CVE 372 HYDROMECHANICS PIPE FLOW

FORMULA SHEET

PIPE FLOW

Reynolds Number: $Re = \frac{\rho V D}{\mu} = \frac{V D}{v}$ Continuity Equation: $Q = V_1 A_1 = V_2 A_2 = VA = constant$

Energy Equation: $z_1 + \frac{p_1}{\gamma} + \alpha_1 \frac{V_1^2}{2g} = z_2 + \frac{p_2}{\gamma} + \alpha_2 \frac{V_2^2}{2g} - H_P + H_T + \sum h_f + \sum h_m$ Pump Head: $H_P = \frac{\eta P_P}{\gamma Q}$ 1 watt = 1 N m/s 1 hp = 745.7 watt Turbine Head: $H_T = \frac{P_T}{\eta \gamma Q}$ Pump Power: $P_p = \frac{\gamma Q H_p}{\eta_p}$ Parallel Pumps: $\eta_p = \frac{\gamma H_p \sum Q}{\sum P_p}$ Pumps in Series: $\eta_p = \frac{\gamma Q \sum H_p}{\sum P_p}$

Momentum Equation: $Fp_1 - Fp_2 + W \sin \theta - F_f = \rho Q (\beta_2 V_2 - \beta_1 V_1)$ Total Head Loss: $h_L = h_f + h_m$ Head Loss (Darcy-Weisbach Equation): $h_f = f \frac{L}{D} \frac{V^2}{2g} = \frac{8f L Q^2}{g \pi^2 D^5} = \frac{4\tau_w L}{\gamma D}$

Head Loss (Hazen – Williams Equation): $h_{\rm f} = \frac{6.8}{C^{1.85}} \frac{L}{D^{1.165}} V^{1.85} = \frac{10.6}{C^{1.85}} \frac{L}{D^{4.87}} Q^{1.85}$ Head Loss (local/minor): $h_{\rm m} = K_m \frac{V^2}{2g} = K_m \frac{8Q^2}{g\pi^2 D^4}$ Pressure Change (horizontal pipe): $\Delta p = \frac{2\pi L}{r} = \frac{4L\tau_w}{D} = \gamma h_L$ Pressure Change (sloped pipe): $\frac{\Delta p - \gamma L \sin \theta}{L} = \frac{2\tau}{r}$ Velocity: $V = \frac{(\Delta p - \gamma L \sin \theta)D^2}{32\mu L}$ Non-circular Pipes: $R_h = \frac{A}{P}$ $D_h = 4R_h$ $h_{\rm f} = f \frac{L}{D_h} \frac{V^2}{2g}$ $\text{Re} = \frac{\rho V D_h}{\mu} = \frac{V D_h}{V}$ Networks: $\Delta Q = -\frac{\Sigma K |Q_a| Q_a}{\Sigma 2 K |Q_a|}$ (Hardy-Cross Method) where $K = \frac{8 f L}{g \pi^2 D^5} + \frac{8 K_m}{g \pi^2 D^4}$ for each pipe.

Equivalent Pipe Equations:

Pipes in Parallel
$$\left(\frac{D_{eq}^5}{f_{eq}L_{eq}}\right)^{1/2} = \sum_{i=1}^n \left(\frac{D_i^5}{f_iL_i}\right)^{1/2}$$
Pipes in Series $\frac{f_{eq}L_{eq}}{D_{eq}^5} = \sum_{i=1}^n \frac{f_iL_i}{D_i^5}$

LAMINAR FLOW IN CIRCULAR PIPES

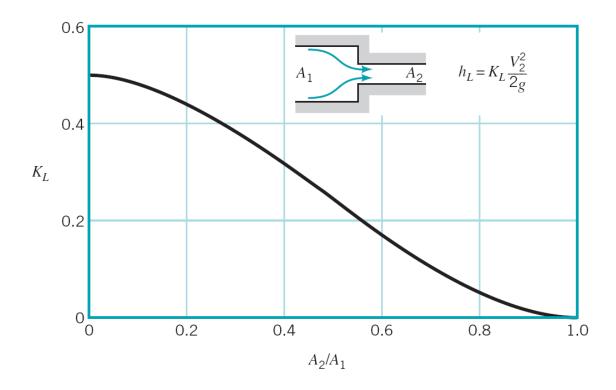
Entrance Length:
$$\frac{l_e}{D} = 0.06 \text{ Re}$$

Shear Stress: $\tau = \mu \frac{du}{dy} = \tau_w \frac{2r}{D}$
Wall Shear Stress: $\tau_w = \frac{\Delta pD}{4L} = \frac{8\mu V}{D} = \frac{f}{8}\rho V^2$
Velocity at the center: $V_c = \left(\frac{\Delta pD^2}{16\mu L}\right)$
Velocity at r: $u(r) = \left(\frac{\Delta pD^2}{16\mu L}\right) \left(1 - \left(\frac{2r}{D}\right)^2\right) = V_c \left(1 - \left(\frac{2r}{D}\right)^2\right)$
Average Velocity: $V = \frac{V_c}{2} = \frac{\Delta pD^2}{32\mu L}$
Flow Rate: $Q = VA = \frac{\pi D^4 \Delta p}{128\mu L}$
Friction (major) Loss: $h_f = f \frac{L}{D} \frac{V^2}{2g} = \frac{4L\tau_w}{\gamma D} = \frac{32L\mu V}{\gamma D^2}$
Friction Factor: $f = \frac{64}{Re} = \frac{8\tau_w}{\rho V^2}$
Friction Velocity: $u^* = \sqrt{\frac{\tau_w}{\rho}} = \sqrt{\frac{f}{8}}V$

TURBULENT FLOW IN CIRCULAR PIPES

Entrance Length: $\frac{l_e}{D} = 4.4 (\text{Re})^{1/6}$ Shear Stress: $\tau = (\mu + \mu_t) \frac{du}{dv} = \mu \frac{du}{dv} - \rho \overline{u'v'} = \tau_{lam} + \tau_{turb}$ Wall Shear Stress: $\tau_w = \frac{\Delta pD}{4I} = \frac{8\mu V}{D} = \frac{f}{8}\rho V^2$ Friction Velocity: $u^* = \sqrt{\frac{\tau_w}{\rho}}$ Average Velocity in the Viscous Sublayer: $\frac{\overline{u}}{u^*} = \frac{yu^*}{v}$ Viscous sublayer thickness: $\delta_* = \frac{5\nu}{v^*}$ Average Velocity in the Overlap Region: $\frac{\overline{u}}{u^*} = 2.5 \ln \left(\frac{yu^*}{v} \right) + 5.0$ Average Velocity in the Turbuent Region: $\frac{V_c - \overline{u}}{u^*} = 2.5 \ln \left(\frac{R}{v}\right)$ or $\frac{\overline{u}}{V_c} = \left(1 - \frac{r}{R}\right)^{1/n}$ $\frac{V}{V_c} = \frac{2n^2}{(n+1)(2n+1)}$ The Gradient of Average Velocity: $\frac{d\overline{u}}{dr} = -\frac{V_c}{nR} \left(1 - \frac{r}{R}\right)^{\frac{1}{n}}$ Friction Factor: $\frac{1}{\sqrt{f}} = -2\log\left(\frac{\varepsilon/D}{3.7} + \frac{2.51}{\text{Re}\sqrt{f}}\right)$

Loss Coefficient for a Sudden Contraction:



Loss Coefficient for a Sudden Expansion:

