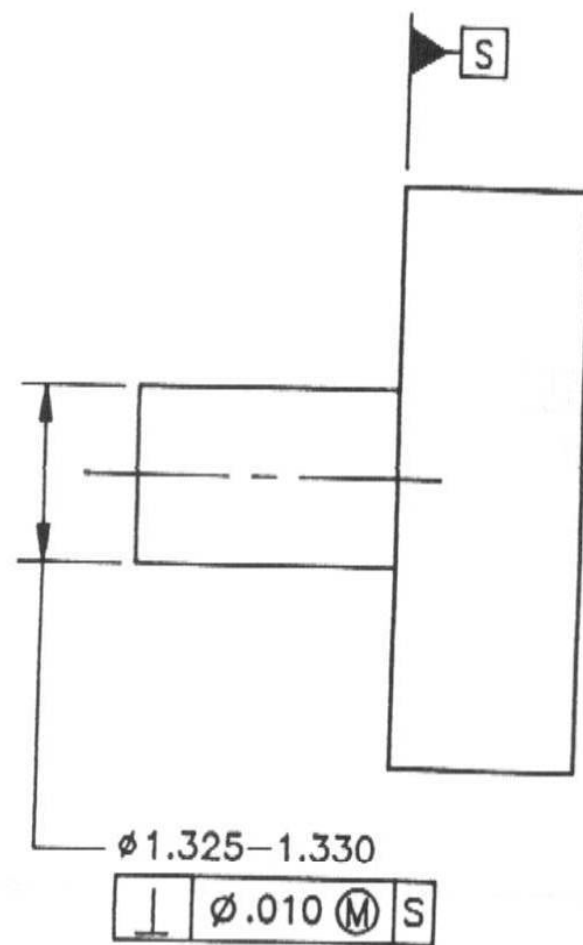
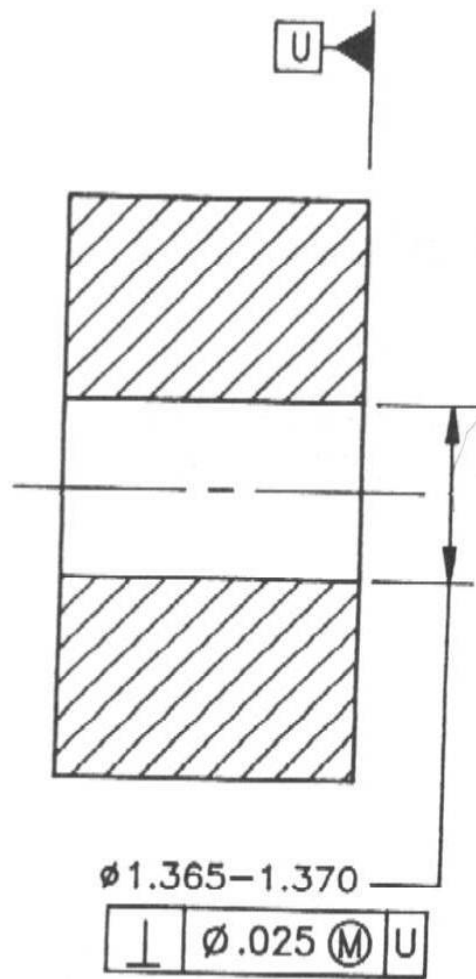
$\phi 1.020 = \text{MMC}$
 $- .020 = \text{Tol. at MMC}$
 $\frac{1.000}{1.000} = \text{Virt. Cond. hole}$

$\phi 1.000 = \text{Virt. Cond. hole}$
 $- .950 = \text{Shaft MMC}$
 $\frac{\phi .050}{\phi .050} = \text{Tol.}$

- Using the illustration below, fill in the rest of the hole's feature control frame to assure:
- that it will mate with the shaft.
 - the most cost-effective design.

Mating Part Design



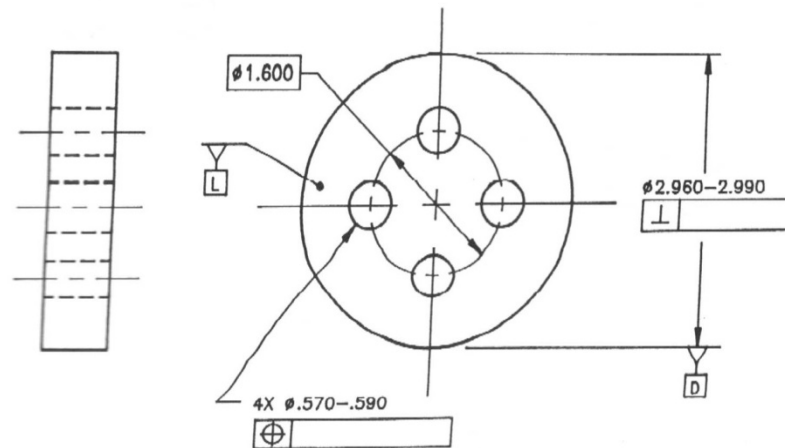
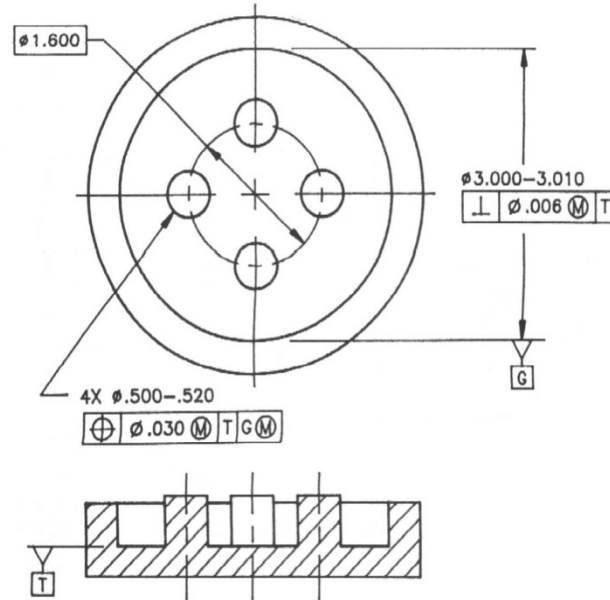


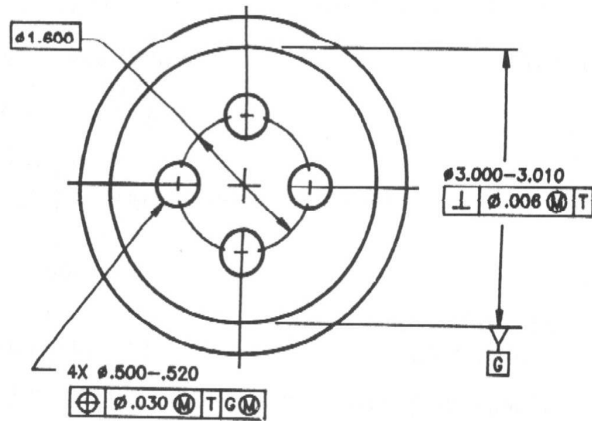
$$\begin{aligned}
 1.330 &= \text{MMC} \\
 + .010 &= \text{Tol. at MMC} \\
 \hline
 1.340 &= \text{Virt. Cond. Shaft}
 \end{aligned}$$

$$\begin{aligned}
 1.365 &= \text{Hole MMC} \\
 - 1.340 &= \text{Virt. Cond. Shaft} \\
 \hline
 \phi .025 &= \text{Tol.}
 \end{aligned}$$

- Using the illustration below, fill in the feature control frame so:
- the hockey puck (below the thick horizontal line) fits down inside of the cylindrical cavity (above the thick horizontal line).
 - the holes in the hockey puck fit over the pins in the cavity.
 - load is not born by the pins but rather by L and T.

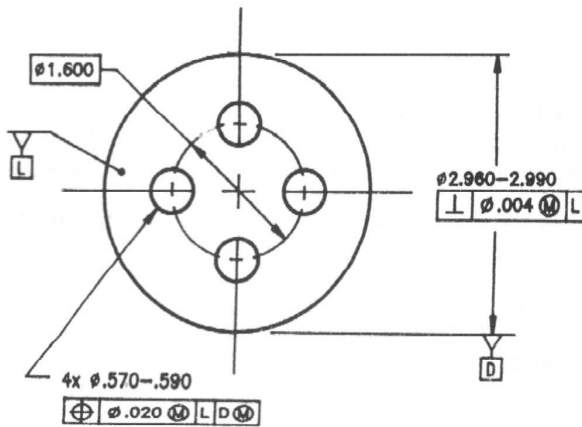
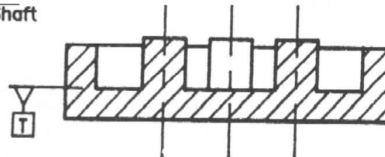
Mating Part Design





$\phi .520 = \text{MMC}$
 $+ .030 = \text{Tol. at MMC}$
 $.550 = \text{Virt. Cond. Shaft}$

$\phi 3.000 = \text{MMC}$
 $- .008 = \text{Tol. at MMC}$
 $\phi 2.994 = \text{Virt. Cond. Hole}$

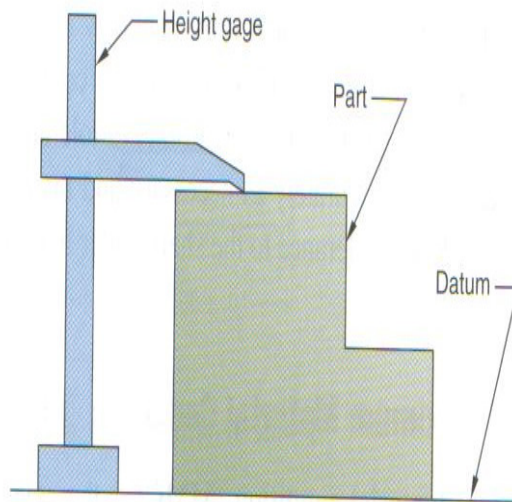


$\phi .570 = \text{MMC}$
 $-.550 = \text{Virt. Cond. Shaft}$
 $\phi .020 = \text{Tol.}$

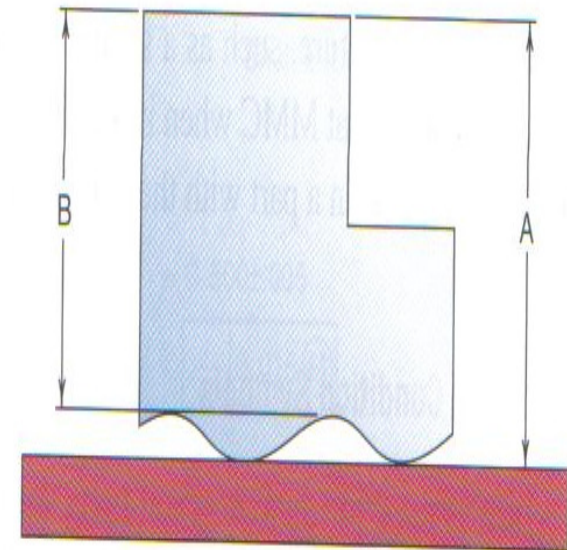
$\phi 2.994 = \text{Virt. Cond. Hole}$
 $- 2.990 = \text{MMC}$
 $\phi .004 = \text{Tol.}$

Datums and Datum Features

A **datum** is a starting place for a dimension. A datum may be a perfect plane, a center line, or a point. Datums are perfect, and they are not real. Examples are the center line of a shaft or the point at the center of a sphere. These are theoretical positions that either can be represented with inspection tools or can be derived. For example, a center line is represented by the center of an inspection pin or gage or by the center of an inspection spindle. A center line is derived by measuring to the edge of a gage pin and then adding half the diameter of the pin to locate the center of the gage pin from an edge or another feature. For a hole, the measurement is *not* to the edge of the feature hole but to the largest-gage pin that will fit into the hole.

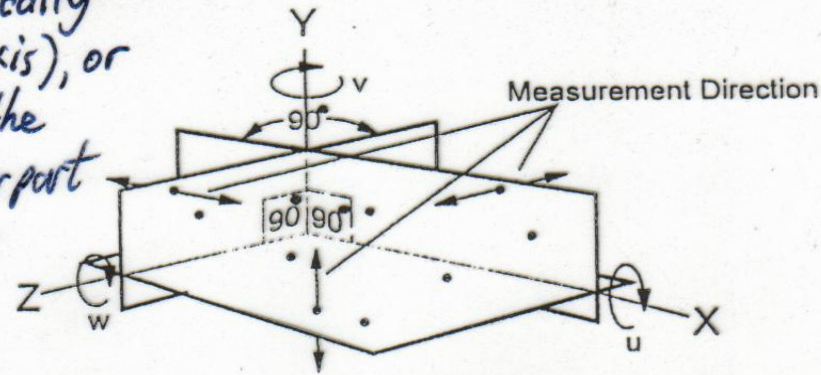


3/16/20 The bottom surface of the part is the datum feature, surface plate is the datum.

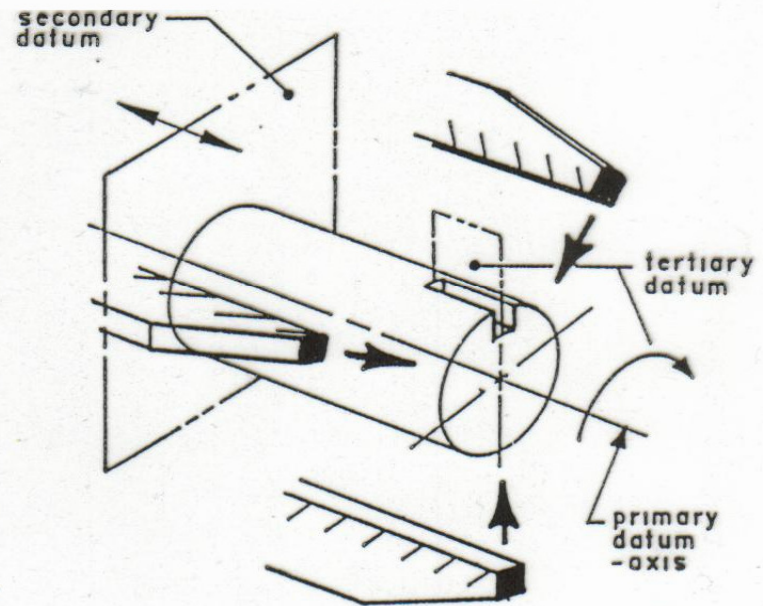
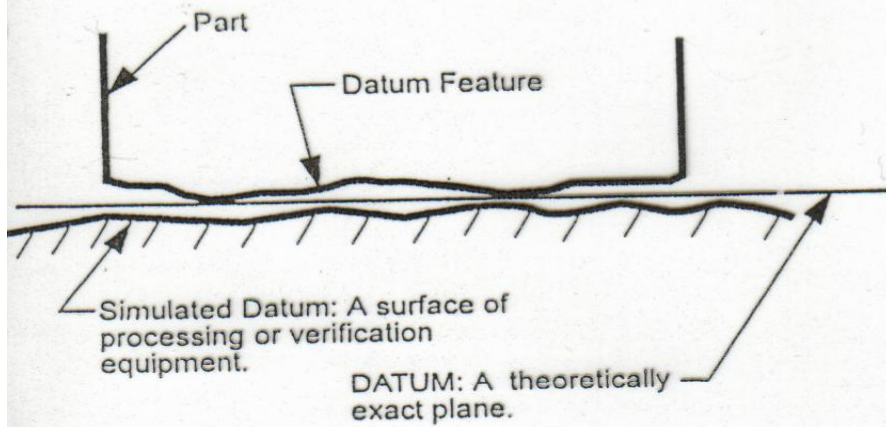


Dr. Murat Sönmez

Datum is a theoretically exact point, line (axis), or plane derived from the true geometric counterpart of a specified datum feature.



Datum Reference Framework. Three Mutually Perpendicular Planes.



Datum

Theoretically perfect points, lines, or planes

Simulated Datum (Datum Simulators)

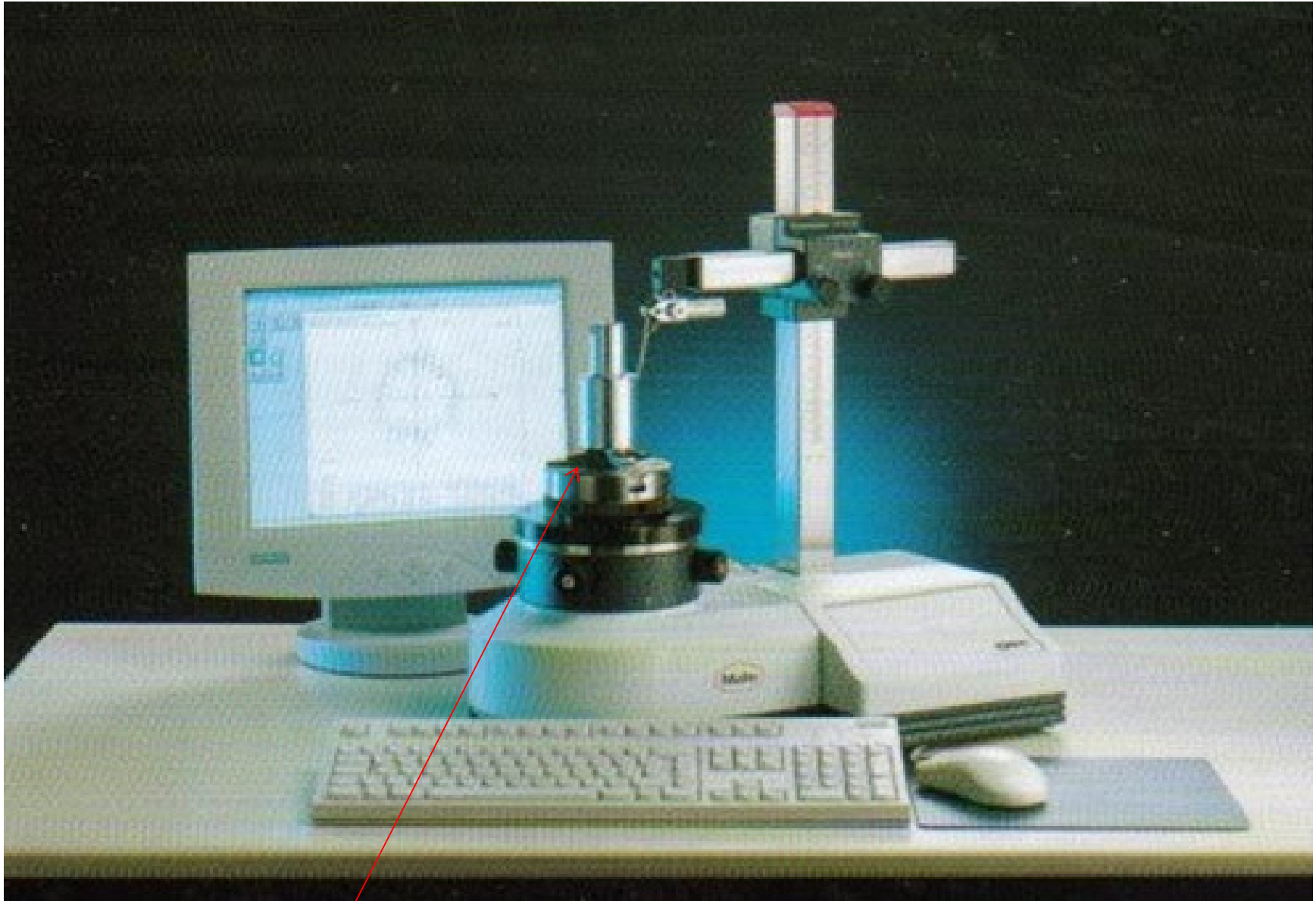
Surfaces and axes of processing or inspection equipment

Datum Feature

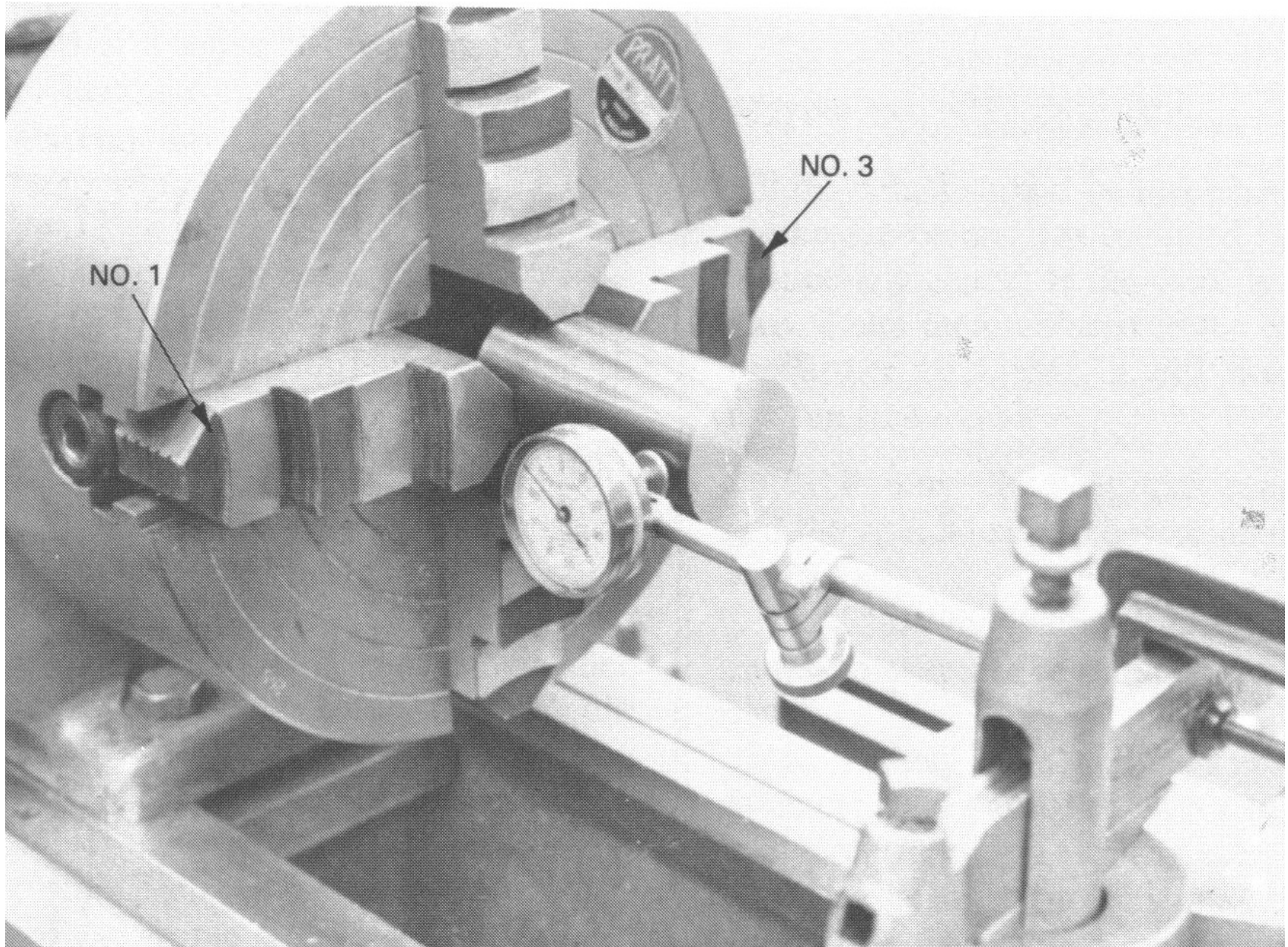
Actual part feature surfaces

Temporary Datum

Introduced for processing or inspection purposes (may be removed)

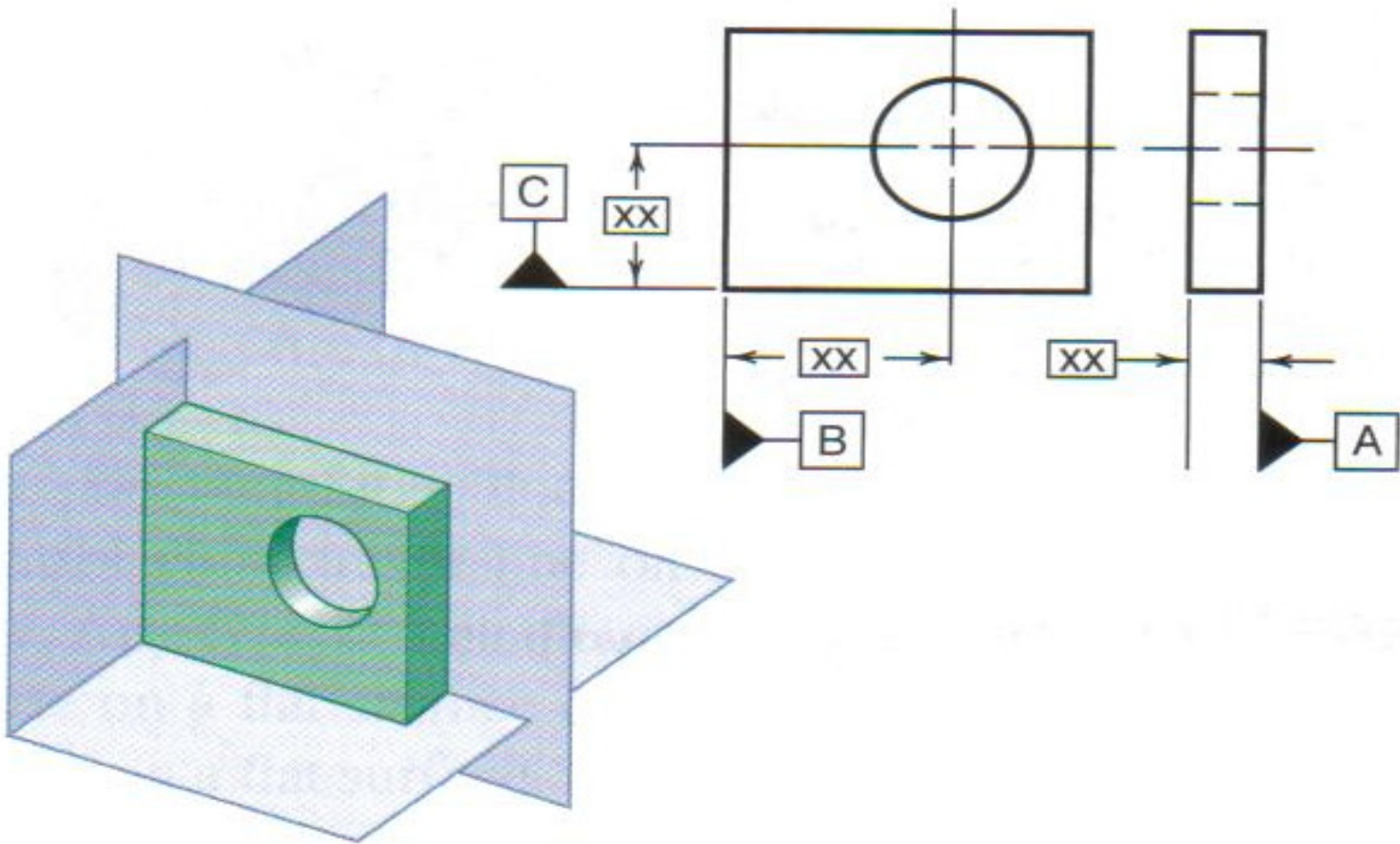


Datum simulator (jaws of the chuck)

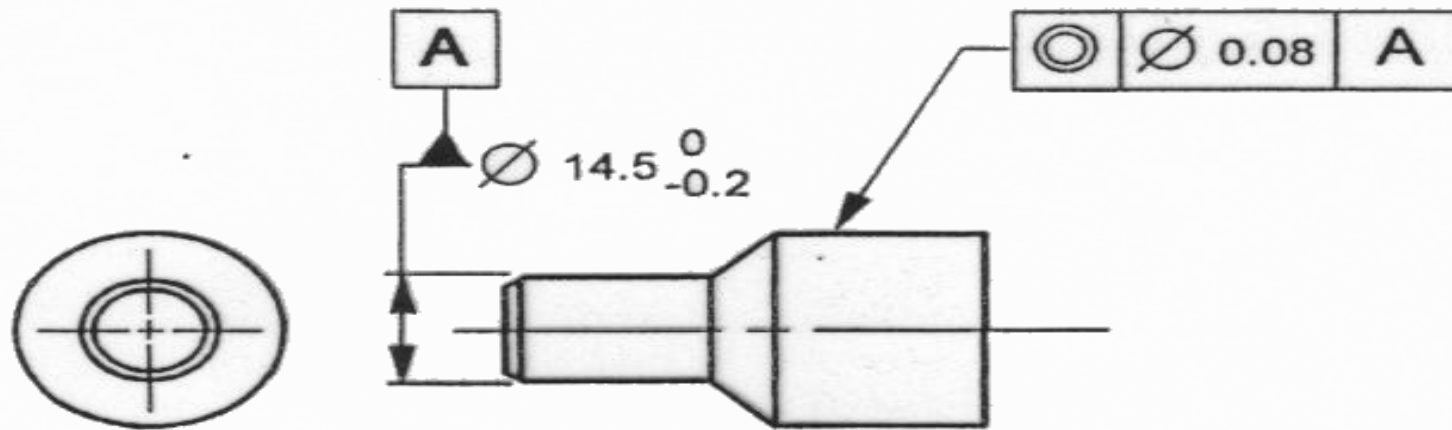


Datum Selection

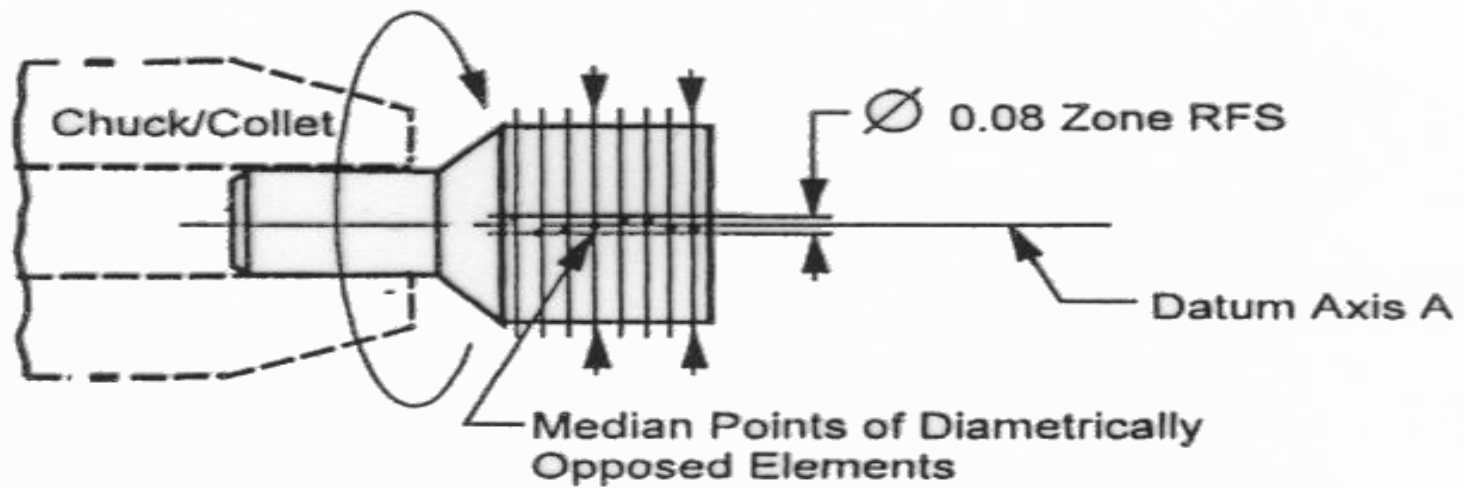
- * **Function and functional relationships:** This is the most critical issue, impacting not only the design but the manufacturing and quality plans as well.
- * **Reality:** Datums should be real, identifiable, and verifiable. Imaginary features, points in space, or features that are impossible (or at least difficult) to locate are acceptable in a lab or mathematical environment, but are difficult for the manufacturing world to deal with. Equally difficult are datum features that are inaccessible or hidden within the product.
- * **Accuracy:** Datums should be accurate and should offer the best repeatability, because datum error can impact assessment and verification of other features. If a datum feature is within its specification control (flatness for example), it becomes theoretically perfect (or zero) for measurement of other features.



Three-plane datum reference plane

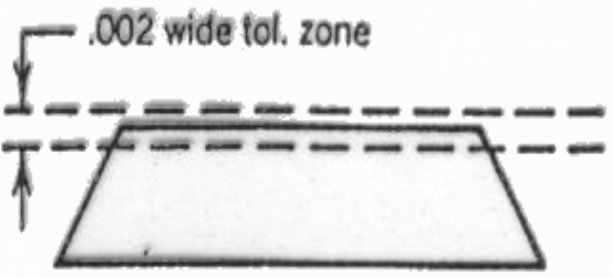
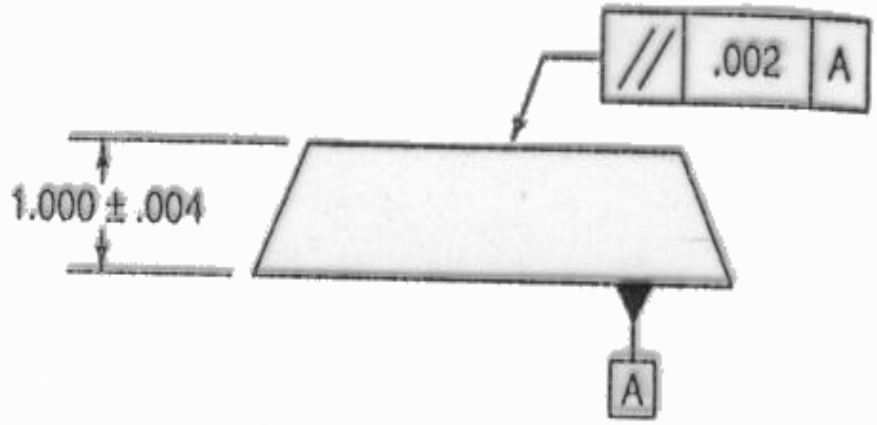


Meaning

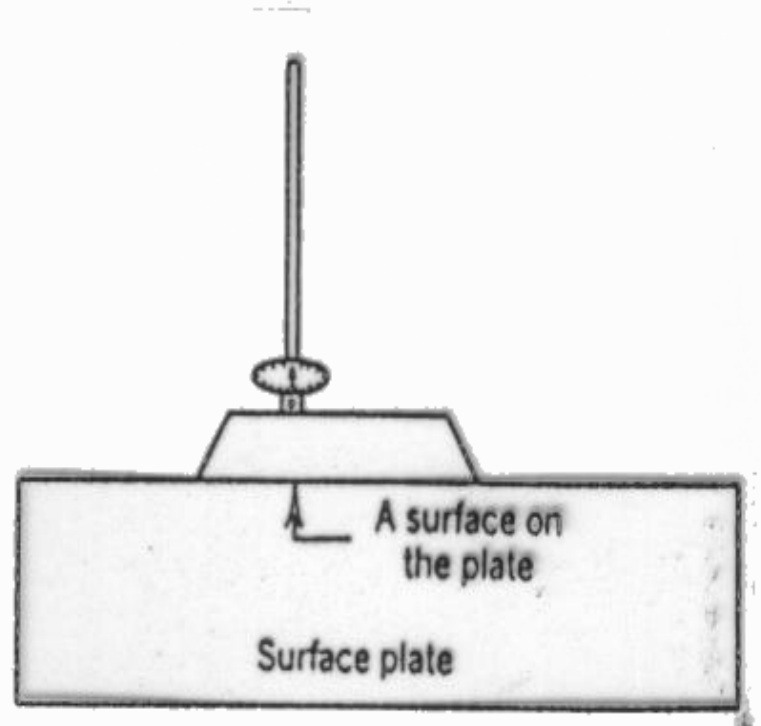


Concentricity.

Parallelism callout.

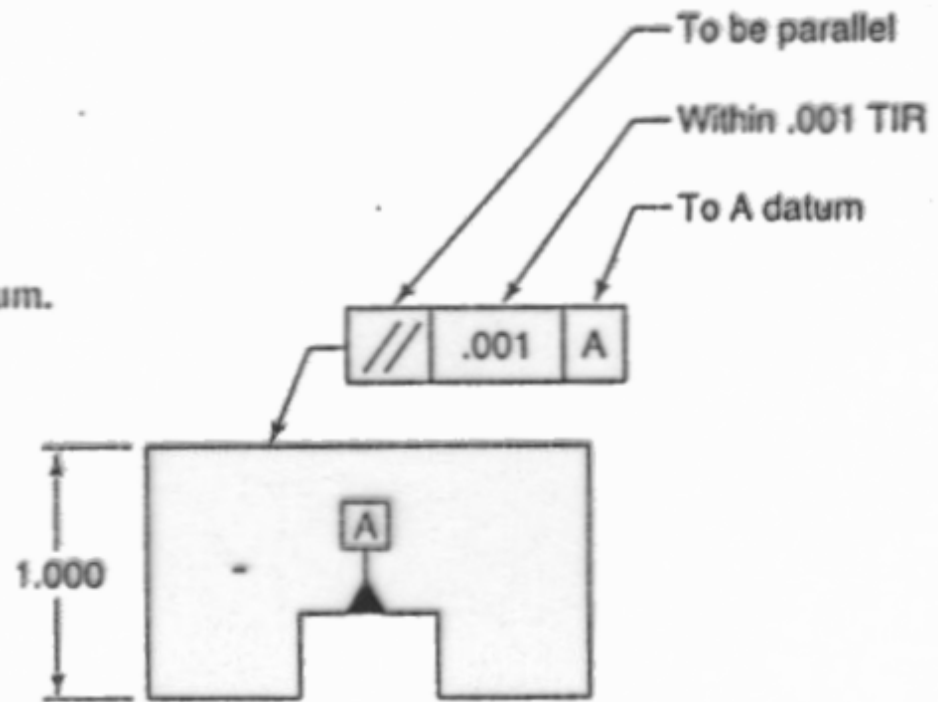


Parallelism tolerance zone.

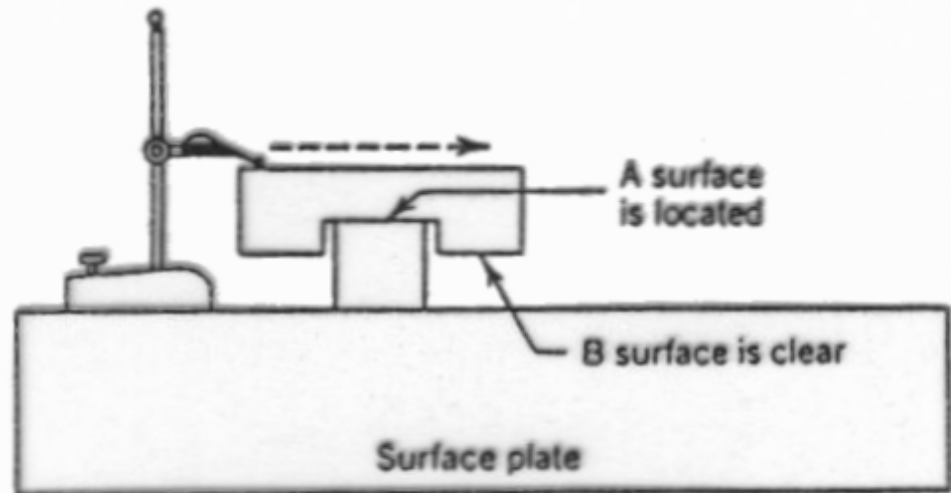


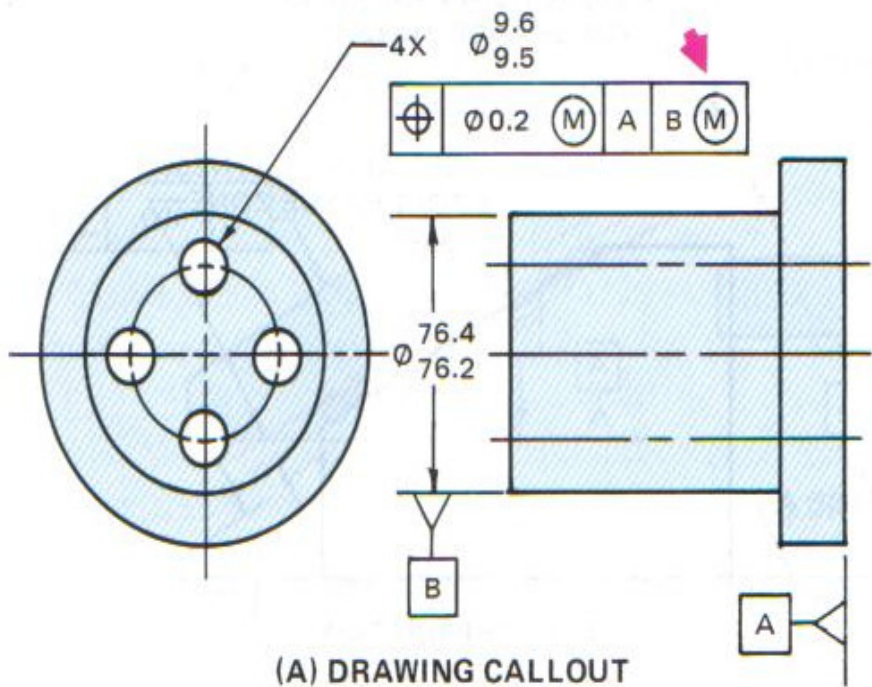
Datum is located.

Parallelism to a hidden datum.



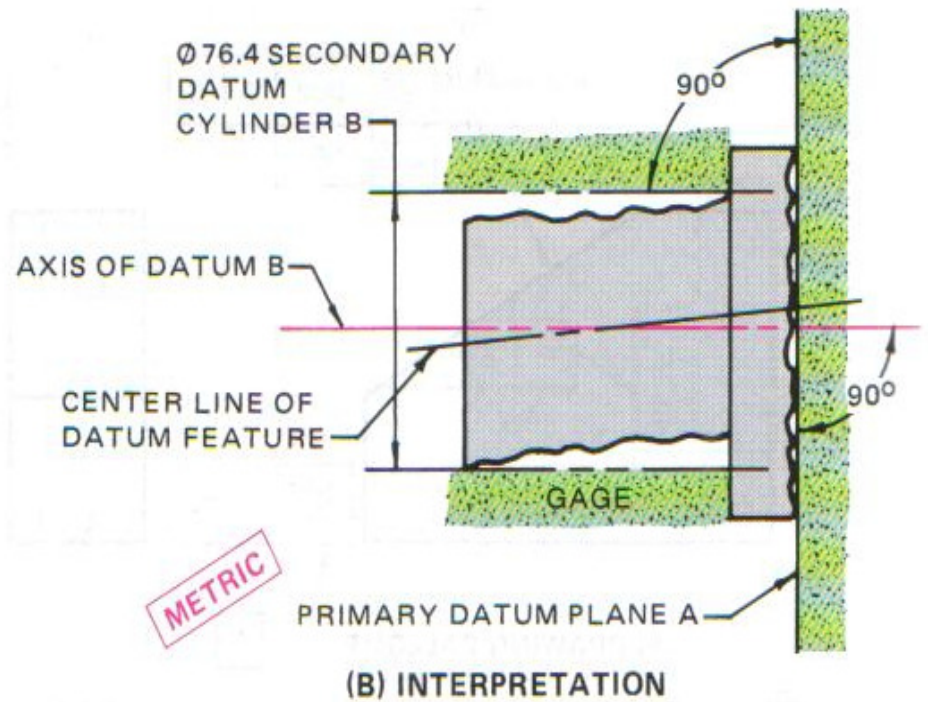
Fixed parallel locates the hidden datum.

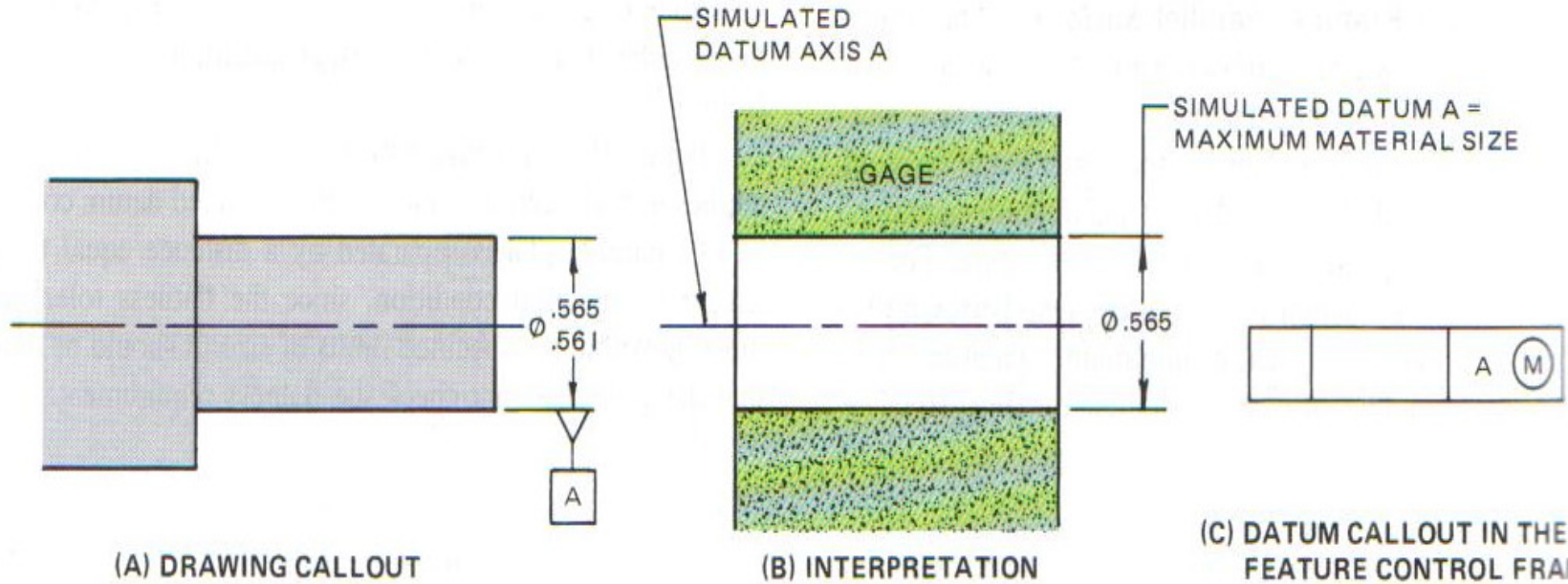




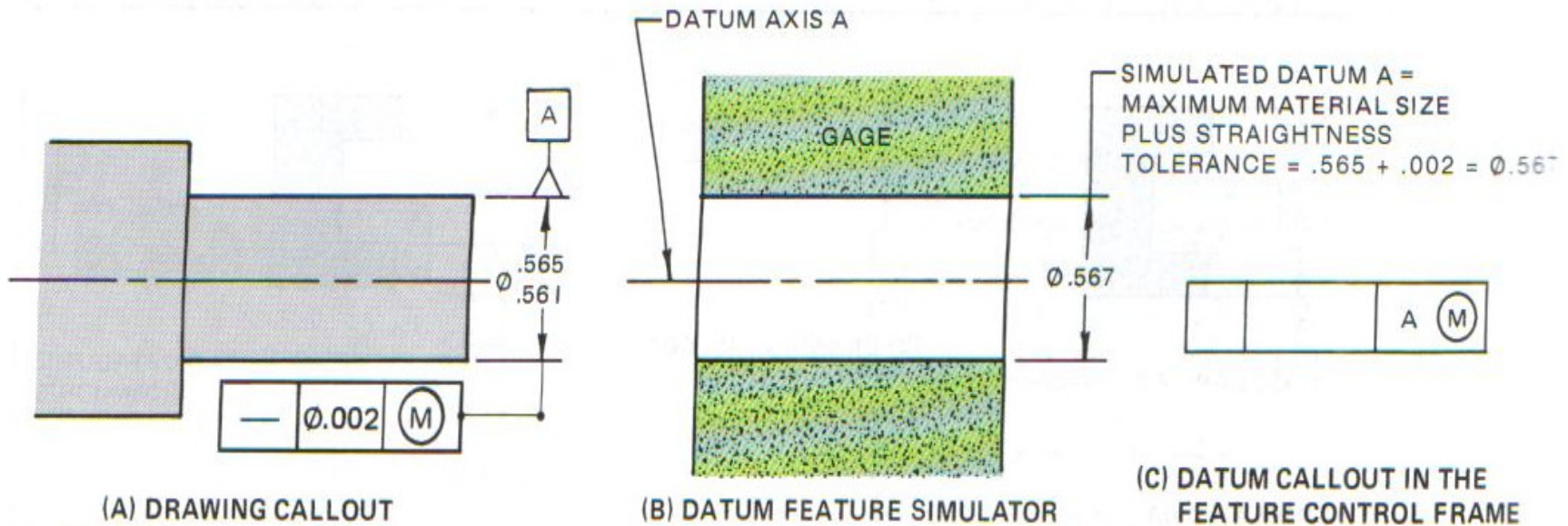
(A) DRAWING CALLOUT

Cylindrical feature as secondary datum.

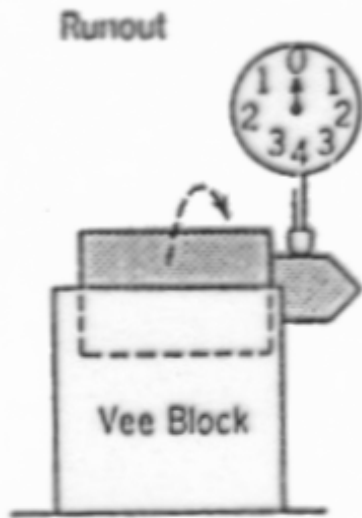




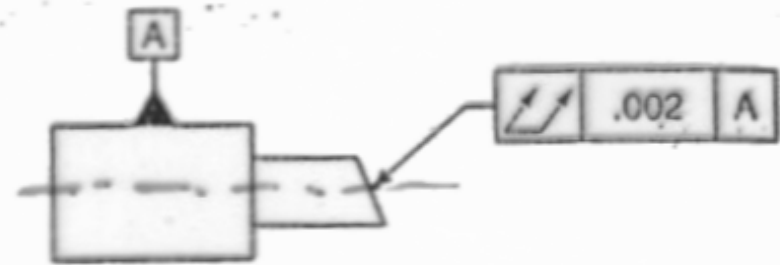
External primary datum without form tolerances—MMC.



External primary datum with straightness tolerance—MMC.



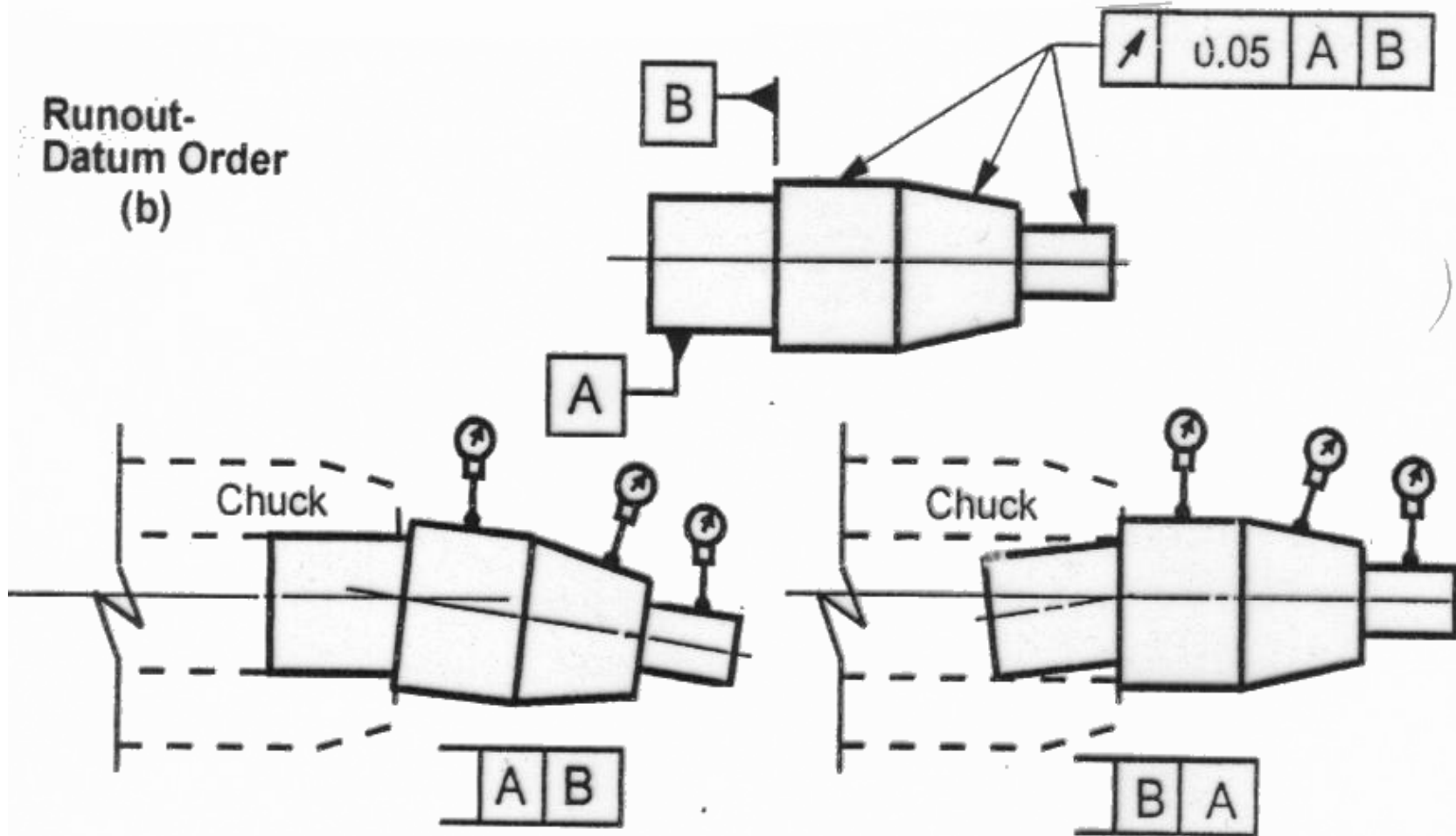
Measuring circular runout.



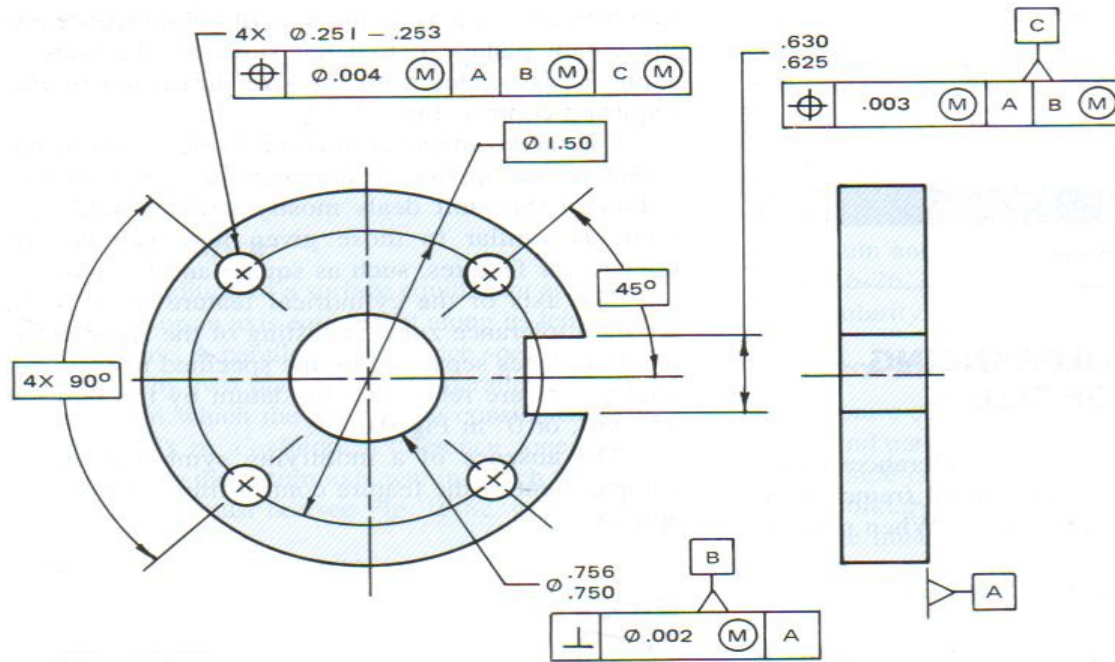
End surface total runout.

Steps for Total Runout Measurement

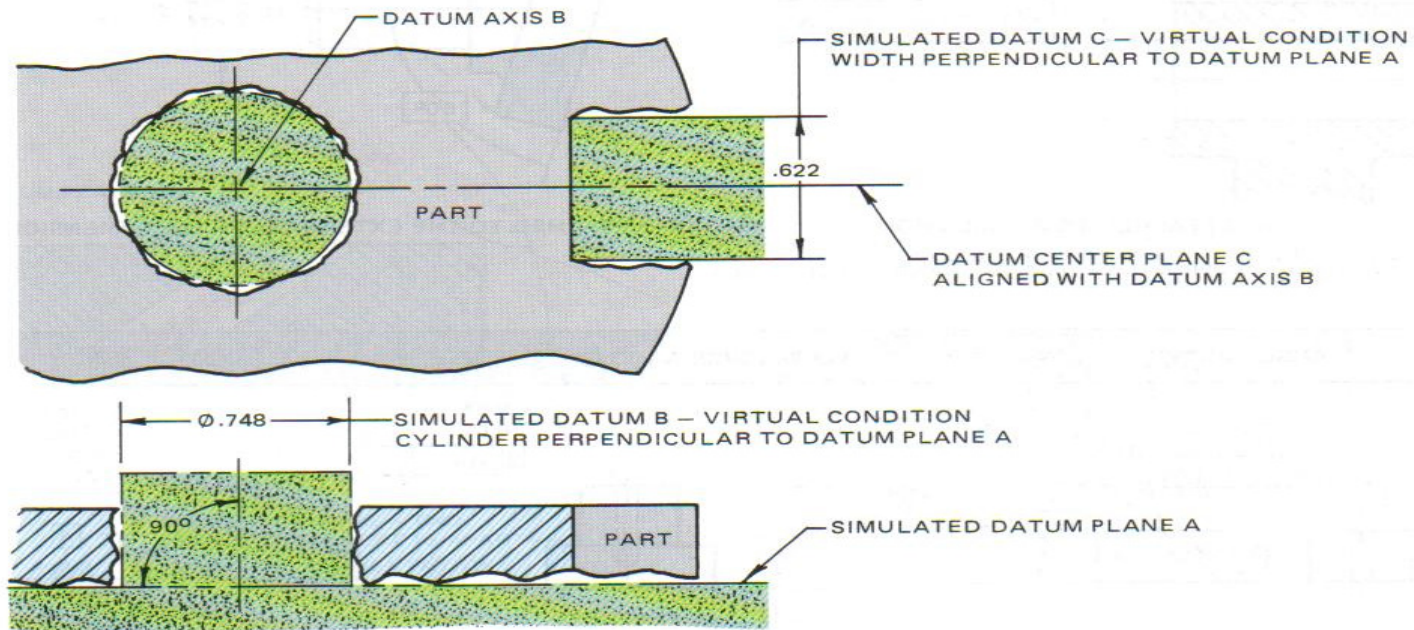
Runout-
Datum Order
(b)



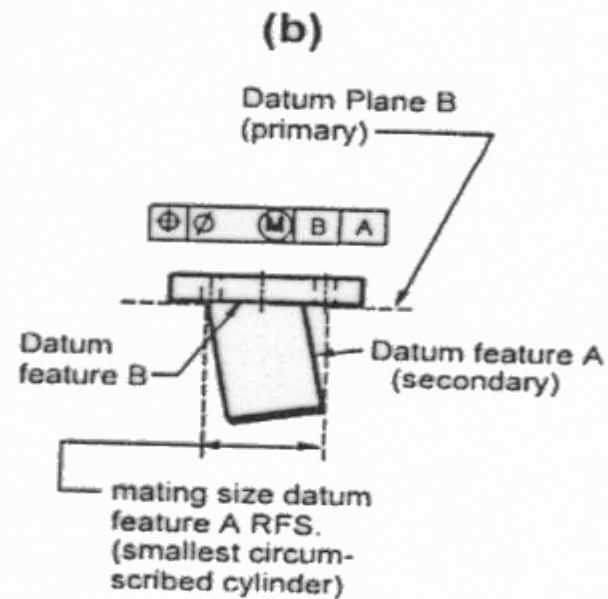
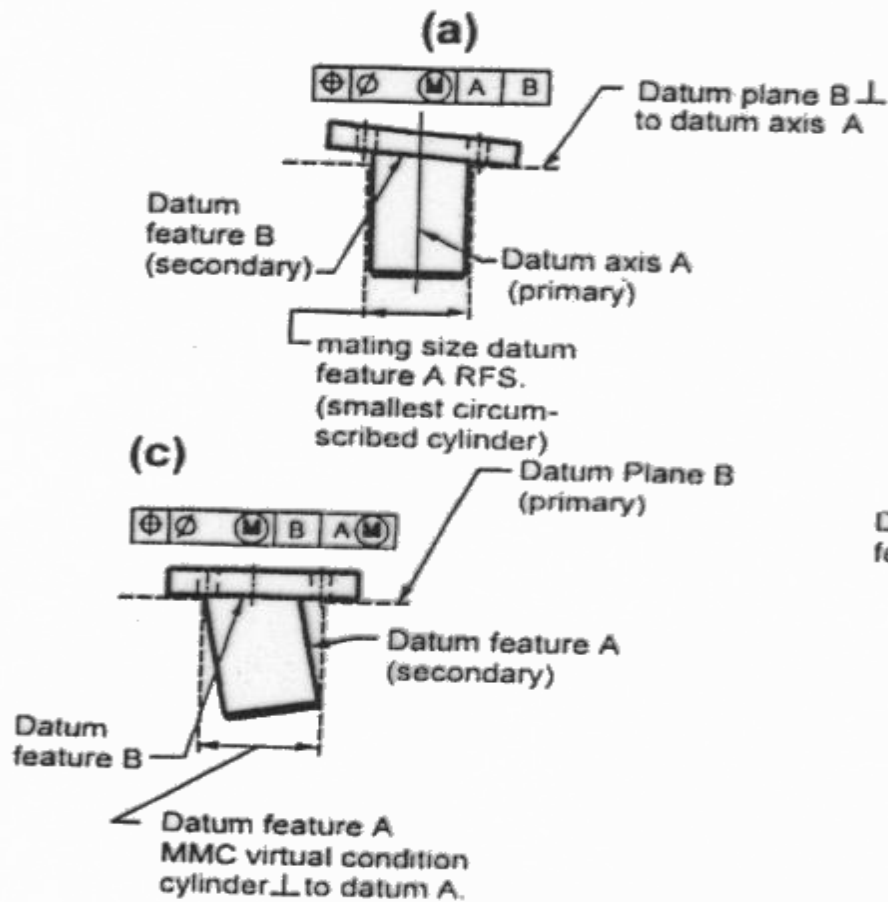
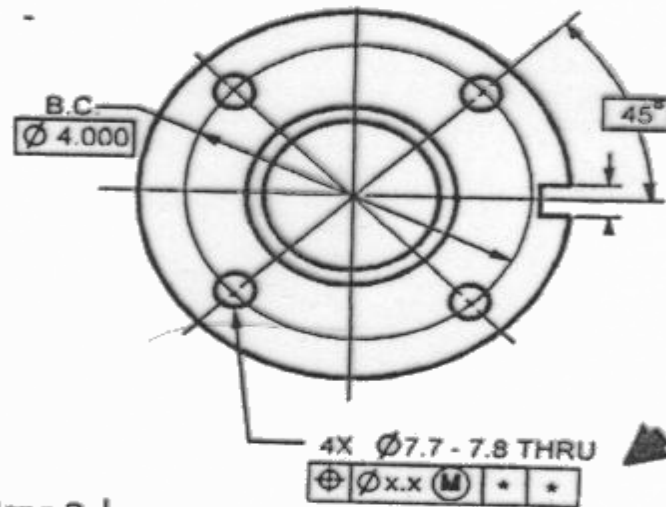
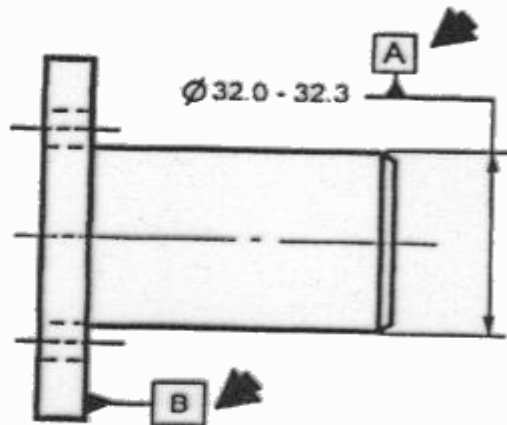
Circular runout and
datum order.



(A) DRAWING CALLOUT

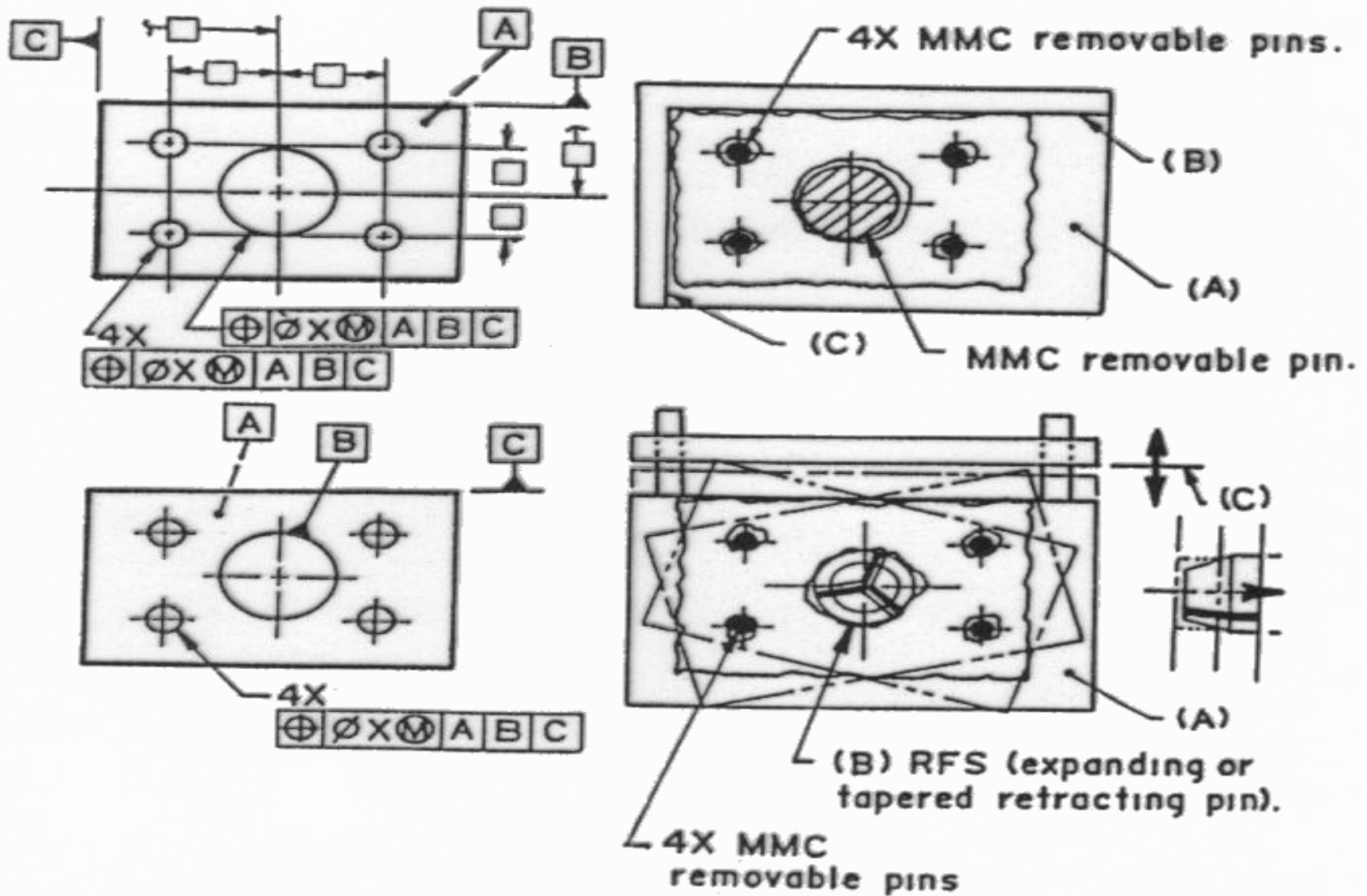


(B) DATUM FEATURE SIMULATORS

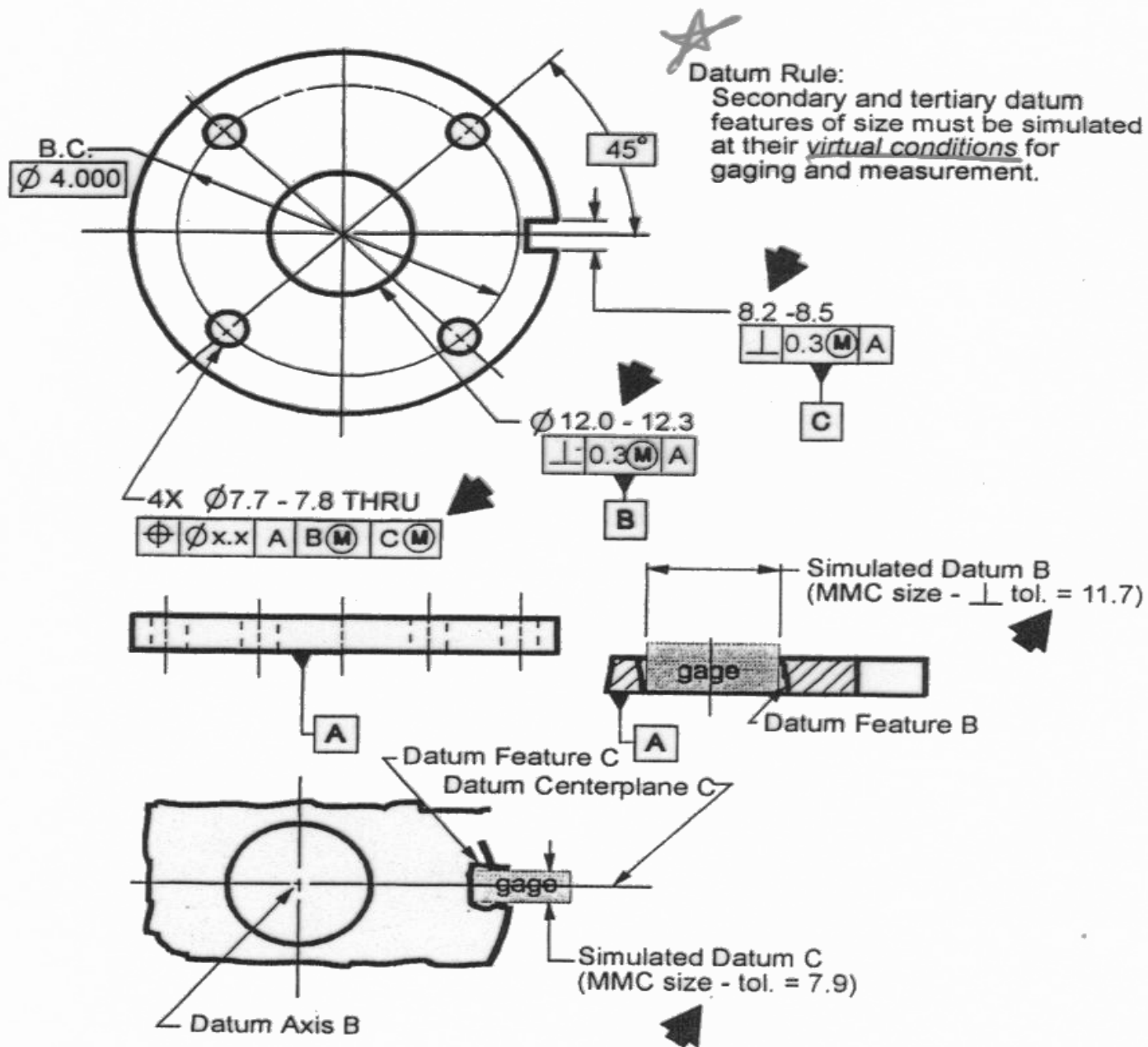


Datum order (precedence).

When the secondary datum is an axis, the tertiary datum serves to orient the part (stop rotation).

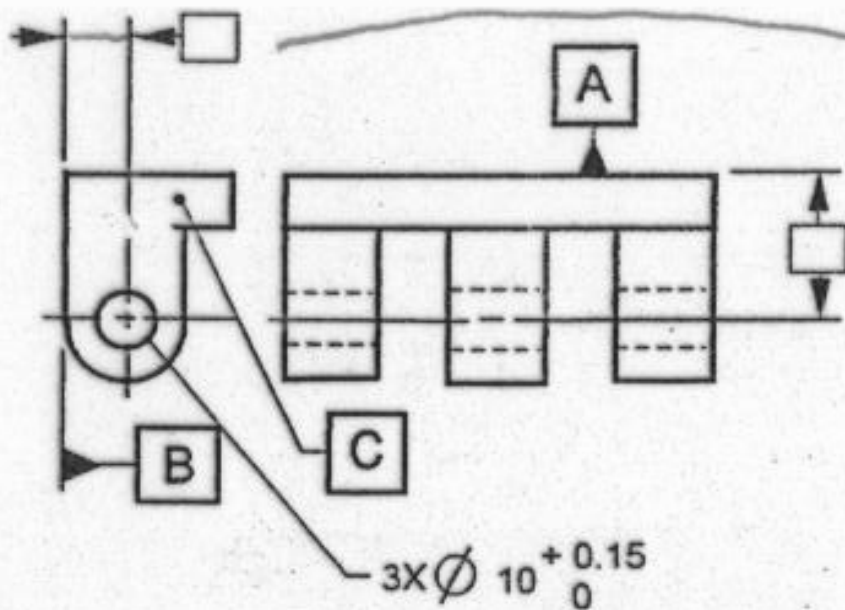


Secondary and tertiary datum features.



(a)

(a) Secondary/tertiary datum rule;
(b) datums MMC and bonus tolerance.



The basic dimensions that control the pattern of features to datum framework apply to the upper control only!

- (a)

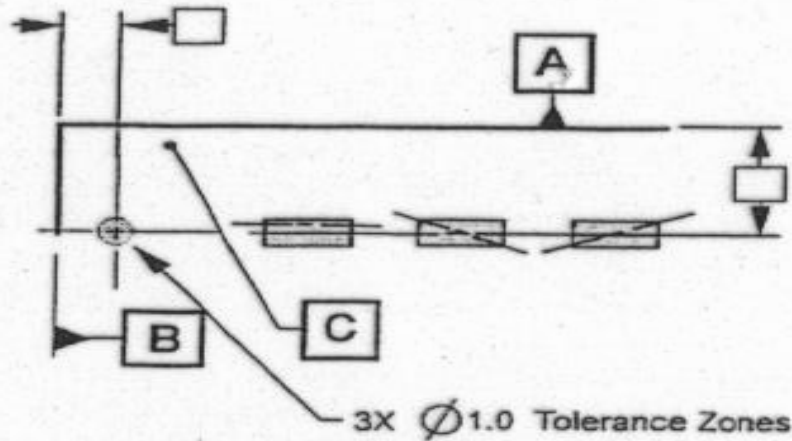
\varnothing	$\varnothing 1.0$ (M) A B C
	$\varnothing 0.5$ (M)
- (b)

\varnothing	$\varnothing 1.0$ (M) A B C
	$\varnothing 0.5$ (M) A
- (c)

\varnothing	$\varnothing 1.0$ (M) A B C
	$\varnothing 0.5$ (M) A B

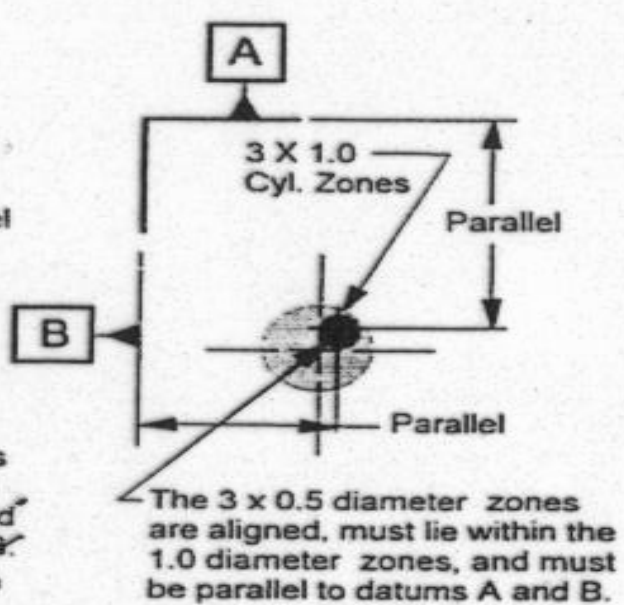
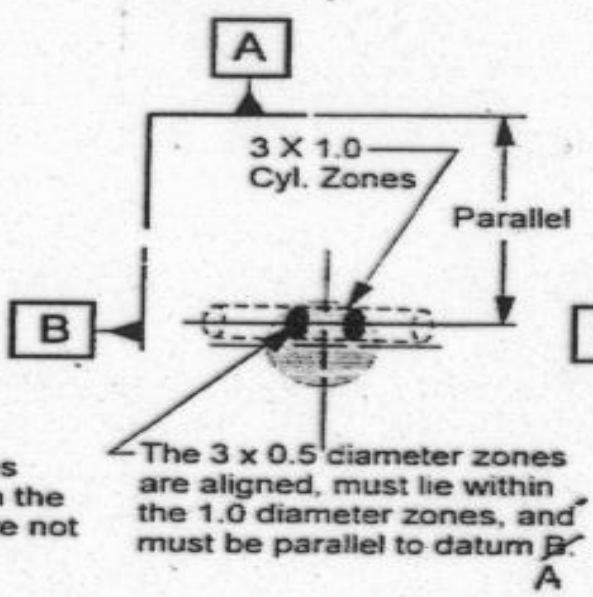
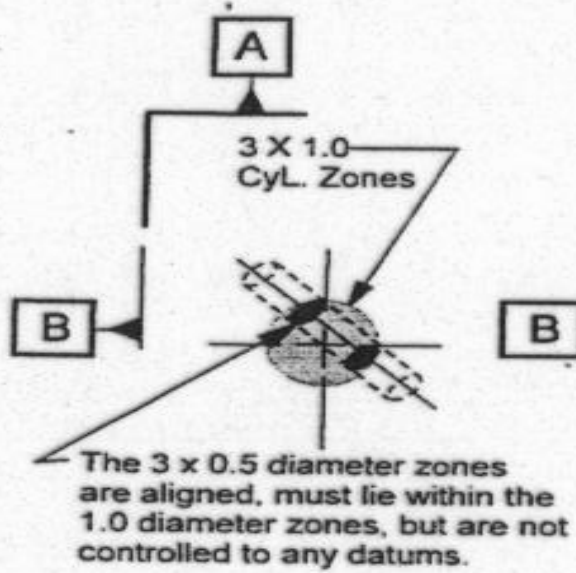
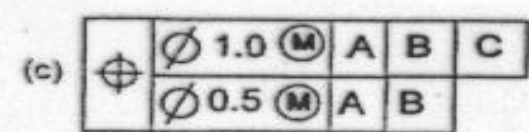
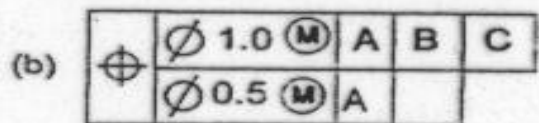
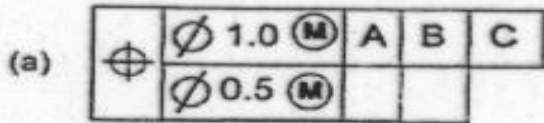
← upper control

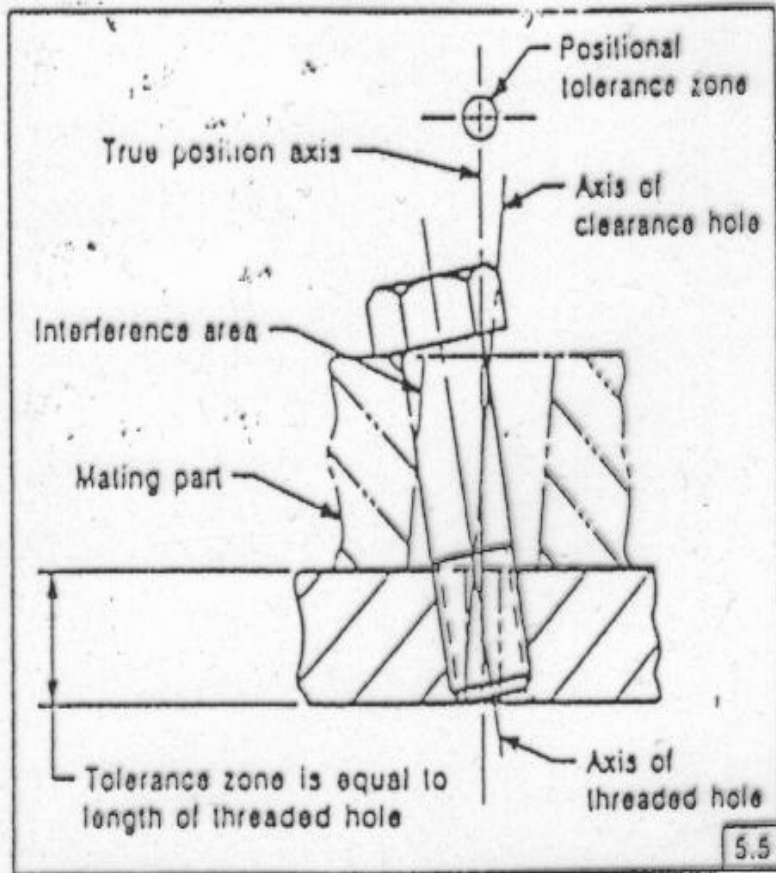
Composite position controls: aligned holes.



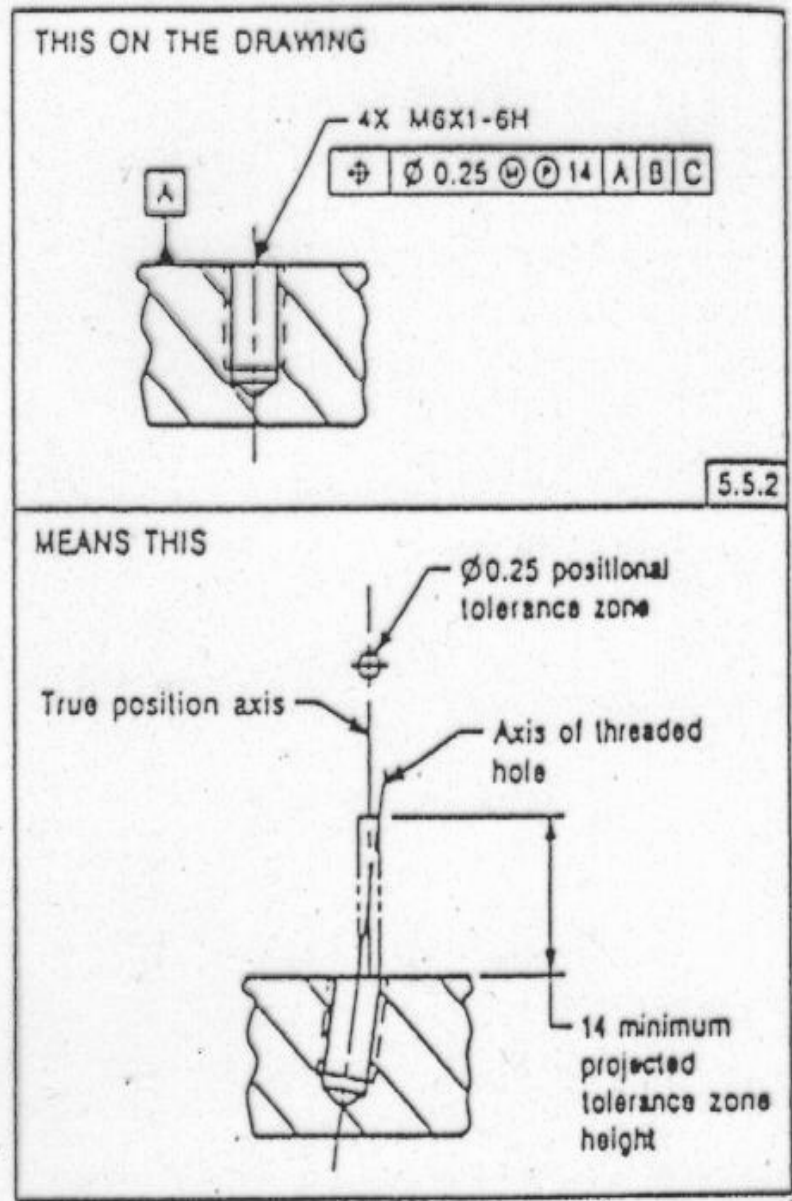
For the Upper Control Callout
 The 1.0 diameter tolerance zones must be aligned and basically located from the datum framework A, B, C.

For the Lower Control Callouts

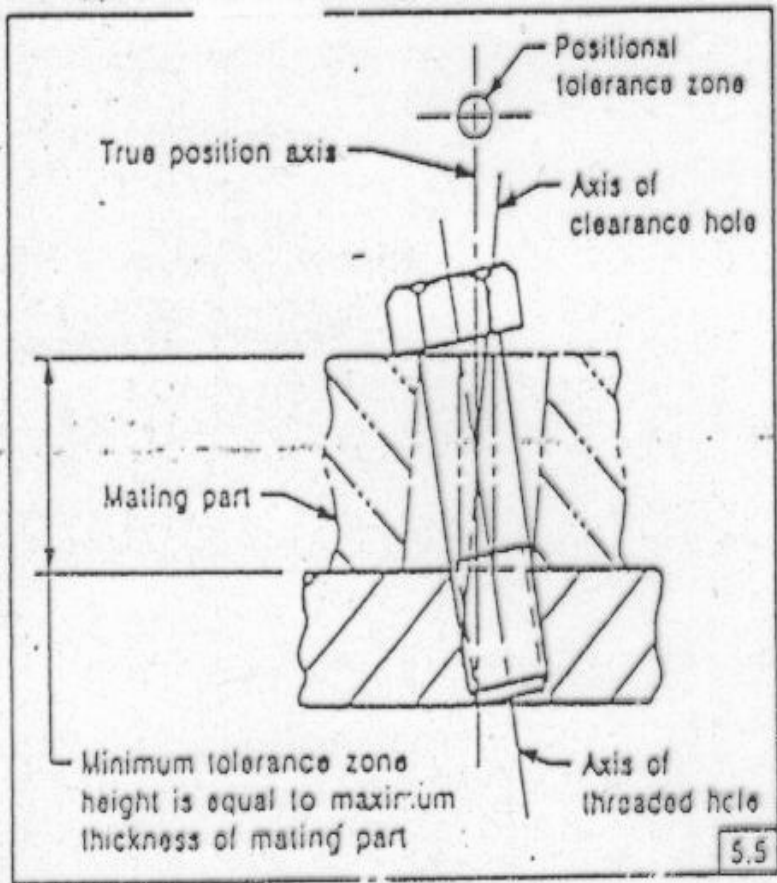




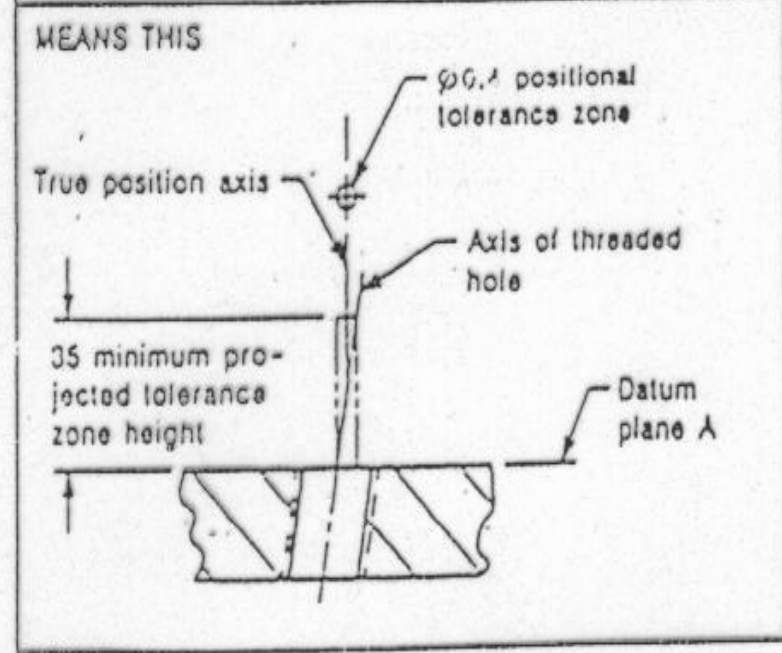
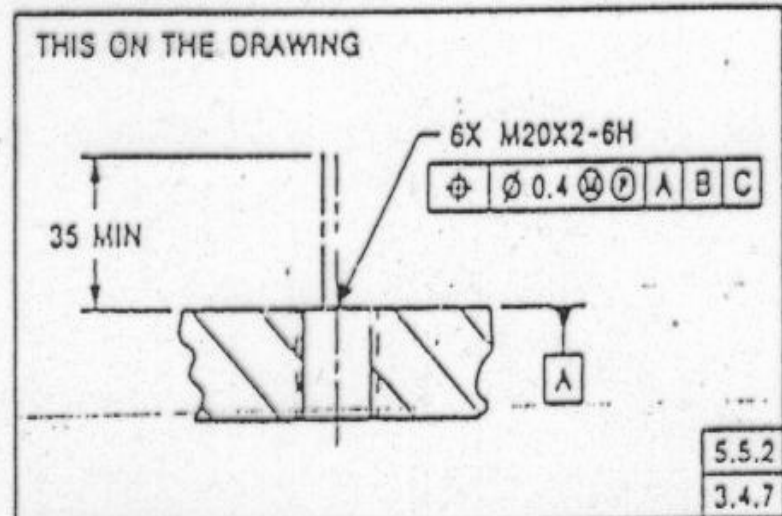
INTERFERENCE DIAGRAM, FASTENER AND HOLE



PROJECTED TOLERANCE ZONE SPECIFIED



BASIS FOR PROJECTED TOLERANCE ZONE



PROJECTED TOLERANCE ZONE INDICATED WITH CHAIN LINE

General tolerances — *(Geometrical)*

Part 2:

Geometrical tolerances for features without individual tolerance indications

5.1.1 Straightness and flatness

The general tolerances on straightness and flatness are given in table 1. When a tolerance is selected from table 1, it shall be based, in the case of straightness, on the length of the corresponding line and, in the case of flatness, on the longer lateral length of the surface, or the diameter of the circular surface.

Table 1 — General tolerances on straightness and flatness

Values in millimetres

Tolerance class	Straightness and flatness tolerances for ranges of nominal lengths					
	up to 10	over 10 up to 30	over 30 up to 100	over 100 up to 300	over 300 up to 1 000	over 1 000 up to 3 000
H	0,02	0,05	0,1	0,2	0,3	0,4
K	0,05	0,1	0,2	0,4	0,6	0,8
L	0,1	0,2	0,4	0,8	1,2	1,6

5.1.2 Circularity

The general tolerance on circularity is equal to the numerical value of the diameter tolerance, but in no case shall it be greater than the respective tolerance value for circular radial run-out given in table 4 (see examples in clause B.2).

5.1.3 Cylindricity

General tolerances on cylindricity are not specified.

5.2.3 Perpendicularity

The general tolerances on perpendicularity are given in table 2. The longer of the two sides forming the right angle shall be taken as the datum; if the sides are of equal nominal length, either may be taken as the datum.

Table 2 — General tolerances on perpendicularity

Values in millimetres

Tolerance class	Perpendicularity tolerances for ranges of nominal lengths of the shorter side			
	up to 100	over 100 up to 300	over 300 up to 1 000	over 1 000 up to 3 000
H	0,2	0,3	0,4	0,5
K	0,4	0,6	0,8	1
L	0,6	1	1,5	2

5.2.4 Symmetry

The general tolerances on symmetry are given in table 3. The longer of the two features shall be taken as the datum; if the features are of equal nominal length, either may be taken as the datum.

NOTE — The general tolerances on symmetry apply where

- at least one of the two features has a median plane, or
- the axes of the two features are perpendicular to each other.

See examples in clause B.5.

Table 3 — General tolerances on symmetry

Values in millimetres

Tolerance class	Symmetry tolerances for ranges of nominal lengths			
	up to 100	over 100 up to 300	over 300 up to 1 000	over 1 000 up to 3 000
H	0,5			
K	0,6		0,8	1
L	0,6	1	1,5	2

5.2.5 Coaxiality

General tolerances on coaxiality are not specified.

NOTE — The deviation in coaxiality may, in an extreme case, be as great as the tolerance value for circular radial run-out given in table 4, since the deviation in radial run-out comprises the deviation in coaxiality and the deviation in circularity.

5.2.6 Circular run-out

The general tolerances on circular run-out (radial, axial and any surface of revolution) are given in table 4.

For general tolerances on circular run-out, the bearing surfaces shall be taken as the datum if they are designated as such. Otherwise, for circular radial run-out, the longer of the two features shall be taken as the datum; if the features are of equal nominal length, either may be taken as the datum.

Table 4 — General tolerances on circular run-out

Values in millimetres

Tolerance class	Circular run-out tolerances
H	0,1
K	0,2
L	0,5

6 Indications on drawings

6.1 If general tolerances in accordance with this part of ISO 2768 shall apply in conjunction with the general tolerances in accordance with ISO 2768-1, the following information shall be indicated in or near the title block:

- a) "ISO 2768";
- b) the tolerance class in accordance with ISO 2768-1;
- c) the tolerance class in accordance with this part of ISO 2768.

EXAMPLE

ISO 2768-m K